

**GZA GeoEnvironmental, Inc.**

**FINAL  
IPEC QUARTERLY LONG-TERM  
GROUNDWATER MONITORING REPORT  
QUARTER THREE 2010  
(REPORT NO. 11)  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NEW YORK**

PREPARED FOR:

**ENTERGY NUCLEAR NORTHEAST, INC.**

INDIAN POINT ENERGY CENTER  
450 BROADWAY  
BUCHANAN, NEW YORK 10511



ON BEHALF OF:

ENTERGY SERVICES, INC.  
INDIAN POINT ENERGY CENTER  
295 BROADWAY, SUITE 3  
P.O. BOX 308  
BUCHANAN, NY 10511-0308

PREPARED BY:

**GZA GEOENVIRONMENTAL OF NEW YORK**

104 WEST 29<sup>TH</sup> STREET  
10<sup>TH</sup> FLOOR  
NEW YORK, NEW YORK 10001

JULY 10, 2012

FILE NO. 01.0017869.92



Copyright © 2011 GZA GeoEnvironmental of New York

**GZA**  
**GeoEnvironmental, Inc.**

*Engineers and  
Scientists*

July 10, 2012  
File No. 01.0017869.92

Mr. Patrick Donahue  
Indian Point Energy Center  
295 Broadway, Suite 3  
P.O. Box 308  
Buchanan, NY 10511-0308



104 West 29<sup>th</sup> Street  
10<sup>th</sup> Floor  
New York,  
New York  
10001  
212-594-8140  
FAX 212-279-8180  
<http://www.gza.com>

Re: **FINAL IPEC Quarterly Groundwater Monitoring Report  
Quarter Three 2010 (Report No. 11)  
Indian Point Energy Center  
450 Broadway  
Buchanan, New York 11501**

Dear Mr. Donahue:


GZA GeoEnvironmental of New York (GZA) is pleased to provide this Quarterly Groundwater Monitoring Report for Indian Point Energy Center located at 450 Broadway, Buchanan, NY.

We trust that this information satisfies your present needs. Should you need any additional information, please do not hesitate to call us at (781) 278-3805.

Very truly yours,

GZA GEOENVIRONMENTAL OF NEW YORK

  
Josh Simpson  
Engineer I

  
David Rusczyk, PE  
Senior Project Manager

  
Michael Powers, PE  
Consultant/Reviewer

  
Matthew J. Barvenik, LSP  
Senior Principal

Attachments: 3 Copies

Copyright © 2011 GZA GeoEnvironmental, Inc.

IPEC00263530



TABLE OF CONTENTS

	Page
<b>1.0 EXECUTIVE SUMMARY .....</b>	<b>1-1</b>
<b>2.0 SCOPE OF WORK .....</b>	<b>2-1</b>
2.1 Groundwater Elevation Measurement.....	2-1
2.2 Monitoring Installation Sampling .....	2-2
2.3 Vapor Containment Building Foundation Drain Sampling .....	2-2
2.4 Proactive Mid-Quarter and Confirmatory Sample Collection .....	2-3
2.5 Preventative Maintenance .....	2-3
<b>3.0 DATA EVALUATION.....</b>	<b>3-1</b>
3.1 Groundwater Mass Flux Computation.....	3-1
3.2 Groundwater Sampling .....	3-2
3.2.1 Groundwater Sampling Results.....	3-2
3.3 Radionuclide Release Rates .....	3-3
3.4 SSCs and Property Boundary Monitoring .....	3-3
3.4.1 Proactive Mid Quarter Samples .....	3-5
3.4.2 Previous Q2-2010 Investigation Level Exceedances.....	3-5
3.4.3 Q3 2010 Boundary Investigation Levels.....	3-7
3.4.4 Q3 2010 SSC Investigation Levels.....	3-8
3.4.5 Conclusions - Boundary and SSC Leak Detection Monitoring.....	3-14
3.5 Plume Natural Attenuation Monitoring .....	3-17
3.5.1 Unit 2 Tritium Plume Attenuation.....	3-18
3.5.2 Unit 1 Strontium Plume Attenuation .....	3-24
<b>4.0 CONCLUSIONS AND PLANNED FUTURE WORK.....</b>	<b>4-1</b>



## TABLES

Table 1	Groundwater Sampling Methods, Equipment, Frequency, and Depths
Table 2	Historic Quarterly Low Tide Groundwater Elevations
Table 3	2010 3 <sup>rd</sup> Groundwater Analytical Results and Averages
Table 4	2010 3 <sup>rd</sup> Quarter Groundwater Analytical Results and I.L.s
Table 5	Historic Groundwater Analytical Results

## FIGURES

Figure 1	Site Location Plan
Figure 2	Site Plan
Figure 3	Lower Hudson Valley Geologic Map
Figure 4	3 <sup>rd</sup> Quarter 2010 Current and Potential Future SSC Source Locations
Figure 5A	3 <sup>rd</sup> Quarter 2010 Longterm Transducer Monitoring Evaluation Map
Figure 6	3 <sup>rd</sup> Quarter 2010 Rolling Average Tritium Activity Map
Figure 6A	Temporal Trends in Unit 2 Rolling Average Tritium Activity Maps
Figure 6B	Unit 2 Leak Collection Device Evaluation 3 <sup>rd</sup> Quarter 2010
Figure 7	3 <sup>rd</sup> Quarter 2010 Rolling Average Strontium-90 Activity Map
Figure 7A	Sr-90 Baseline Analysis–Unit 1 Defueling Evaluation 3 <sup>rd</sup> Quarter 2010
Figure 8	3 <sup>rd</sup> Quarter 2010 Rolling Average Cesium, Cobalt, and Nickel Activity Map

## APPENDICES

Appendix A	Limitations
Appendix B	Transducer Installation Logs
Appendix C	Chains of Custody
Appendix D	3 <sup>rd</sup> Quarter 2010 Sampling Data Sheets
Appendix E	Post-Q3 2010 Mid-Quarter Sampling Data Sheets
Appendix F	Dose Calculations
Appendix G	Unit 2 Tritium Plume Trend Analyses
Appendix H	Southern Boundary Wells





## 1.0 EXECUTIVE SUMMARY

On behalf of Entergy Nuclear Northeast, Inc., GZA GeoEnvironmental of New York (GZA) has completed the Q3 2010 quarterly groundwater monitoring for the Indian Point Energy Center (IPEC), culminating in this report. Interpretations of the monitoring data have been made in the context of the current Conceptual Site Model. Development of this model began at the outset of the site investigations and has been iteratively enhanced as subsequent data has become available, in part through quarterly monitoring. The report has been written with a focus on the subject quarter's data. Relationships to prior data, more in-depth technical explanations and exceptions to generalized statements and conclusions have typically been relegated to footnotes. This report format was chosen to allow efficient assimilation of the most current data and analyses by those already familiar with the project. The footnotes contain important information and should be carefully read by all, but particularly by those less familiar with the technologies involved and the project history. It is further noted that the analyses and conclusions presented in this report are based on the data and information available up to and including the subject quarter. Data that becomes available after the subject quarter, but before the finalization date of the report is sequentially reflected in the associated subsequent reports.

Based on the quarterly groundwater sampling data for Q3 2010, GZA concludes that groundwater contaminants continue to migrate toward the Hudson River to the West, and have not migrated off the Site to the North, East or South.

Radionuclide concentrations measured during Q3 2010 were combined with previous quarterly and post-quarterly data to compute rolling average concentrations reflective of groundwater contaminant levels over the past twelve months. These data were multiplied by the associated individual zone-specific groundwater flux values, derived from the Precipitation Mass Balance Model<sup>1</sup>, to compute yearly average radionuclide release rates to the Discharge Canal and Hudson River. The Conceptual Site Model<sup>2</sup> (CSM), upon which this radionuclide dose computation is based, continues to be validated through: (1) groundwater elevation data downloaded quarterly from a focused set of transducer-monitored well installations; and (2) the behavior of both the Unit 1 Strontium plume and the Unit 2 Tritium plume as evaluated each quarter. These data, in our opinion, continue to support the use of the current CSM as a basis for Long Term Monitoring Program design.

The most recent quarterly data further support the conclusion that the overall Tritium activity in the Unit 2 plume is generally showing a historically decreasing trend, from both qualitative and quantitative perspectives. These overall reductions are seen on **Figure G-17**, where the total Tritium activity has decreased by approximately 45% since Q2 2007, and 89% when compared to the bounding level Tritium activities. This overall trend is also evident on **Figures 6 and 6A**, where the shaded plume<sup>3</sup> no longer extends downgradient to the river, as first observed in the

<sup>1</sup> Refer to Appendix H of the Quarter 2 2009 Quarterly Long-Term Groundwater Monitoring Report for discussion of the recalibration of the Precipitation Mass Balance Model. Precipitation and groundwater elevation data were collected onsite between 2007 and 2009 and used to compute groundwater fluxes across the site. Based on analyses of these data, it was concluded that this data set sufficiently encompassed the historical variability in groundwater elevation and flux response to seasonal and yearly precipitation variability. Therefore, maximum onsite groundwater fluxes were calculated from the elevation data, and used to conservatively recalibrate the Precipitation Mass Balance Model, as discussed and employed in the Q2 2009 Quarterly LTM Report.

<sup>2</sup> The formulation and basis for the overall CSM and the Precipitation Mass Balance model are presented in the Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc, on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

<sup>3</sup> The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value, and provides a reasonable demarcation level for illustrating plume geometry and temporal variation. Although this value equates to one-quarter of the drinking water standard for Tritium, GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to

## Section 1.0 Executive Summary

---

Q2 2009 quarterly data. It is further visually evident from **Figure 6A** that the core of the plume has also shown a marked decrease in concentration and extent over time in the vicinity of MW-111. These findings are consistent with our CSM, which anticipates overall decreasing trends in Tritium activity.

Consistent with one of the purposes of this Report, we also point out and explain data which, when first considered, may initially appear inconsistent with the assumptions used to develop the CSM. Such examples, where Tritium has increased in recent quarters, include:

- A transient Tritium peak in Manhole A2 and, to a lesser extent, MH-A4 was observed during the current (Q3 2010) quarterly monitoring round. Following the early July 2010 peak, the Tritium activity rapidly decreased (<1 week) to typical levels within the storm drain system. A similar transient Tritium peak was also observed in Manhole A2 during Q2 2009. As discussed in more detail in **Section 3.4** below, while the investigation into the source of these peaks is still ongoing, all indications are that it is associated with higher levels of washout entering the Fuel Storage Building (FSB) roof drain leading into MH-A2 when the SFP vent fan is not operating.
- The Q3-2010 result for MH-5 VCFD also showed a clear increase in Tritium activity when compared to the previous base line sampling results (including the previous sample from Q2 2010); however, the Post-Q3 2010 sampling data from only 10 days later show the Tritium activity in MH-5 VCFD had already returned to the previous baseline levels. The remaining radionuclides were all non-detect during both the Q3 2010 and the Post-Q3 2010 sampling events at MH-5 VCFD.
- A clear increase in the volume of water collected by the Unit 2 Leak Collection Device (LCD) was measured during the current (Q3 2010) quarter, beginning on July 5, 2010. The flow rate averaged approximately 1.5 L/day over the quarter. Investigations indicated that the increased flow could potentially be correlated<sup>4</sup> with atypically elevated water levels in the fuel pool, as associated with dry cask work. Following the limiting of these increases in pool water elevation, a marked decrease was observed in the LCD flow rate by the end of Quarter 3 / beginning of Quarter 4, back to levels generally consistent with baseline values of less than approximately 0.02 L/day. Based on these observations, a new figure (**Figure 6B**) has been included in this, Q3 2010, quarterly report which visually presents both the U2 LCD data and the historical Tritium data for the sampling intervals located within the Unit 2 Tritium plume boundaries. The recent LCD data are discussed in more detail in **Section 3.4** below.
- Peaks in Tritium activity have been observed in multiple sampling ports of MW-31 and MW-32 since Q1 2009, and to a lesser extent since monitoring began. This long-term variability appears to be consistent with episodic releases of Tritium historically stored in the subsurface via natural and anthropogenic Retention Mechanisms<sup>5</sup>. This conclusion is further supported by the tracer data and other analyses discussed in Section 3.6 of the Q1 2009 Long Term Monitoring Report.
- While Retention Mechanisms clearly appear to impact Tritium levels as summarized above, more noticeable increases in Tritium activity in a number of intervals within MW-31 and MW-32 were initially measured during the Q1 and post Q1 2010 sampling events, where Tritium activities peaked at levels higher than previously measured. Similarly elevated Tritium activities continued in Q2 and through the current Q3 and post

---

develop plume delineations. This is a typical approach to conservatively represent three-dimensional contaminant data sets on two-dimensional maps.

<sup>4</sup> While the data trends appear to correlate, it is noted that simple correlation does not demonstrate causation.

<sup>5</sup> These Retentions Mechanisms are discussed along with the CSM in the previously cited Hydrogeologic Site Investigation Report.

## Section 1.0 Executive Summary

---

Q3 2010 sampling events at these Unit 2 locations. These Q1 through Q3 2010 Tritium peaks appear related to a Q4 2009 localized and transient surface spill from a temporary rental RWST/R.O. processing skid<sup>6</sup> which was first detected during routine 80-10 sampling of MH-9 in mid-January 2010.

- The activity at most downgradient wells this quarter appears to be decreasing relative to the previous quarter, with only a limited number of new peaks observed. While the number of these peaks is significantly lower than that observed in the previous quarter, it is expected that such peaks, potentially exceeding the Unit 2 Tritium I.L.s, will continue to be observed in downgradient wells as the transient RWST/R.O. spill works its way towards the river. The number and degree of Tritium peaks measured in the previous quarter (Q2 2010) resulted in an increase in the Unit 2 plume total Tritium activity. However, as shown on **Figure G-17 (Appendix G)**, this previous increase was immediately followed by a decrease (of similar magnitude) in total Tritium activity during the current, Q3 2010 quarter.
- Pursuant to the RWST/R.O. surface spill, it is further noted that Tritium activity in MH-9 quickly returned to typical background levels once the spill was addressed. It is therefore anticipated that the Tritium peaks attributed to the RWST/R.O. skid surface spill will also continue to generally decrease over the next several quarters, as is already reflected by the decrease in the current Q3 2010 graph of total Tritium activity in the Unit 2 plume.
- Our review of data generally found no compelling evidence that the observed increases in Tritium activity result from development of new, unidentified leaks in the Unit 2 SFP or other monitored Systems, Structures, or Components. However, it is noted that the LCD showed increased flow rate during this quarter. While all LCD water is fully contained and does not enter the groundwater regime, and the Tritium peaks observed in the groundwater monitoring intervals can be explained by the transient RWST/R.O. processing skid surface spill and associated Retention Mechanisms, peaks in MW-31, MW-32 and MH-5 VCFD appear to be potentially correlated, on a temporal basis, with this increased LCD flow rate<sup>7</sup>.

The overall Sr-90 activity within the Unit 1 plume had generally been stable to decreasing in response to the West Pool demineralization operations conducted by Entergy beginning in 2006. However, the final defueling of the Unit 1 SFPs, completed in Q4 of 2008, resulted in a noticeable increase in Strontium activity proximate to the SFPs, followed by downgradient increases (see **Figure 7 and 7A**). This was expected given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing leakage rate from the SFPs<sup>8</sup>. As expected, the levels proximate to the pool have since decreased to pre-defueling Strontium activities and levels downgradient of the pool are currently exhibiting decreasing trends approaching pre-defueling levels or have already decreased to pre-defueling Strontium activities (MW-55, MW-57) this quarter. It is expected that the further downgradient wells will also fully return to pre-defueling levels once this transient perturbation has passed through the groundwater flow system. It is anticipated that this flushing mechanism will be protracted given the impact of partitioning on Strontium levels in the groundwater.

Based on the data and analyses provided herein, our conclusion is that the Tritium and Strontium plumes have both been undergoing overall long-term reductions in activity after the

---

<sup>6</sup> The spill involved a rented RWST/R.O. processing skid brought on-site by an outside contractor. As such, this equipment is not an in-place Unit 2 SSCs and is no longer on site.

<sup>7</sup> While the data trends appear to correlate on a temporal basis, it is noted that simple correlation does not demonstrate causation.

<sup>8</sup> As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

## Section 1.0 Executive Summary

---

respective source interdiction. Given this conclusion, and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP<sup>9</sup> and has decommissioned the Unit 1 SFPs, these plumes satisfy the requirements for Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. However, it is also concluded that, while a portion of the leakage from the above cited localized, transient spills traveled directly to the saturated groundwater regime and resulted in the observed transient “peaks” in radionuclide levels, additional portions of these releases likely remain above the water table as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events). These localized release events also interfere with the goal of resetting Site Investigation Levels (I.L.s); updating of Strontium I.L.s must therefore await return to the original Strontium baseline levels existing prior to Unit 1 defueling, and additional seasonal data is required to better assess Tritium response to precipitation-driven Retention Mechanism release variability. Therefore, the ultimate confirmation of the above conclusions will require monitoring over a number of years so as to allow ranges in seasonal variation to be adequately reflected in the monitoring data and thus demonstrate the rate of continued depletion of Tritium and Strontium from the Retention Mechanisms. In this regard, it is important to recognize that even with the somewhat increased Tritium levels currently observed due to the transient surface spill from the temporary rental RWST/R.O. skid, the amount of radionuclides being released through the groundwater pathway is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

In summary, based on the data collected to date, the apparent strength of the CSM to evaluate that data, and the completion of source interdictions by Entergy, we believe all Program Objectives (see **Section 3.0**) are being met. These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI).

---

<sup>9</sup> Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report. The Q1 2009 Report summarizes additional, more quantitative analyses which were completed to further investigate the integrity of the Unit 2 SFP. These analyses provide further support for the original conclusion that the Unit 2 SFP is no longer leaking. However, given the behavior observed in the Unit 2 collection device data (see Section 3.6 of the Q1 2009 Long Term Monitoring Report and the more recent data presented herein for this quarter – Q3 2010), additional investigations/data evaluations are underway to further rule out potential Unit 2 SFP leak mechanisms. In this regard, it is noted that these analyses cannot definitively and completely rule out the possibility of a remaining small leak which could then also be supplying Tritium to the groundwater flow regime in addition to the Retention Mechanism(s) and surface spill from the process skid discussed above. While it is not possible to quantify the size of the minimum detectable leak with any degree of certainty, we believe that the maximum leak rate from the Unit 2 SFP that could potentially remain undetected by the groundwater monitoring system is less than 10 to 30 gpd (0.007 to 0.021 gallons per minute). It is also likely that if a small leak exists in the Unit 2 SFP liner, it should not get worse with time. This opinion is based on liner evaluations previously conducted by Entergy. It is further emphasized that while a leak of more than 0.02 gallons per minute should be large enough to be readily detectable with the existing Long Term Monitoring Program; this amount of Tritium release to the river is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.



## 2.0 SCOPE OF WORK

During Q3 2010, GZA performed groundwater monitoring at IPEC in Buchanan, New York (Site) as part of IPEC's overall Long Term Groundwater Monitoring Program (LTMP) at the Site<sup>10</sup>. The overall foundation for the development and execution of this LTMP is based on the CSM, a description of which is contained within GZA's Hydrogeologic Site Investigation Report<sup>11</sup>. The scope of work completed for this quarter's monitoring is described in the Sections below. Refer to **Figures 1 and 2** for a Site Location Plan and Site Plan. **Figure 3** provides a Lower Hudson Valley Geologic Map and **Figure 4** summarizes Current and Potential Future SSC Source Locations.

### 2.1 Groundwater Elevation Measurement

GZA maintains a network of long-term monitoring transducers and dataloggers as part of the instrumentation located across the Site. These instruments record groundwater elevation and temperature measurements at regular time intervals<sup>12</sup>, which are then downloaded on a quarterly basis<sup>13</sup>. Transducer installation logs are presented in **Appendix B**.

During the quarterly sampling, GZA downloaded groundwater elevation data from the long-term monitoring transducers, which collected data over the entire duration of the quarter. The low-tide groundwater elevation data during Q3 2010 (07/31/2010) from these 22 transducers are presented in **Table 2** and compared to historic minimum and maximum values on **Figure 5A**<sup>14</sup>. The Q3 2010 groundwater elevation data at two locations (three transducer intervals) are outside the Q2-2007 through Q2-2009 range; however, the maximum deviation was still only one foot in elevation. In addition, the data showed no change in groundwater flow direction and no substantial variations in overall horizontal and vertical gradients were evident from these Q3 2010 groundwater elevation data. Therefore, these data demonstrate that substantial variations to the observed flow field have not occurred. These data thus further validate the applicability of the Precipitation Mass Balance Model (PMBM) for use in subsequent radiological dose computations – see **Section 3.1**.

<sup>10</sup> Refer to the "Quarterly Long-Term Groundwater Monitoring Report Q2-Q4 2007 (Report No. 1)," dated May 2008 for Site background information and a description of the environmental setting.

<sup>11</sup> Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc, on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

<sup>12</sup> Currently, transducers record groundwater elevation and temperature readings on a 20 minute time interval so as to allow capture of tidal variability. An original, more extensive network of pressure transducers provided critical data inputs for the development of the CSM and the computation of yearly radiological dose to the Hudson River. Over the first nine quarters of the LTM program (Q2 2007 through Q2 2009) sufficient data was collected from this more extensive network of transducers to capture groundwater elevation response to seasonal and yearly precipitation variability. Therefore, starting with the Q3 2009 quarterly report, the transducer monitoring program was refocused on a select subset of locations to routinely monitor the on-Site groundwater conditions going forward. These locations were selected to provide the data required to document that groundwater flow conditions remain consistent with the CSM, thus demonstrating the veracity of the subsequent dose computations. The rationale for the specific locations and depths included in the LTMP transducer redeployment are provided in Appendix K of the Q1 2009 Quarterly Monitoring Report (Report No.5), dated July 2, 2010 and Appendix J of the Q2 2009 Quarterly Monitoring Report (Report No.6).

<sup>13</sup> With regard to these ongoing long term monitoring locations, it is noted that the transducers have a limited life. While some of the transducers can be replaced, and have been replaced in the past, others are permanently installed in the subsurface and are no longer accessible for replacement. However, with time, the base of data upon which model validity is assessed becomes increasingly more robust. Therefore, if some of these transducers fail over time, it is not likely that replacement will be imperative. This is because the likelihood of encountering a precipitation event substantially outside the already captured range becomes increasingly more remote with time as more data are collected. In addition, it is again emphasized that considerable conservatism has been incorporated within the model development and the dose rates computed are still far below those permitted by regulation.

<sup>14</sup> Figure 5, which previously presented shallow and deep groundwater contours, can be found in quarterly reports prior to, and including Q2 2009. This figure is no longer required given that sufficient quarterly contour data has already been obtained (See Q2 2009 for further analysis).

## Section 2.0 Scope of Work

---

### 2.2 Monitoring Installation Sampling

During Q3 2010, GZA collected groundwater samples for radionuclide analysis from scheduled sampling intervals within select monitoring installations (“wells”) as shown in **Table 3**. Chains of Custody for these samples are presented in **Appendix C**. Collection of additional groundwater sample volume to provide aliquots to regulatory agencies (e.g., Nuclear Regulatory Commission (NRC), NYDEC, etc.) was not required this quarter.

GZA used a number of different types of pumping equipment depending upon the sampling method and the characteristics of the individual monitoring installation<sup>15</sup>. **Table 1** lists the monitoring installations sampled, the sampling depths and elevations within sampling installations, and the sampling method and equipment used.

In general, GZA implemented two basic methods of sampling to collect representative groundwater samples: the Low Flow method and a modified well volume purge method. The Low Flow method allows collection of representative groundwater samples from discrete sampling zones within a monitoring installation, while limiting the accumulation of wastewater<sup>16</sup>. As agreed by Entergy Nuclear Northeast, the NRC, NYSDEC, and GZA, the modified traditional purge method<sup>17</sup> allows for the collection of a representative groundwater sample from a monitoring installation after purging 1.5 volumes of water<sup>18</sup>. We implemented this method in wells where low flow sampling was not practical. Sampling Data Sheets summarizing water quality data and sampling information are presented in **Appendix D**.

With all of the above sampling methods, GZA used dedicated sampling equipment, including polyethylene and/or nylon tubing and submersible electric pumps to the extent practical. The use of dedicated sampling equipment limits the possibility of cross-contamination between monitoring installations and/or individual multi-level samples within a single installation. Refer to **Table 1** for a summary of the sampling methods, equipment, frequency, and depths employed during this quarter’s groundwater monitoring round.

### 2.3 Vapor Containment Building Foundation Drain Sampling

GZA collected a water sample from on-Site manholes MH-5 VCFD, B-1 and B-6 to characterize discharge from foundation drains around and below the Unit 2 and 3 Vapor Containment Structures. These drains include both foundation drains around the building peripheries (“curtain drains”) as well as those around the sumps near the middle of the structures (“reactor sump footing drains”<sup>19</sup>).<sup>20</sup>

---

<sup>15</sup> Refer to Section 4.3 of the Final 2007 Quarterly Long-Term Groundwater Monitoring Report No. 1, dated May 2008, for sampling method and equipment selection rationale.

<sup>16</sup> As described in: Low-Flow Sample Collection, GZA, 7/18/2007

<sup>17</sup> As described in: Modified Traditional Groundwater Sample Collection, GZA, 7/18/2007

<sup>18</sup> When external factors (such as well-surface-flooding from storm water runoff or overland flow of plant component leaks) might have infiltrated the top of the well and impacted ambient groundwater conditions at a specific sampling location, GZA typically purged three to five volumes of water (using the modified traditional purge method) prior to collection of a sample to attempt to obtain a representative groundwater sample.

<sup>19</sup> We could not verify that a foundation drain exists around the reactor sump in Unit 2. The assumption that it does exist is based on the plans for Unit 3 and the similarities in construction of both units.

<sup>20</sup> These two Unit 2 drains which discharge into MH-5, along with similar drains for Unit 3 which discharge into Manholes B-1 and B-6, form an integral part of the early leak detection monitoring network. However, sampling from these three manholes has generally been problematic for a number of reasons, but particularly due to conflicts with plant security measures which mandate that the manhole covers be permanently welded shut. Some limited access has been reestablished by modifying the manhole covers to allow for a small access opening. However, for Manholes B-1 and B-6, this modification still limits the ability to routinely collect samples clearly representative of only the foundation drain discharges rather than the total flow through the storm drains. The piping configuration in MH-5 does allow sampling specific to the foundations drains, hence the designation of this sample as MH-5 VCFD (i.e., Vapor Containment Foundation Drain). Further work is being undertaken on the manhole sampling systems in B-1 and B-6 to facilitate more representative sampling of these foundations drains.

## Section 2.0 Scope of Work

---

### 2.4 Proactive Mid-Quarter and Confirmatory Sample Collection

In response to the recent peaks in Tritium activity in multiple MW-31 and MW-32 sampling intervals, additional Post-Q3 2010 groundwater samples were collected at all sampling intervals within MW-31 and MW-32 (as well as MW-30). Post-Q3 2010 groundwater samples were also collected at MW-33, MW-111 and MH-5 VCFD. The MH-5 VCFD confirmatory sample was collected to investigate/verify the elevated Tritium result during the Q3 2010 sampling event (discussed in **Section 3.4.4** below).

The results of the confirmatory and proactive mid-quarter samples are presented in **Section 3.4** along with the quarterly data. Sampling Data Sheets summarizing water quality data and sampling information are presented in **Appendix E**.

### 2.5 Preventative Maintenance

GZA performed general wellhead maintenance tasks, such as housekeeping of well vaults and roadboxes, and replacement of dedicated sampling equipment, tubing and transducers, as required.



### 3.0 DATA EVALUATION

The Long Term Monitoring Program was designed to provide data to address four main objectives:

- Monitor radionuclide activities and evaluate groundwater flow rate to both detect and characterize current and potential future off-Site groundwater contaminant migration to the Hudson River, both via direct groundwater discharge to the river and through infiltration into the Discharge Canal, from unplanned radionuclide releases of liquid effluents, so as to allow computation of potential radiation dose to the public from these releases;
- Monitor groundwater proximate to Systems, Structures and Components (SSCs) that exhibit a credible probability of resulting in a visually undetected release of radionuclides to the subsurface carrying an activity level of significance;
- Monitor groundwater along the property boundary to confirm that contaminated groundwater is not migrating off of the property to locations other than the river; and
- Monitor the groundwater plumes identified on-Site to demonstrate overall reductions in total activity over time as is consistent with the requirements of Monitored Natural Attenuation (MNA)<sup>21</sup>, the selected remediation for the IPEC Site.

These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI). The following sections provide data analyses to address these four objectives.

#### 3.1 Groundwater Mass Flux Computation

As presented in the Hydrogeologic Site Investigation Report, the groundwater flow in both the upper and lower flow zones is toward the power block area from the North, East and South, with subsequent discharge to the Hudson River to the West. We estimate that groundwater flow associated with infiltration from the watershed may be as deep as 350 feet, but still ultimately discharges to the river. A corollary to this conclusion is that there is no groundwater flow, and thus no off-Site radionuclide migration from the power block area to the North, East or South.

To estimate groundwater flow (i.e., groundwater mass flux) beneath the Site, a groundwater flow model was constructed based on a precipitation mass balance analysis. This analysis is based on the precept that, on a long term average, the groundwater flowing through and discharging from the aquifer is equal to the watershed infiltration recharge; this conclusion was reached because the only substantial source of recharge to the aquifer is areal recharge derived from precipitation. The previous fifteen year average for precipitation measured at the Site is approximately 36 inches per year. Based on a USGS infiltration study<sup>22</sup>, as well as the Precipitation Mass Balance Model (PMBM) calibration<sup>23</sup>, approximately 25 percent of the

<sup>21</sup> The selection of MNA as the remedial strategy for the Site is discussed further in the Hydrogeologic Site Investigation Report.

<sup>22</sup> USGS. Water Use, Ground-Water Recharge and Availability, and Quality of Water in the Greenwich Area, Fairfield County, Connecticut and Westchester County, New York, 2000-2002.

<sup>23</sup> The Precipitation Mass Balance Model (PMBM) was initially calibrated to groundwater fluxes based on a Darcy's Law Model with groundwater gradients derived from Q2 2007 (June 1, 2007) low-tide groundwater elevation contours (initial reference data set). The two models use different sets of input parameters which are not dependent or related to each other. This calibration not only verified the reasonableness of the overall groundwater flow rates predicted by the PMBM, but also allowed further discretization of the groundwater flow into upper and lower flow zones as well as flow volumes upgradient and downgradient of the Discharge Canal. After reviewing the groundwater elevation and precipitation data from the Indian Point meteorological station over the time period from Q2 2007 to Q2 2009, it was concluded that sufficient seasonal data had been collected to encompass the majority of the precipitation variability observed over the last fifteen years. Therefore, the PMBM was also recalibrated after collecting the final full set of transducer data in Q2 2009. Data analyses demonstrated that recalibration to the Q4 2008 data set yielded the most



## Section 3.0 Data Evaluation

---

precipitation falling on pervious surfaces over the Site watershed area recharges the groundwater system via infiltration.

Since precipitation represents the driving variable for groundwater flux in the PMBM<sup>24</sup>, the yearly precipitation just prior to Q3 2010 (approximately 37 inches) was calculated and input into the recalibrated model to compute the flows used in the estimation of Q3 2010 dose values. Based on the USGS study cited above, the aquifer recharge rate is therefore approximately 10 inches for the year prior to the Q3 2010 monitoring event. Applying this value to the pervious surfaces within the six individual groundwater flow zones shown on **Figure 4**, it is estimated that approximately 5 gpm of groundwater flowed into the Discharge Canal from the upper and lower zones during the previous year. In addition, approximately 9 gpm and 11 gpm of groundwater flowed into the Hudson River from the upper and lower zones, respectively. Storm water discharging into the Discharge Canal and directly into the Hudson River was estimated to be approximately 41 and 4 gpm, respectively. These flows are further subdivided into flow zones with the further detail shown in the table in **Appendix F**.

### 3.2 Groundwater Sampling

The following sections describe the groundwater sampling results and associated QA/QC protocols.

#### 3.2.1 Groundwater Sampling Results

Groundwater samples collected on behalf of Entergy during Q3 2010 were analyzed at GEL Laboratories for Tritium, Sr-90, Cs-137, Co-60, and Ni-63<sup>25</sup>. **Table 3** presents the Q3 2010 analytical results for these radionuclides. The rolling yearly averages, which are calculated using all the valid data from the previous year [Q4 09 through Q3 10], including Mid-Quarter and confirmatory samples, are also presented in **Table 3**. **Table 4** presents minimum detection concentrations (MDC), standard deviation, and I.L.s assigned to each well for the Q3-2010 analytical results. **Table 5** presents historic Site groundwater analytical data. Isopleth maps of rolling averages for Tritium and Sr-90 are presented in **Figures 6** and **7**, respectively. **Figure 8** presents a data map of rolling averages for Cs-137, Co-60, and Ni-63<sup>26</sup>.

An overall evaluation of the sample handling, shipment and analytical procedures, indicates that the quality assurance quality control protocols have been met in Q3 2010 for all of the samples, and the analytical results should be useable as presented in **Table 5**. This conclusion is further supported by a review of the Q3 2010 analytical data, as compared to previous historical trends.

---

conservative (highest dose to the river) calibration of the nine quarterly data sets obtained during the LTMP, thus this quarter's (Q4 2008) data set was adopted for further dose computations. The recalibration of the model to the Q4 2008 data yielded Unit ½ Zone and total groundwater fluxes approximately 40% and 25% greater, respectively, than the original reference (Q2 2007) data set. Further information and the data analyses are provided in the Q2 2009 LTM report.

<sup>24</sup> To continue to validate the appropriateness and applicability of the PMBM, a subset of the existing transducers are being maintained and monitored quarterly as part of the Long Term Monitoring Program, starting with the Q3 2009 Quarterly Report. The primary objective of maintaining these transducers is to provide ongoing confirmatory data that demonstrate substantial changes to the on-Site groundwater flow field have not taken place and thus verify that the basic assumptions inherent in the PMBM continue to remain valid. The transducer locations are provided on **Figure 5A** of this quarterly report, and the rationale for the selection of these specific individual transducer locations is discussed in the Q1 and Q2 2009 quarterly reports. With regard to these ongoing long-term monitoring locations, it is noted that the transducers have a limited life. While some of the transducers can be replaced, and have been replaced in the past, others are permanently installed in the subsurface and are no longer accessible for replacement. However, with time, the base of data upon which model validity is assessed becomes increasingly more robust. Therefore, if some of these transducers fail over time, it is not likely that replacement will be imperative. This is because the likelihood of encountering a precipitation event substantially outside the already captured range becomes increasingly more remote with time as more data is collected. In addition, it is again emphasized that considerable conservatism has been incorporated within the model development and the dose rates computed are still far below those permitted by regulation.

<sup>25</sup> It should be noted that samples were also analyzed for gamma emitters via gamma spectroscopy. Although only Co-60 and Cs-137 are reported, gamma spectroscopy should detect and identify other gamma emitters if they became present in groundwater.

<sup>26</sup> Isopleths were not drawn for Cs-137, Co-60, and Ni-63 because the few positive detections observed did not indicate the existence of a groundwater plume containing these radionuclides. This is likely a result of the high surface affinity (highly adsorptive nature) of these radionuclides for solid geological materials. They therefore tend to rapidly partition out of the groundwater.

## Section 3.0 Data Evaluation

Refer to **Section 5.2.2** of the Final 2007 Quarterly Long-Term Groundwater Monitoring Report No. 1 for further details pursuant to quality assurance quality control protocols.

### 3.3 Radionuclide Release Rates

The recalibrated PMBM-derived groundwater flows within each of the six flow zones are multiplied by yearly rolling average radionuclide levels within each zone to compute groundwater radionuclide release rates to the Discharge Canal and Hudson River. These groundwater radionuclide release rates are computed separately for upper and lower flow zones as well as upgradient and downgradient of the Discharge Canal. The selection of specific monitoring locations for each of the six zones is described in the January 25, 2008 Memorandum – Synopsis of Long Term Monitoring Plan Bases.

Storm drain flows<sup>27</sup> computed based on yearly precipitation rates are multiplied by radionuclide concentrations measured in the storm drains to compute the associated storm drain radionuclide release rates<sup>28</sup> to the Discharge Canal and Hudson River.

The radionuclide release rates from the groundwater and storm drains to the Discharge Canal and Hudson River for Q3 2010 are shown in the table below.

	GROUNDWATER AND SURFACE WATER TO RIVER (Ci/YR)	GROUNDWATER AND SURFACE WATER TO CANAL (Ci/YR)
Northern Clean Zone*	3.64E-04	0.00E+00**
Unit 2 North Zone	5.55E-04	4.17E-02
Unit ½ Zone	5.98E-03	6.34E-03
Unit 3 North Zone	2.87E-03	8.32E-04
Unit 3 South Zone	1.67E-03	1.90E-02
Southern Clean Zone*	3.38E-03	1.17E-02

\* Activity in the Northern Clean Zone is attributable to an assumed Tritium background concentration of 150 pCi/L in the groundwater. The remaining radionuclides were assumed to not be present in this streamtube. Radionuclide release rate in the Southern Clean Zone is calculated from activity measured in monitoring wells MW-40 and MW-51.

\*\* The radionuclide release rate to the Discharge Canal from the Northern Clean Zone is zero because the Discharge canal does not extend far enough to the north to be downgradient of the Northern Clean Zone.

These release rates are then used by Entergy to calculate the radiological dose to a hypothetical maximally exposed individual and the environment via the Discharge Canal and the Hudson River using the procedure outlined in the Off Site Dose Calculation Manual (ODCM) Reversion 3.

### 3.4 SSCs and Property Boundary Monitoring

In addition to providing the data for the dose computation discussed above, the Long Term Monitoring Program has been designed to also provide rapid detection of potential leaks from SSCs. This monitoring is specifically focused on those SSCs which exhibit a credible probability of resulting in a visually undetected release of radionuclides to the subsurface<sup>29</sup>. The monitored SSCs are shown on **Figure 4** and a description of the specific monitoring installations

<sup>27</sup> The storm drain flows also include groundwater discharges from the foundation drains for Unit 2 and Unit 3 VC Buildings, but not from the Unit 1 NCD and SFDS, which are otherwise accounted for.

<sup>28</sup> It is noted that storm drain samples are not typically taken at times coincident with peak, or even average storm drain flow rates. By its very nature, the vast majority of the flow through the storm drain system tends to be episodic and of short duration due to storm events; sampling rounds are generally scheduled to avoid such events. Radionuclide concentrations are primarily due to groundwater infiltration into the drains and thus tend to be highest during periods of little rain when this infiltration is not diluted by the storm water flow. This incongruence therefore yields a high bias to the dose computation because the elevated concentrations associated with low flow rates are multiplied by the much higher flow rates based on total yearly rainfall.

<sup>29</sup> As discussed further in the following sections, reporting of visually identified spills/leaks within structures is included within Condition Reports under Entergy's Corrective Action Program. Additional emphasis has been placed on routine review of these reports as they potentially relate to GPI objectives.

## Section 3.0 Data Evaluation

---

associated with each SSC are provided in the January 25, 2008 Memorandum – Synopsis of Long Term Monitoring Plan Bases. In addition to monitoring the SSCs, on-Site and off-Site wells are used to monitor the property boundaries for unanticipated radionuclide migration across these boundaries. Again, the rationale underpinning the selection of wells designated for this purpose is provided in the above cited Memorandum. These monitoring protocols are consistent with the NEI Groundwater Protection Initiative (GPI).

Entergy is also in the planning process to add an additional multi-level monitoring installation located near the south west corner of the Unit 3 Transformer Yard, downgradient of MW-46<sup>30</sup>. While MW-46 was previously evaluated relative to Unit 3 monitoring effectiveness, and was found to be very useful for detecting potential future releases, we also concluded that without a further monitoring well installation, there is a moderate risk that some releases could go undetected. In particular, it appears that a release in the vicinity of the Waste Holdup Tank pit could potentially proceed toward the river to the south of MW-46, given the likely hydrology associated with the pre-construction bedrock valley in this area. As such, we recommend, and Entergy agreed to, the construction of an additional monitoring installation at Unit 3 to increase the robustness of the Unit 3 well network and thus reduce this potential risk. Installation of this well is currently scheduled for 2011. The sampling of U1-NCD and U1-SFDS will also be continued as part of the Long Term Monitoring Program.

I.L.s were established for the associated monitoring wells to set quantitative radionuclide concentrations above which further action would be undertaken. As part of the ongoing groundwater monitoring program, the reported analytical concentrations are compared against I.L.s established based on the criteria shown in the table below. I.L.s are currently computed each year based on yearly averages of all the valid groundwater sampling analytical results of the previous year including Aliquot, Confirmatory, and Mid-Quarter sample results<sup>31</sup>. The monitoring well-specific I.L.s are presented in **Table 4** and are established for comparison with 2010 analytical results based on the quarterly samples collected and analyzed in 2009.

---

<sup>30</sup> A cross section has also previously been developed through the Unit 3 area to supplement **Figure 4** and further demonstrate the relationship of site groundwater flow patterns and monitoring well placement relative to the individual Unit 3 SSCs (similar cross sections were previously developed for Units 1 and 2, as presented in the Hydrogeologic Site Investigation Report). This Unit 3 cross section C-C' is included in the Q1 2009 Quarterly Report as Figure 4A.

<sup>31</sup> The calculation of ILs and yearly rolling averages prior to the Q1 2009 Report were based on the analytical results from the quarterly sampling rounds only, and therefore excluded aliquot, confirmatory and mid-quarter sample results. For the Q1 2009 Report and thereafter, if an aliquot analytical result confirms that the original quarterly analytical result was false, then only the aliquot result is utilized in the yearly IL calculation. If the aliquot result confirms the original quarterly result is valid, then both the original and the aliquot results are averaged together and then averaged into the yearly IL calculation as a single value. Confirmatory analytical results have the potential to impact the use of the original quarterly sample in the same manner as aliquots; however, unlike aliquots, these "independent samples" are averaged directly into the yearly rolling average without "pre-averaging" with the associated quarterly sample. Similar to confirmatory samples, mid-quarter samples are also averaged directly into the yearly rolling average calculation. However, mid-quarter sample results do not have any impact on the use of the initial quarterly samples as can either aliquot or confirmatory samples, as described above. In the case of both confirmatory and mid-quarter sample results, direct averaging into the yearly average of these additional results can somewhat bias the yearly average toward a particular quarter/season. However, given that confirmatory and mid-quarter samples are typically taken to confirm and/or prepare for uncharacteristically high radionuclide concentrations, this direct averaging provides a high bias to the subsequent yearly dose computations, and is thus conservative. In cases such as this where some bias inevitably will be created, establishing a conservative bias in the dose computations is considered more important than maintaining a seasonal non-bias.

**Section 3.0 Data Evaluation**

WELL ID	INVESTIGATION LEVELS (I.L.s)		
	TRITIUM pCi/L	Sr-90 pCi/L	OTHER PLANT-RELATED RADIONUCLIDES
Off-Site Boundary Wells (LAF-002)	any detection*	any detection*	any detection*
On-Site Boundary Wells (MW-40, MW-51, MW-52, and MW-107)	1,000**	2**	any detection*
Riverfront Boundary Wells (MW-60, MW-62, MW-63)	2,000**	2**	any detection*
All Other Wells	>2x average***	>2x average***	>2x average***

\* A radionuclide is positively detected when the result is greater than or equal to the MDC and 3 times the 1 sigma uncertainty.  
 \*\* The values of 1000 and 2000 pCi/L for H-3 and 2 pCi/L for Sr-90 have been chosen to be low enough to result in timely detection of a new release or change to an existing release and still be outside the normal expected range of sample results at these locations, to the extent possible with the currently available data over time.  
 \*\*\* Any positively detected radionuclide that has a result greater than 2 times the average from the previous year. However, the IL is not reached until an H-3 result is also greater than 1000 pCi/L or a Sr-90 result is also greater than 2 pCi/L.

In the event that the analytical results of a groundwater sample exceed the designated I.L., the following series of actions will be considered:

- Contact the laboratory to verify that all quality control checks were satisfactory, sufficient sample volume was used; required MDC's were met, etc.;
- Re-analyze Aliquots of the original sample;
- Re-sample the location (Confirmatory sample) to verify the result;
- Increase the frequency of sampling (Mid-Quarter samples) for this location<sup>32</sup>;
- Initiate an investigation utilizing Entergy's corrective action program and related resources as appropriate (e.g. site engineering / radiation protection); and
- Initiation of source/ground water remediation techniques commensurate with the potential dose impact analyses and good environmental stewardship.

**3.4.1 Proactive Mid Quarter Samples**

During the Q3 2010 monitoring period, there were no planned operations that required increased sampling. However, recent peaks in Tritium levels have been observed in multiple MW-31 and MW-32 sampling intervals and also in MH-5 VCFD; thus, additional Post-Q3 2010 groundwater samples were collected at all sampling intervals within MW-31 and MW-32 (as well as MW-30, MW-33, MW-111, and MH-5 VCFD). The results of these samples are reported and discussed below along with the quarterly results.

**3.4.2 Previous Q2-2010 Investigation Level Exceedances**

As indicated in the previous Q2 2010 Quarterly LTM Report, a comparison of the Q2 2010 analytical results to their respective I.L. values showed that the I.L.s were initially exceeded at ten sampling locations. Four of these I.L. exceedances are still ongoing, and are discussed individually in **Section 3.4.4** below. The remaining six I.L. exceedances (MW-36-24, MW-37-40, MW-50-42 (Tritium), MW-53-82, MW-111 and U3-4D) were resolved during the Post Q2 2010 and/or Q3 2010 sampling, as summarized below.

**MW-36-24.** The Q2 2010 Tritium activity at this sampling location slightly exceeded the I.L.<sup>33</sup> The subsequent Q3 2010 results indicate that Tritium has decreased to a level approximately

<sup>32</sup> It is noted that Mid-Quarter samples are also proactively obtained when plant operations could potentially result in an increased probability of a release to the subsurface.

## Section 3.0 Data Evaluation

---

one order of magnitude below the I.L.. Based on the downgradient well location and the Q2 2010 timing of the increase, it was concluded that the likely cause was the transient surface spill from the temporary rental RWST/R.O. processing skid<sup>34</sup>. Because the RWST/R.O. skid spill was terminated and Tritium is a non-sorbing radionuclide, Tritium levels were expected to decrease relatively quickly, as supported by the Q3 2010 data.

**MW-37-40.** The Strontium result for Q2 2010 slightly exceeded the I.L. for this sampling interval; however, the Strontium activity decreased below the I.L. during the current, Q3 2010 sampling event. An elevated Strontium activity has been observed at MW-37-40 since Q3 2009, which has been attributed to a delayed response to the increase in water levels during defueling operations in the Unit 1 SFPs. The trend for this depth interval over the previous two years is similar to those exhibited by the intervals immediately above and below (MW-37-32 and MW-37-57), except that MW-37-40 lags in response somewhat. This time lag is likely a result of the lower hydraulic conductivity (by two to three orders of magnitude) of the bedrock accessed by this depth interval. Because MW-37-57 had already decreased to pre-defueling levels and MW-37-32 had steadily decreased towards pre-defueling levels over the past four quarters (including a greater magnitude decrease from Q2 2010 to the current (Q3 2010) quarter - see **Figure 7A**), it is expected that the Strontium activity in MW-37-40 will continue to decrease towards pre-defueling levels over the next few quarterly monitoring rounds.

**MW-50-42.** The Q2 2010 Tritium result, which slightly exceeded the I.L. at this sampling location, was immediately followed by a decrease in activity by nearly one order of magnitude in Q3 2010. Similar to MW-36-24<sup>35</sup>, it was concluded that the likely cause for this increase was the transient RWST/R.O. processing skid spill. It was therefore also expected that Tritium levels would decrease relatively quickly in this well, again as supported by the Q3 2010 data.

**MW-53-82.** After generally<sup>36</sup> stable levels for the previous 3.5 years, a peak in Tritium activity was observed at this location during the Q1 2010 sampling event. Tritium levels exceeding the I.L. by nearly a factor of two and were the highest observed since Q4 2006. The Tritium activity decreased in Q2 2010, but still exceeded the I.L. The Tritium activity in MW-53-82 continued to decrease (by a factor of over two) with the current, Q3 2010 result at a level below the I.L.. While MW-53 is not located in the groundwater flow path downgradient of the RWST/R.O. spill, the timing of this peak is consistent with this release. In addition, and more importantly, this location has previously been demonstrated to be “down-slope” of the RWST/R.O. spill along vadose zone flow paths, as demonstrated by the tracer testing conducted as part of the hydrogeologic site investigations (see Figure 7.2 of the Hydrogeologic Site Investigation Report, January 7, 2008). While it is noted that other monitoring locations in the vicinity of MW-53-82 did not exhibit peaks in Tritium activity during the Q1 2010 and Q2 2010 sampling events (e.g., the deeper, companion sampling interval (MW-53-120), the two sampling intervals in upgradient monitoring well MW-42 and the nearby U1-NCD monitoring location), these findings are also

---

<sup>33</sup> Additionally, the Tritium I.L. was previously exceeded at MW-36-24 in Q3 2009; but the Q4 2009 and Q1 2010 results showed a decreasing trend over that time period. Therefore, this I.L. exceedance is not likely related to the past exceedance.

<sup>34</sup> The spill involved a rented RWST/R.O. processing skid brought on-site by an outside contractor. As such, this equipment is not an in-place Unit 2 SSC and is no longer on site. This release was first detected during routine 80-10 sampling of MH-9. The Tritium levels were measured at ~85,000 pCi/L in this MH on January 14<sup>th</sup> and 15<sup>th</sup>, 2010, and then decreased to 4,650 pCi/L on January 19<sup>th</sup>. Typical Tritium levels prior and post-spill were ~1,500-4,000 pCi/L in MH-9. It is therefore likely that Tritiated water entered the subsurface through this storm drain pathway, as well as potentially through the upper portions of the MW-32 installation (see Q1 2010 Quarterly Report, 1/11/11).

<sup>35</sup> It is noted that MW-36-24 and MW-50-42 are similarly located proximate to the upgradient (eastern) discharge canal wall, and are likely at least somewhat connected along preferential flow paths associated with the canal wall construction (e.g., blast-fractured bedrock and backfilling with permeable soils (Unit 2)). As such, it is not surprising that these two sampling locations have shown remarkably similar Tritium trends over the past 2.5 years

<sup>36</sup> It is noted that a clear peak in Tritium activity in this interval was measured in Q1 2009. This peak was attributed to a transient release from the Unit 1 distillation tank valves, which subsequently has appeared to have dissipated through the groundwater flow system.

## Section 3.0 Data Evaluation

---

consistent with the tracer test data as shown in the above referenced Figure 7.2. Therefore, it appears that the Tritium peak observed in MW-53-82 was a result of the Q4 2009 RWST/R.O. spill. Because this source was quickly terminated and Tritium is a non-sorbing radionuclide, the Tritium activity at this location will likely continue to decrease to pre-R.O. spill levels.

**MW-111.** Cesium was detected for the first time at this sampling location during Q2 2010. The Cesium activity was only slightly greater than the three times 1 sigma uncertainty level. Therefore, one possible explanation for the Cesium detection at MW-111 was a laboratory false positive. Both the Q3 2010 and the Post-Q3 2010 laboratory analytical results, which indicate non-detect Cesium activity at MW-111, are in agreement with this explanation.

**U3-4D.** The Q2 2010 Tritium result slightly exceeded the I.L. at this sampling location<sup>37</sup>. This I.L. exceedance was preceded (Q1 2010) by a noticeable increase above the baseline established in 2008 and 2009. The current, Q3 2010 result showed a return to 2008 and 2009 baseline levels. While it is not understood what caused this Tritium increase at U3-4D, it was possibly related to a delayed response to the Tritium increase noted in manhole A2 and MW-45-42 in Q2 2009.

### 3.4.3 Q3 2010 Boundary Investigation Levels

A comparison of the Q3 2010 analytical results for the On and Off-Site Boundary Wells to their respective I.L. values shows that the I.L.s were not met for any of the monitoring locations. Therefore, there was no requirement to further investigate radionuclide activity in these wells. However, monitoring installation MW-40 and MW-51 are being further evaluated on a routine basis, as discussed below.

**MW-40 and MW-51.** While there have been no historic I.L. exceedances at these two southern boundary locations, and all of the data from this quarter (Q3 2010) fall within previous ranges, these monitoring locations continue to be closely scrutinized on a routine basis given the sensitivity associated with the southern power block boundary. Even though it is recognized that the peak Tritium levels detected are low (less than 350 pCi/L) and near the lower limit of detection, there appears to be a general correlation in Tritium peaks (seasonal cyclical pattern) at multiple depth intervals in both of these monitoring installations (see **Figure H1** in **Appendix H**). This general correlation is evident in MW-51 this quarter (Q3 2010) as all of the depth intervals recorded an increase (similar magnitude) in Tritium activity since the previous (Q2 2010) sampling event. MW-40 also remained consistent with the trend, but it peaked earlier than MW-51, with most its intervals decreasing this quarter. An appropriate metric to evaluate whether or not these peaks are due to groundwater migration of Tritium from the power block area is the relative groundwater elevations between these locations and the power block areas where Tritium contamination exists. As discussed at length in the CSM sections of the Site Investigation Report, southern boundary groundwater elevations are well above those in the power block area. As such, groundwater, and thus Tritium in the groundwater, cannot migrate from the power block to the south; in fact, groundwater is migrating in the opposite direction. This conclusion was previously validated for nine quarters (between Q2 2007 and Q2 2009) through analyses of groundwater elevation contours (see **Figure 5** in the quarterly reports prior to Q3 2009). In addition, starting with the Q1 2009 Quarterly Report, **Figure 5A** is being generated to specifically compare high importance transducer readings to historic maximum and minimum readings. The objective of this analysis is to demonstrate that substantial changes to the on-site groundwater flow field have not taken place and that the CSM remains valid. Multiple sampling zones from both the MW-40 and MW-51 monitoring installations are included in this analysis. Based on these analyses, as well as the substantial body of data developed

---

<sup>37</sup> It should be noted that the Tritium I.L. is only 1,000 pCi/L at this sampling location, and the Q2 2010 analytical Tritium result was 1,070 pCi/L. Therefore, the Q2 2010 Tritium activity at U3-4D is still five times lower than the lowest isopleth drawn for the Unit 2 Tritium plume (5,000 – 10,000 pCi/L). It is noted that there is no Tritium plume associated with Unit 3.

## Section 3.0 Data Evaluation

over the last 5 years of investigation which underpin our CSM, we conclude, with a high degree of confidence that the low level peaks in the Tritium activities observed in these two monitoring installations are not due to groundwater migration from the power block area. This conclusion has continued to be validated each quarter. However, we do not have a definitive explanation for the observed peaks. Further investigation into other potential mechanisms, such as seasonal atmospheric Tritium washout and seasonal laboratory biases are ongoing.

### 3.4.4 Q3 2010 SSC Investigation Levels

For the SSC monitoring wells, a comparison of the Q3 2010 and Post-Q3 2010 analytical results to their respective I.L. values shows that the I.L.s were met at ten sampling locations this quarter. The following table summarizes the cases where the I.L.s were met, with these exceedances individually discussed below.

WELL ID	RADIONUCLIDE	RESULT (pCi/L)***	REANALYZED RESULT (pCi/L)	INVESTIGATION LEVEL (pCi/L)
MW-31-49 (Q3 2010 / Post Q3)	H3	54,600 / 104,000	NA*	42,776
MW-31-63 (Q3 2010 / Post Q3)	H3	61,700 & 66,900 / 46,500	NA*	39,857
MW-32-59 (Q3 2010 / Post Q3)	H3	65,400 / 74,400	NA*	34,230
MW-32-149 (Q3 2010 / Post Q3)	H3	3,810 & 2,600 / 2,120	NA*	1,000
MW-32-173 (Q3 2010 / Post Q3)	H3	2,470 & 2,190 / 1,980	NA*	1,496
MW-39-102	Sr-90	4.05	NA*	3.64
MW-41-40	H3	2,790	NA*	1,000
MW-46	H3	1,920	NA*	1,844
MW-50-42	Sr-90	8.43	NA*	8.20
MW-67-105	Sr-90	2.61	NA*	2.0

\* NA indicates that the sample was not reanalyzed.

\*\* ND indicates that the radionuclide was not detected greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

\*\*\* A radionuclide is positively detected when the result is greater than or equal to the MDC and 3 times the 1 sigma uncertainty.

**MW-31-49.** The Q3 2010 Tritium activity at MW-31-49 increased by a factor of three, which was the highest Tritium activity measured in this interval since the initiation of the LTMP. Following this I.L. exceedance, a second Q3 2010 sample was collected which showed a noticeable decrease (thirteen-fold) in activity to a level well below the Tritium I.L. However, the Post-Q3 2010 result was once again elevated above the I.L., and to a level twice that ever measured in this interval (including the previous Q3 2010 peak). These peaks in Tritium activity are possibly related to a somewhat delayed response to the transient RWST/R.O. skid surface spill<sup>38</sup> in Q4 2009<sup>39</sup>, as potentially mediated by Retention Mechanisms. This hypothesis is further supported by the response of MW-31-63, as discussed below. Assuming the R.O. skid spill is, in fact, the source, tritium activity in his well should relatively quickly return to pre-release levels given this spill was terminated and Tritium is a non-sorbing radionuclide (see further discussion below and in **Section 3.4.5**).

However, it has also been observed that these two recent Tritium peaks, as well as the previous peak in Q4 2009, appear to closely follow noticeable increases in flow into the Leak Collection

<sup>38</sup> The spill involved a rented RWST/R.O. processing skid brought on-site by an outside contractor. As such, this equipment is not an in-place Unit 2 SSC and is no longer on site. This release was first detected during routine 80-10 sampling of MH-9. The Tritium levels were measured at ~85,000 pCi/L in this MH on January 14<sup>th</sup> and 15<sup>th</sup>, 2010, and then decreased to 4,650 pCi/L on January 19<sup>th</sup>. Typical Tritium levels prior and post-spill were ~1,500-4,000 pCi/L in MH-9. It is therefore likely that Tritiated water entered the subsurface through this storm drain pathway, as well as potentially through the upper portions of the MW-32 installation (see Q1 2010 Quarterly Report, 1/11/11).

<sup>39</sup> Based on forensic research conducted by Entergy, it appears that the date of the spill was November 21, 2009.

## Section 3.0 Data Evaluation

---

Device (LCD)<sup>40</sup>, and also coincide with a ten-fold increase in the tritium level in MH-5 VCVD<sup>41</sup> (see **Figure 6B**). These temporal correlations lead to consideration of a potential link between LCD flow and peaks in groundwater tritium activity<sup>42</sup>. Because the flow rate into the LCD has decreased back to baseline levels (typically less than 20 ml/day after 10/4/2010), the Tritium activity in MW-31-49 is also expected to decrease, if there is a link as contemplated above. This location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring rounds to better understand the underlying cause of the recent peaks in Tritium activity.

**MW-31-63.** The three 2010 third quarter data points define a new tritium peak at this location; the Q3 result is increasing toward the peak from lower values measured in Q2 and post-Q2 2010, the first post-Q3 result is at the peak, with the second post-Q3 sample showing a decrease. This third quarter peak is nearly as high as the previous peak observed in the first quarter (post-Q1 2010 sample), which was the highest measured Tritium activity in this interval since the initiation of the LTMP. The first of these two recent peaks was previously attributed to the localized, transient RWST/R.O. processing skid surface spill in Q4 2009. The second peak is hypothesized to be a continued, delayed response to this spill (similar to MW-31-49 above), with the delay due to release of additional Tritium via the Retention Mechanisms. Given that the apparent source of this peak has been terminated and Tritium is a non-sorbing radionuclide, Tritium levels should relatively quickly returned to pre-release levels in MW-31-63 once the residual impact of the RWST/R.O. spill has flushed through the groundwater system, as mediated through the Retention Mechanisms (see further discussion below and in **Section 3.4.5**).

In this regard, it is noted that peaks in Tritium level, likely related to mobilization of historically stored Tritium<sup>43</sup>, have been noted in MW-31-63 since the Q1 2009 sampling event, with somewhat less, but still noticeable variability evident all the way back to the beginning of monitoring. This behavior has also been noted in other sampling depths at this location as well as at proximate locations MW-32 and MW-30, particularly at shallower depth intervals<sup>44</sup>. Therefore, while the post-Q1 2010 peak has been associated with the transient RWST/R.O. skid spill, which had been terminated prior to the second Tritium peak observed in the Post-Q3 2010 samples, this subsequent peak is still likely due to the spill through R.O. skid spill replenishment of the Retention Mechanisms, thus resulting in further releases from these Retention Mechanisms into the groundwater flow regime (i.e., second peak). Therefore, future Tritium increases at this sampling location due to the transient RWST/R.O. processing skid spill are still likely.

However, as discussed above for MW-31-49, it is also possible that while the initial post-Q1 2010 peak at this location was due to the R.O. skid spill, the subsequent Post-Q3 2010 peak could potentially be related to the increased flow observed in the LCD. Given the uncertainty,

---

<sup>40</sup> Recent and ongoing investigations indicate that the increased LCD flow could potentially be related to particularly high SFP levels associated with dry cask work. Procedures have therefore been put in place to better control pool levels. It is also noted that all flow into the LCD is captured, measured and discharged as a monitored release.

<sup>41</sup> While this is the highest Tritium level measured at this location since monitoring began, it is noted that the increased Tritium in this drain is captured and routed to the discharge canal as a monitored release.

<sup>42</sup> While the data trends appear to correlate on a temporal basis, it is noted that simple correlation does not demonstrate causation.

<sup>43</sup> As discussed in the January 7, 2008 Hydrogeologic Site Investigation Report, it has been concluded that portions of the Tritium released prior to Energy's last remediation interdiction (rectifying the Transfer Canal liner weld imperfection in December 2007 - the final identified leak) have been stored in the subsurface (Retention Mechanism(s)).

<sup>44</sup> As discussed in previous quarterly reports, the historic variability in Tritium activity measured in MW-30, 31 and 32 has typically been attributed to the mobilization of Tritium stored in the shallow bedrock and/or within anthropogenic structural features. This storage/Retention Mechanism(s) was confirmed during tracer testing as described in the Hydrogeologic Site Investigation Report prepared by GZA, dated January 7, 2008, and as further supported by more recent tracer data discussed in the Q1 2009 LTM Report. Therefore, while the storage/Retention Mechanism(s) clearly contribute to the observed Tritium variability, it is equally clear that some of this variability is attributable to localized transient release events.



## Section 3.0 Data Evaluation

---

this potential relationship will be further evaluated based on the additional data obtained during the upcoming quarterly monitoring rounds.

**MW-32-59.** Similar to the Q1 2010 through Post-Q2 2010 samples<sup>45</sup>, the initial Q3 2010 Tritium result at this sampling location exceeded the Tritium I.L. However, a noticeable decrease in Tritium activity is observed from the Post-Q2 result to this initial Q3 2010 sample, and the initial Q3 2010 result represented the lowest activity in MW-32-59 since the transient R.O. processing skid surface spill. A second Q3 2010 sample showed another noticeable decrease to a Tritium activity well below the I.L. in MW-32-59. However, a subsequent Tritium peak was observed in Post-Q3 2010, with the Tritium activity back above the I.L. and slightly above the initial Q3 2010 result. Similar to the MW-31-49 Tritium I.L. exceedances, this recent Tritium peak is likely attributable to the transient surface spill which occurred in Q4 2009 during RWST/R.O. processing skid operations. In addition to entering the subsurface through the storm drain system, this spill also entered the MW-32 well vault<sup>46</sup>, and may have penetrated the well casings, thus potentially explaining the particularly high Tritium activities observed in this shallowest interval in MW-32. Because the surface spill was transient in nature, as concluded, in part, from the MH-9 data, it is expected that the Tritium activity should again quickly decrease below the I.L. at this location. However, this expected decrease could be masked by additional future contributions of Tritium from the storage/Retention Mechanism(s), as discussed more fully above for MW-31-63 and possibly seen in the Post-Q3 2010 result.

Inspection of **Figure 6B** indicates that this recent Post-Q3 2010 Tritium peak could also possibly be attributed to the increase leakage observed in the Unit 2 LCD. Prior to the Post-Q3 2010 peak, the previous two sampling results indicated a noticeable decrease in Tritium at this location, which was expected due to the transient source, the chemical nature/transport behavior of Tritium, and the rapid decrease in Tritium activity observed in MH-9. The noticeable decrease at this sampling interval (MW-32-59) occurred prior to the increased leakage measured in the U2 LCD. However, the Post-Q3 2010 sample was collected after the increased leakage was observed, and therefore, could be possibly attributed to the recent conditions observed at the U2 LCD. As such, this location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

**MW-32-149.** The Q1 2010 through Post-Q2 2010 results at this location showed an increase in Tritium activity to nearly ten times the I.L. in the Post-Q2 2010 sample<sup>47</sup>. The current, Q3 2010 and Post-Q3 2010 samples all exceeded the Tritium I.L. at this location, but the Tritium activity noticeably decreased by a factor of greater than four at MW-32-149 during these current sampling events. Similar to the other MW-31 and MW-32 exceedances discussed above and below, this Tritium peak has also been attributed to the transient surface spill which occurred in Q4 2009 during RWST/R.O. processing skid operations. The quick response of this deep sampling interval to the Tritium surface release provides further evidence that the spill may have penetrated the well casings and entered the subsurface immediately proximate to the sampling installation. This conclusion is based on the previously observed behavior of this sampling interval, which had historically exhibited a relatively uniformly decreasing trend for the last three

---

<sup>45</sup> The Post-Q2 2010 result was the highest Tritium activity measured at this location (in all depth intervals) since the initiation of the LTMP, and exceeded the I.L. by a factor of nearly five.

<sup>46</sup> An initial sample was taken of the water remaining in the MW-32 vault on 2/1/2010. This water exhibited a Tritium activity of 390,000 pCi/L. Subsequent sampling of this water in May 2010 measured residual Tritium levels of ~65,000 pCi/L prior to the water being fully removed from the vault. It is further noted that the water in the vault contained other radionuclides in addition to Tritium. These included Co-60, Sb-125, Cs-134, Cs-137, etc. Therefore, the Q1 2010 groundwater data from wells proximate to, and downgradient of, the MH-9 and MW-32 vault release points were evaluated for detections of these radionuclides, none were found. However, Cs-137 was detected at MW-111 in Q2 2010. While this well is located downgradient of MW-32, no other wells showed detections of Cs-137, or the other radionuclides discussed above, in Q2 2010. Cs-137 at MW-111 and downgradient of MW-111 will be closely monitored in the upcoming quarterly reports.

<sup>47</sup> Only the first sample collected at this location (1/19/2007) showed a higher Tritium activity (10,500 pCi/L) than the Post-Q2 2010 sample results (9,760 pCi/L).

## Section 3.0 Data Evaluation

---

years, absent the peaks observed in shallower intervals<sup>48</sup>. Because the probable source has been terminated, we anticipate that the Tritium activity should continue to decrease at this location. However, as discussed above for MW-32-59, the future behavior of this sampling interval is in question due to possible contributions from the storage/Retention Mechanism(s) and will therefore be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

**MW-32-173.** Both the Q2 2010 and Post-Q2 2010 Tritium results exceeded the I.L. at this sampling location following the initial increase in Tritium activity during the Q1 2010 sampling event to a level near the I.L. Similar to MW-32-149, the Tritium activity steadily decreased over the current (Q3 2010 and Post-Q3 2010) sampling period; however, a slightly delayed response is observed as the activity slightly increased between Post-Q2 2010 to the initial Q3 2010 result. The activity still remains above the Tritium I.L. at this location. Similar to the other MW-31 and MW-32 exceedances discussed above, this overall increase in Tritium levels over the past three quarters has also been attributed to the transient surface spill which occurred in Q4 2009 during RWST/R.O. processing skid operations. The delayed response, compared to MW-32-59 and MW-32-149, and the shallower slope to the increasing trend at this sampling depth provide evidence that this depth interval may be responding to vertically downward migration from above. This conclusion is supported by both the four-fold higher activities measured in intervals immediately above this point, as well as the strong vertically downward gradients exhibited by the bedrock formation at this location. As discussed above, the Tritium activity at this depth interval should continue to decrease as the Tritium activity above decreases (given the transient nature of the spill), but is likely to decrease more slowly<sup>49</sup>. It is also noted that the expected decrease could be masked by future contributions of Tritium from the storage/Retention Mechanism(s), as discussed more fully above for MW-31-63. As such, this location will therefore be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

**MW-39-102.** The Q3 2010 Strontium activity at this sampling location slightly exceeded the I.L. and represents the highest Strontium activity measured at MW-39-102 since the initiation of the LTMP. Similarly, the sampling interval directly below this location (MW-39-124) and the uppermost sampling interval (MW-39-67) also showed increases in Strontium during Q3 2010. As discussed in the Hydrogeologic Site Investigation Report prepared by GZA, dated January 7, 2008, MW-39 is located near the Legacy IP1 Storm Drain piping, which historically carried water collected in the Unit 1 SFDS. Previous testing along these pipes revealed that numerous sections were compromised and leaking; therefore, the SFDS discharge was rerouted in 1994 after detecting Strontium contamination in the effluent of the SFDS. As such, no active source of contamination was present in the Legacy piping after 1994, but several Strontium peaks were observed in multiple MW-39 sampling intervals since the initiation of the LTMP. Therefore, releases from storage/Retention Mechanism(s) and/or the sorptive properties of Strontium (desorbs back into groundwater) possibly contributed to these previous peaks and this current I.L. exceedance in MW-39-102. It is also noted that in addition to terminating the Strontium contamination in the Legacy piping, the ultimate source (Unit 1 SFPs) has also been terminated during the defueling and pool sealing operations in 2008. Therefore, the current Strontium peak in MW-39-102 will likely be transient and quickly return to lower levels at this location. Due to this Q3 2010 peak in MW-39-102, as well as Strontium increases in MW-39-67 and MW-39-124, this location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

---

<sup>48</sup> It is also noted that the sampling interval immediately above this interval, MW-32-85, did not exhibit a Tritium peak in Q1 2010; however, the Tritium activity increased during Q2 2010 through Post-Q3-2010 to levels slightly below the Tritium I.L.

<sup>49</sup> The current (Q3 2010 and Post-Q3 2010) sampling period results support this premise, as the Tritium activity decreased by ~1,700 pCi/L in MW-32-149 and only ~500 pCi/L in MW-32-173. Similarly, the Tritium activity in MW-32-149 has decreased by ~7,600 pCi/L since Post-Q2 2010, while MW-32-173 has only seen a ~350 pCi/L decrease over that time period.

## Section 3.0 Data Evaluation

---

**MW-41-40.** The Q3 2010 Tritium activity exceeded the I.L. by nearly a factor of three at this sampling location. A noticeable increase in Tritium activity (~60,000 pCi/L) was also concurrently observed in manhole A2 during routine 80-10 Effluents Program sampling (7/7/2010 sample date). Similarly, an increase in Tritium activity was also observed in a downstream manhole, A4, of this storm drain system. MW-41 is located directly adjacent to this storm drain system, between manholes A2 and A4. Therefore, this Q3 2010 Tritium increase in MW-41-40 is likely related to the increases observed in manholes A2 and A4. Rapid decreases in Tritium activity were observed in subsequent samples collected from these manholes (<1 week); therefore, this current Tritium peak would be expected to be transient in nature based on this information. However, an additional Tritium peak was also previously observed in manhole A2<sup>50</sup> in Q2 2009, and other potential similar, but undetected increases are certainly possible given the likely release mechanism. While investigation into the source of the peaks in the drain system, and thus this monitoring well, is still ongoing, all indications are that they are associated with higher levels of washout entering the Fuel Storage Building (FSB) roof drain leading directly into A2 when the vent fan is not operating; during specific climatic conditions, SFP evaporation can condense on the roof, and be transported into the storm drain system via rain water. Thus, this location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

**MW-46.** The Q3 2010 Tritium activity at this sampling location exceeded the Tritium I.L. by over a factor of two. While the exact cause of this increase in Tritium activity is not fully clear, it appears that, like upgradient well MW-41-40, it is a groundwater response to the Tritium peak observed in manhole A2, as discussed above. Similar to A2, no other radionuclides were detected at MW-46 during the Q3 2010 monitoring event. Because the Tritium activity in manhole A2 (and A4) rapidly decreased, this current Tritium peak observed in MW-46 should also be transient, with similar reasoning and cautions as discussed above for MW-41-40. Therefore, this location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

**MW-50-42.** The Strontium activity for Q3 2010 slightly exceeded the I.L. for this sampling interval. A slightly elevated Strontium activity has been observed at MW-50-42 since Q3 2009, which has been attributed to a delayed response to the increase in water levels during defueling operation in the Unit 1 SFPs (see MW-50 graph on **Figure 7A**). Prior to this current peak, the Strontium activity exhibited a decreasing trend from Q4 2009 to Q2 2010; thus the Q3 2010 result could indicate a contribution of Strontium from the storage/Retention Mechanism(s). However, it is also noted that these elevated levels are still significantly lower than the Strontium levels in the interval below (MW-50-66), which are exhibiting a substantial downward trend. Because the probable source is terminated, it is expected that the Strontium activity in MW-50-42 will again decrease towards pre-defueling levels over the next few quarters. The eventual decrease to pre-fueling levels might extend over multiple quarterly monitoring events due to the sorptive behavior of this radionuclide and the Retention Mechanism(s) discussed previously. Therefore, this location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

**MW-67-105.** The Strontium result for Q3 2010 represented the historical maximum Strontium activity measured at this sampling interval since the initiation of the LTMP and exceeded the I.L. Furthermore, this current peak was preceded by a noticeable increase in Strontium activity during the previous (Q2 2010) monitoring event. However, it is also noted that these relatively elevated levels are still significantly lower than the Strontium levels in the interval above (MW-67-39), which are exhibiting a substantial downward trend. Prior to Q2 2010, relatively low and

---

<sup>50</sup> A concurrent peak in Tritium activity and I.L. exceedance was also noted in the uppermost sampling interval of MW-45 (MW-45-42) during Q2 2009. Similar to the rapid decrease of Tritium activity noted in manhole A2, the Tritium activity in MW-45-42 quickly decreased to levels below the I.L. during the following, Q3 2009, monitoring round.

## Section 3.0 Data Evaluation

---

stable Strontium levels were observed at MW-67-105 since the first sample was collected in August 2007. Because this riverfront monitoring location is downgradient of Unit 1, this current peak is likely a response to the Unit 1 SFP defueling operation, as the water containing higher Strontium activity has migrated farther downgradient. Because the probable source has been terminated, the Strontium activity is expected to eventually return to the historical, low levels seen from August 2007 through Q1 2010 at this sampling interval as the perturbation passes through the system. This location will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring round.

**MH-5 VCFD, B-1 and B-6.** The Unit 2 foundation drains which discharge into MH-5 VCFD, along with similar drains for Unit 3 which discharge into Manholes B-1 and B-6, form an integral part of the early leak detection monitoring network.

The Q3-2010 result for MH-5 VCFD shows a clear increase in Tritium activity (approximately by an order of magnitude) when compared to the previous base line sampling results (including the previous sample from Q2 2010); however, the Post-Q3 2010 sampling data from only 10 days later, show the Tritium activity in MH-5 had already returned to the previous baseline levels (see **Figure 6B**). The remaining radionuclides were all non-detect during both the Q3 2010 and the Post-Q3 2010 sampling events at MH-5.

The Q3 2010 results at Unit 3 indicate a noticeable increase in Tritium activity in B-1 to the historical maximum activity at this manhole (approximately one order of magnitude greater than previous results). This peak is consistent with the transient increase in Tritium activity observed in Manhole A2 during the current (Q3 2010) quarter. This increase in A2 Tritium levels is believed to be due to condensation of SFP evaporation on the roof when the vent fan is not operating, which then enters the building roof drain leading directly into A2 during rainfall events, as is currently still being verified. Cesium also increased by a factor of approximately two at B-1 during Q3 2010, as compared to the previous sampling result (Q2 2010). These Cesium levels are well below the 80-10 Effluents Program reporting limits, and are believed to be associated with contaminated Unit 1 backfill in the vicinity of the Unit 3 VC Building.

All radionuclides (including Tritium) were non-detect at B-6 during the Q3 2010 sampling event.

**Leak Collection Device (LCD).** A clear increase in the volume of water collected by the Unit 2 LCD was noted during the current (Q3 2010) quarter, beginning on July 5, 2010. The flow rate averaged approximately 1.5 L/day over the quarter<sup>51</sup>. Investigations indicated that the increased flow appeared correlated with atypically elevated water levels in the fuel pool as associated with dry cask work. Limiting such increases in pool water elevation resulted in a marked decrease in the LCD flow rate, at the very beginning of quarter 4, back to levels generally consistent with the baseline of less than approximately 0.02 L/day. Based on these observations, a new figure (**Figure 6B**) has been included for the first time in this, Q3 2010, quarterly report which visually presents both the historical Tritium data and the U2 LCD data for the sampling intervals located within the Unit 2 Tritium plume boundaries. Potential correlations between the Q3 increased LCD flow rate and proximate monitoring intervals, including MH-5 VCFD, are discussed above under monitoring interval MW-31-49 and below in **Section 3.4.5**.

**U1 NCD AND U1-SFDS.** Sampling of the Unit 1 North Curtain Drain (U1-NCD) and the Unit 1 Sphere Foundation Drain Sump (U1-SFDS) are currently included as part of the Long Term Monitoring Program. These drains have been documented to capture a large proportion of the Strontium leakage from the Unit 1 SFPs, and continue to collect groundwater containing Strontium and Cesium and direct it to treatment. These drains have also historically been

---

<sup>51</sup> The LCD collected approximately 50 liters of water during the July to September 2010 time frame, which is greater than the total volume of water collected during the previous 3 year period (April 2007 through June 2010). In this regard, however, it is noted that all of the water collected by the LCD is fully contained and does not enter the groundwater regime.

## Section 3.0 Data Evaluation

---

assumed to collect some groundwater contaminated with Tritium from the Unit 2 SFP. This conclusion was validated by the tracer test conducted as part of the hydrogeologic site investigation (see the Hydrogeologic Site Investigation Report prepared by GZA, dated January 7, 2008). The limited amount of quarterly sampling data, as well as the impact of the Unit 1 defueling operations, render the setting of I.L.s for these monitoring points currently premature. However, visual inspection of the existing data was performed and relatively stable Tritium levels were exhibited by the Q1 2010 through Q3 2010 U1-SFDS data, while a noticeable increase in Tritium levels in U1-NCD is evident over this time frame, particularly in Q3 2010<sup>52</sup>. Therefore, the Tritium results for this drain will be specifically evaluated further with the additional data acquired during the upcoming quarterly monitoring rounds. Strontium data from these drains continued to show relatively stable (U1-NCD) and slightly increasing (U1-SFDS) trends. Both drains have generally reached and decreased to pre-defueling Strontium levels, as summarized on **Figure 7A**.

### 3.4.5 Conclusions - Boundary and SSC Leak Detection Monitoring

Recognizing that measured activities in the Off-Site and On-Site Boundary Wells have remained below I.L. levels, this overall data set continues to demonstrate that radionuclides are migrating toward the Hudson River to the West, and are not migrating off of the property to the North, East or South, as expected given the measured groundwater flow directions from the property periphery toward the power block area.

Given the analyses discussed above, there is also no compelling reason to believe that any new unidentified, leaks have developed<sup>53</sup> in the SSCs monitored relative to Unit 2 or 3. As discussed in Section 3.4.4 above, the increased Q3 Tritium activity in manholes A2 and A4 is, in all probability, due to condensation of SFP evaporation on the building roof when the vent fan is not operating, which then enters the building roof drain leading directly into A2 during rainfall events; Entergy is in the process of final verification of this hypothesis. It is further believed that this condensation is also the underlying cause of the Tritium I.L. exceedances observed in both nearby and downgradient sampling locations, MW-41-40, and MW-46 and B-1, respectively. Finally, it is noted that the tritiated water vapor evaporating from the SFP is a permitted release<sup>54</sup> and is accounted for as such in the dose computations. This same Tritium is therefore “double counted” because it is again included in the storm drain and groundwater portions of the dose computations.

Additionally, as discussed in the Q1 2010 Quarterly Monitoring Report, a peak in Tritium activity was measured in MH-9 during routine 80-10 Effluents Program sampling. The Q1 2010 sample from the upper-most interval of MW-32 (MW-32-59) also exceeded its I.L. with the highest Tritium activity measured since the initiation of the LTMP. After further investigation by IPEC, it appears that these Tritium increases originated from a Q4 2009 localized, transient surface spill just outside the Unit 2 FSB. The spill involved a rented RWST/R.O. processing skid brought on-site by an outside contractor<sup>55</sup>; the temporary leakage likely emanated from connection hoses during or just after the filtration process. It appears that this transient release entered both MH-9 and the well vault for MW-32 (which employs a drain emptying into MH-9), and may have also penetrated the MW-32 well casings. Both the storm drains and the well vault likely provided pathways for radionuclides to enter the subsurface. The Q2 2010 and Post-Q2 2010 data

---

<sup>52</sup> The Q3 2010 Tritium result in U1-NCD increased by nearly a factor of three and is the highest Tritium activity measured in this drain to date.

<sup>53</sup> However, as discussed further below, it is possible that a small leak exists and remains undetected in the Unit 2 SFP. Given the recent data from MH-5 VCFD and the LCD, additional investigations have been initiated.

<sup>54</sup> It is noted that the permitted release is through the Plant Vent located atop the VC building. Analyses were conducted to account for this release to the FSB roof in the dose computations.

<sup>55</sup> As such, this unit is not an in-place, plant SSC, and is no longer on site.

## Section 3.0 Data Evaluation

---

showed further I.L. exceedances both at deeper intervals (MW-32-173) and farther down gradient (MW-36-24 and MW-50-42), as would be expected as the spill worked its way through the groundwater flow regime. These additional Tritium exceedances were also attributed to this transient R.O. skid surface spill. The Q3 2010 and Post-Q3 2010 data indicate that the downgradient Tritium activities in MW-36-24 and MW-50-42 have both quickly returned below the I.L.; however, the Tritium levels in multiple “near source” sampling intervals (MW-31-49, MW-31-63, MW-32-59, MW-32-149, and MW-32-173) still exceed the Tritium I.L. Based on the above analysis, it is clear that a previously unidentified transient spill has once again successfully been identified by the LTMP.

Finally, increased leakage measured in the Unit 2 Leak Collection Device (LCD) from July 2010 to October 2010 appears attributable to raised pool levels within the U2 SFP during various dry cask fuel transfer procedures. While all the flow into the LCD is captured and released through monitored pathways, the recent Tritium peaks seen in MW-31-49, MW-32-59 and MH-5 VCFD appear to be potentially correlated, on a temporal basis, with this increased LCD flow rate. Based on the data from the end of Quarter 3 / beginning of Quarter 4, the flow into the LCD has decreased back to baseline levels of less than 0.02 L/day. This decrease appears to be in response to the post-investigation limiting of pool elevation increases during dry cask work.

The U2 plume<sup>56</sup> is continuing to generally exhibit overall, long-term reductions in Tritium activity<sup>57</sup>. While Q2 2010 increases in Tritium activity were observed in multiple monitoring locations within the delineated U2 plume, these data were consistent with both the Q4 2009 transient RWST/R.O. processing skid surface spill and the overall historic variability observed in Tritium levels attributed to episodic releases of Tritium stored in the subsurface via natural and anthropogenic Retention Mechanisms<sup>58</sup>. This conclusion is further supported by the tracer data and other analyses<sup>59</sup> discussed in Section 3.6 of the Q1 2009 Long Term Monitoring Report. Furthermore, reductions in Tritium activity were seen in numerous Unit 2 monitoring locations during Q3 2010, and the total tritium activity returned to the previous trend, as seen in **Figure G-17**.

Relative to the Unit 1 Strontium data, increased leakage was anticipated during final fuel removal from Unit 1 SFPs. This leakage was readily detected as increased Strontium in the groundwater by the Long Term Monitoring Program. The initial near-pool and subsequent downgradient Strontium increases have been routinely monitored as summarized on **Figure 7A**. Currently, the near-pool and more downgradient monitoring locations have generally returned to pre-defueling Strontium levels, with outliers (such as MW-37-40<sup>60</sup>) expected to continue to show further decreases towards pre-defueling levels in the upcoming quarters. Additionally, the near-river monitoring locations (MW-67-39, MW-67-105, and MW-62-138) are currently exhibiting an increase in Strontium activity, as the perturbation migrates downgradient.

Overall, GZA believes that continued monitoring will further demonstrate decreasing long term trends in groundwater contaminant activities over time for both the Unit 1 and Unit 2 plumes

---

<sup>56</sup> It is noted that there is no Tritium plume associated with Unit 3.

<sup>57</sup> It is noted that an increase was observed in the total Tritium activity of the Unit 2 plume during Q2 2010, as elucidated in **Figure G-17**. This Tritium mass increase was attributed to the transient RO. skid surface spill, which was only expected to temporarily increase the Unit 2 Tritium mass. Accordingly, a reduction back to the previous trend has been observed in the Q3 2010 total plume activity.

<sup>58</sup> These Retention Mechanisms are discussed along with the CSM in the previously cited Hydrogeologic Site Investigation Report.

<sup>59</sup> These data and analyses further support a conclusion that the Unit 2 SFP had ceased leaking after the transfer canal “pin hole leak” was repaired in late 2007. However, given the more recent behavior observed in the Unit 2 collection device data (see Section 3.6 of the Q1 2009 Long Term Monitoring Report), additional investigations/data evaluations are underway to further rule out potential Unit 2 SFP leak mechanisms.

<sup>60</sup> As discussed above, the 40 foot interval in the MW-37 monitoring installation is showing a delayed decrease in Strontium levels as compared to the depth intervals above and below. This response time lag is likely a result of the lower hydraulic conductivity (by two to three orders of magnitude) of the bedrock accessed by this depth interval.

## Section 3.0 Data Evaluation

---

given the source interdictions completed by Entergy. However, ultimate confirmation of these conclusions will require monitoring over a number of years to demonstrate continued depletion of Tritium and Strontium from the Retention Mechanisms originally sourced by: (1) historic Unit 2 SFP Tritium leakage; and (2) the historic and more recent Strontium leakage due to Unit 1 defueling, as well as impacts associated with a number of localized, transient release events. It is further noted that quantification of these overall radionuclide reductions will require that ranges in seasonal variation be adequately reflected in the monitoring data and any further additions of radionuclides to the Retention Mechanisms, such as through the transient releases discussed above, be dissipated from the geohydrologic flow regime.

Given the above cited constraints, it is premature to begin recalibrating the I.L.s, which were originally established at the beginning of the LTMP in 2007. Since inception of this program, it has been observed that I.L.s have been routinely exceeded in a number of cases where subsequent data have demonstrated that no new leaks have occurred. The majority of these cases occur where the radionuclide levels are generally low and/or near their detection limits. It appears that data variability, likely due to seasonal precipitation influences and local variations in flow paths and/or other in-situ processes, is the primary cause of these false positives<sup>61</sup>, particularly pursuant to Tritium. Therefore, the basis upon which the I.L.s are computed needs to be re-evaluated in light of the long-term natural transient variability of the groundwater system in response to precipitation events, etc. Furthermore, while re-evaluation/re-setting of I.L.s is a clear goal, it is still premature given the lack of sufficient data. This is particularly true given the recent behavior in Strontium levels due to the Unit 1 defueling (see **Figure 7A**) and the transient Tritium releases discussed above and in the Q1 2009 Quarterly LTM Report. As such, the current I.L.s will remain in effect while a sufficient data base is acquired to allow better quantification of the natural (non-leak related) variability in the data.

Five critical conclusions can be drawn from the above summarized data and analyses:

1. The current CSM for the IPEC site provides a good basis for the design of the Long Term Monitoring Program;
2. The procedures and rationale used for selecting monitoring locations for leak detection have been further validated given the clear detection of the confirmed Unit 1 SFPs increased leakage during fuel removal, the transient Q1 2009 U1 FSB distillation tank valve leak (see Q4 2009 Quarterly LTM Report for further discussion), the surficial release of Tritium to Manhole A2 in Q2 2009 and Q3 2010, and the Q4 2009 RWST/R.O. processing skid surficial release to MH-9;
3. Increases in Strontium levels following a documented leak take longer to materialize in the groundwater than might otherwise be expected<sup>62</sup>;
4. Localized, transient Tritium spills have a pronounced short term impact on Unit 2 Tritium plume activity, with potential longer term impacts via Retention Mechanism(s); and
5. Even with the somewhat increased Tritium levels currently observed due to the RWST/R.O. skid transient surface spill, the amount of radionuclides being released through the groundwater pathway is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

---

<sup>61</sup> In this context, "false positive" does not refer to an error in the actual data value. Rather, it means that the I.L. exceedance in question did not result from a new release. While I.L.s are meant to be set at conservatively low values, and thus "false positives" should be expected, a corollary objective is to set I.L. values which keep the number of false positives low enough to eliminate development of complacency.

<sup>62</sup> Given the proximity of monitoring installations to documented release events, the delay in release arrival is likely due primarily to Strontium partitioning and the time required for leakage to traverse anthropogenic features.

## Section 3.0 Data Evaluation

---

### 3.5 Plume Natural Attenuation Monitoring

The fourth and final objective of the Long Term Monitoring Program is to evaluate if the groundwater plumes identified on-Site demonstrate overall reductions in total activity over time, as is consistent with the requirements of Monitored Natural Attenuation (MNA), the selected remediation for the IPEC Site<sup>63</sup>.

Given the likely ages of the SFP leaks identified and characterized during the hydrogeologic investigation, it is probable that the Unit 2 (Tritium) and Unit 1 (Strontium) plumes had reached steady state conditions prior to the beginning of the LTMP. Given that: (1) the identified leaks in the Unit 2 SFP have all been previously repaired (the last leak repaired in 2007) and; (2) the water in the Unit 1 West Pool underwent intensified demineralization (beginning in April 2006 with a reduction in Strontium levels of over 95 percent), one might expect that the plumes should have started to markedly attenuate toward zero with time. Both plumes have in fact generally shown significant levels of attenuation, when they are viewed in their entirety and past release events and expected seasonal variability in the sampling data are accounted for. However, the attenuation has not been as rapid as we originally anticipated during time frames subsequent to the source interdictions implemented by Entergy.

In the case of the Unit 2 Tritium plume, levels have dropped markedly from the highest levels measured during the two-year hydrogeologic investigation. However, the rate of Tritium decrease with time has decreased. This rate of reduction has been difficult to predict due to the impact of natural geologic and anthropogenic Retention Mechanisms. These subsurface features have trapped and stored Tritium released during historic Unit 2 SFP leaks, and are still likely releasing this Tritium to the groundwater flow regime in an episodic manner after the physical leaks have been terminated. This conclusion is consistent with the original CSM presented in the Hydrogeologic Site Investigation Report, as further supported by the tracer test data in that report as well as subsequent tracer data, as described in Section 3.6 of the Q1 2009 Quarterly Monitoring Report, dated July 2, 2010. In addition, trend identification is further complicated by impacts associated with localized transient releases (most recently, the RWST/R.O. processing skid surface spill). As described above, these transient spills have resulted in a clearly identified, increasing trend in Tritium activity in a number of wells proximate to, and downgradient of, these spills. As such, these increases do not appear to be indicative of a new leak in the Unit 2 SFP. Further discussion of this quarter's data pursuant to evaluation of the Unit 2 Tritium plume MNA is provided in **Section 3.5.1** below.

Relative to the Unit 1 Strontium plume, Strontium levels should drop much more slowly than Tritium levels. This is because, in addition to the Retention Mechanisms discussed above for Tritium (which also apply to Strontium), Strontium also undergoes partitioning whereby this radionuclide is adsorbed from the groundwater onto solid surfaces (both geologic and anthropogenic). When the input of Strontium to the groundwater is reduced (such as via the initial fuel pool demineralization and subsequent decommissioning) the solid surfaces desorb the "stored" Strontium back into the groundwater, thus maintaining Strontium levels. Strontium partitioning is therefore expected to substantially slow plume attenuation. Despite partitioning effects, some plume attenuation was observed in response to pool demineralization prior to defueling, particularly proximate to the pool. However, defueling of Unit 1 resulted in a temporarily increase in the leakage rate of West Pool water into the formation. This was expected based on previous work on the Unit 1 SFPs, but was unavoidable given the requirement to raise the pool level for fuel rod removal<sup>64</sup>. The increased leakage rate had resulted in a noticeable increase in Strontium levels in the immediate vicinity, and downgradient

---

<sup>63</sup> The selection of MNA as the remediation for the Site is more fully discussed in the Hydrogeologic Site Investigation Report.

<sup>64</sup> As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.



## Section 3.0 Data Evaluation

---

of, the fuel pool. However, as more currently observed, the near-pool and more downgradient monitoring locations have generally returned to pre-defueling Strontium levels, with outliers expected to continue to show further decreases towards pre-defueling levels in the upcoming quarters, as discussed further in **Section 3.5.2** below.

### 3.5.1 Unit 2 Tritium Plume Attenuation

#### Qualitative Evaluation

From a qualitative perspective, a reduction in overall Tritium activity in the Unit 2 plume can be seen through a comparison of the Q3 2010 delineated plume boundary (**Figure 6A**) to those in early LTMP quarterly reports (2007 and 2008). Not only have Tritium levels within the plume generally shown an overall, long-term decreasing trend, but the reductions over the past few quarters, downgradient of the discharge canal, have become particularly evident in the delineated, shaded bounds of the plume. This quarter continues the trend where the shaded plume<sup>65</sup> no longer extends to the river as it did in previous quarters through 2008. Additionally, the rolling average Tritium activity in MW-111, indicative of the core of the plume, has shown an overall decrease by a factor of approximately two from Q1 2009 (70,150 pCi/L) to the current, Q3 2010, quarterly monitoring round (33,580 pCi/L). This trend over time has been summarized on **Figure 6A**, which is a compilation of the quarterly Tritium plume maps as well as that from the Investigation Report.

#### Mann-Kendall Quantitative Analysis

To more quantitatively evaluate MNA progress, a Mann-Kendall analysis, as referenced in USEPA Guidance for Data Quality Assessment – Practical Methods for Data Analysis,<sup>66</sup> was performed on the Tritium levels measured through Q3 2010 at monitoring locations associated with the IP2-SFP and downgradient Unit 2 Tritium plume<sup>67</sup>. Each of the vertical monitoring intervals at each monitoring installation location was analyzed separately. In general, only data collected after final completion of the multi-level installation<sup>68</sup> was used. However, there were a number of exceptions to this generalization where open borehole and/or borehole packer testing data were also used. These data were incorporated where possible given the importance of early time data (proximate to when documented leaks were still active). Additional, more detailed discussion relative to the basis for including these data is provided in Section 3.6 of the Q1 2009 Quarterly LTM Report.

---

<sup>65</sup> The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value, and provides a reasonable demarcation level for illustrating plume geometry and temporal variation. Although this value equates to one-quarter of the drinking water standard for Tritium, GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to represent three-dimensional contaminant data sets on two-dimensional maps.

<sup>66</sup> USEPA Guidance for Data Quality Assessment – Practical Methods for Data Analysis, EPA QA/G9, QA00 UDATE; EPA/600/R-96/084, July, 2000.

<sup>67</sup> The Mann-Kendall statistical technique was initially chosen because it is particularly well suited for data sets with a limited number of points. The method was subsequently retained because it is also a non-parametric analysis and therefore does not introduce bias by presupposing any particular shape for the trend curve. In addition, the method is robust with respect to outliers, which allows it to handle the variability inherent in the data set. Finally, the method tolerates non-uniform sampling frequencies. This is important because while the sampling frequency is typically quarterly, more frequent samples are proactively taken when a scheduled operation carries an increased risk of potential release, and also when something unexpected is observed that could indicate a new leak or spill.

<sup>68</sup> The majority of the boreholes were completed as multi-level installations. These multi-level completions were designed to segregate the borehole length into individual sampling zones with depth. The sampling zones were generally established to coincide with the more productive zones of the fractured bedrock and overburden (both natural soils and backfill). These zones were then isolated from each other with various types of seals placed in the open borehole. The objective of the seals is to prevent vertical flow through the borehole and thus establish the same conditions in the formation which existed prior to the drilling of the borehole. As such, the Tritium data is considered depth-discrete. It is noted that the multi-level installations at some monitoring locations were removed and replaced with upgraded systems, such as for the monitoring installation at MW-32.

## Section 3.0 Data Evaluation

---

Graphs showing the variation in Tritium concentration over time in the immediate vicinity of the Unit 2 SFP are presented as **Figures G-1, G-2 and G-3** in **Appendix G**, for MW-30, 31 and 32, respectively. Additional graphs are also presented in the appendix for the other monitoring locations downgradient of the Unit 2 SFP (see **Figures G-4 through G-14** for MW-33 through 37, 42<sup>69</sup>, 49, 50, 53<sup>69</sup>, 55 and 111) and downgradient<sup>30</sup>, river boundary wells (see **Figures G-15 and G-16** for MW-66 and 67, respectively). The Mann–Kendall analyses for the individual monitoring points are summarized on **Table G-1** in **Appendix G**. The table includes the results of the analysis for each depth interval (“well”) at each of the multi-level monitoring locations enumerated above. The table is color coded, with green shading designating wells showing a decreasing trend, yellow for no trend, and red for an increasing trend.

Comparison of **Table G-1** for Q3 2010 to that from Q2 2010 indicates that there have been no major changes since last quarter. Of the 32 non-river-boundary intervals included on the table for Q3 2010, approximately one-half (17) show a decreasing trend, which is the same as last quarter. Slightly less than one-half (4) of the 9 river boundary monitoring intervals show a decreasing trend, similar to last quarter. It is important to note that this group of “decreasing wells” includes all those located within the core of the plume with the highest Tritium activities (MW-30-69, MW-33 and MW-111). These high-activity wells better represent overall plume behavior because they encompass a high percentage of the total Tritium activity in the plume.

However, relative to the primary intent of the Mann-Kendal analyses for evaluation of plume attenuation after SFP leak termination, it is noted that the number of wells exhibiting a decreasing trend is decreasing (i.e., changing to a no-trend status). This issue is, in part, due to a shortcoming of the Mann Kendall analysis method, itself. This method only evaluates the number of increases relative to decreases, and does not weight the analysis relative to the magnitude of each change. Therefore, once a clearly decreasing trend, even of substantial magnitude, has reached a nearly horizontal asymptotic behavior, numerous insignificantly small positive and negative changes over time (such as due to sampling and hydrogeologic variability) can overwhelm the relatively short, early-time string of decreasing changes, thus resulting in a switch from a decreasing trend to a no-trend status. This is particularly true when a 95% confidence interval is applied. Of even greater import relative to the masking of SFP plume attenuation is the impact of localized, transient Tritium surface spills. These have been shown to result in increases in activity, which, while valid measures of plume activity, impair the ability of the trend analysis to serve as a measure of plume attenuation due to successful SFP leak termination, the intended purpose of this analysis. As a case in point, and as described in more detail for individual impacted wells below, a number of wells have changed from decreasing to no-trend and from no-trend to increasing trends this quarter (Q3 2010) in response to the RWST/R.O. transient surface spill<sup>70</sup>. While this transient spill was identified and described two quarters ago, the number of samples showing increased tritium levels has reached a point where these data have overwhelmed the previously decreasing trend which was reflective of the SFP leak terminations. Of the 11 non-river-boundary wells shaded in yellow (exhibiting “no-trend”), only one currently potentially provides a valid representation (as shaded) of Unit 2 plume behavior pursuant to the Unit 2 SFP (discussed at the end of this section). The shading

---

<sup>69</sup> MW-42 and MW-53 are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP. However, these two wells were included in the analyses due to the long-standing hypothesis that the Unit 2 SFP contributes Tritium to the Unit 1 groundwater flow regime via vadose zone transport (see the graphic representation in **Figure 6** herein and the discussion in the Hydrogeologic Site Investigation Report). It is noted that any decreasing Tritium trend in this area due to the termination of leaks from the Unit 2 SFP could be masked by increased leakage of Tritiated water from the Unit 1 SFPs up through the completion of defueling in November 2008, and then thereafter via the Retention Mechanism(s) and localized transient releases, as described above.

<sup>70</sup> Investigation of this type of spill typically results in numerous samples over a short period of time during the peak activity. Again, only the number of elevated points is considered and not the duration of the increased activity, which then results in a misleadingly prolonged deviation from the underlying SFP decreasing trend condition.

## Section 3.0 Data Evaluation

---

designation (in and of itself) for the others can no longer<sup>71</sup> be used to infer conclusions relative to overall plume trend as an indicator of Unit 2 SFP integrity based on this analysis, as follows:

- Three wells (MW-42-49, MW-42-78, and MW-53-82) are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP.<sup>72</sup> In addition, as discussed in **Section 3.4.2**, MW-53-82 appears to have been impacted during the Q2 2010 quarterly monitoring event by the more recent RWST/R.O. spill, as well as the prior U1 FSB valve leak.
- Inspection of the graph for MW-36-24 (**Figure G-7**) shows a rapid and large decrease in Tritium activity at early times in this overburden (discharge canal backfill) well (from >30,000 pCi/L to <3,000 pCi/L). This large decrease is followed by a number of small perturbations around a relatively flat trend. While it is visually clear that this well has shown a major decrease in Tritium levels since containment of the 2005 shrinkage crack leak, the Mann–Kendall analysis only evaluates the number of increases relative to decreases and does not weight the analysis relative to the magnitude of each change. As such, visual inspection demonstrates that this location actually exhibits an overall decreasing trend, even though the analysis results in a no-trend designation (yellow shading on table). However, it is also noted that the last few quarters have shown what appear to be short-term, small peaks in the Tritium activity in this well, as likely associated with the transient Q1 2009 release from the U1 FSB distillation valves, the Q4 2009 RWST/R.O spill and/or the recent increases noted in MW-31 and MW-32.
- Inspection of the graph for MW-50-42 (**Figure G-11**) shows a similar historical trend as exhibited by MW-36-24, as discussed above. As such, the same conclusion has been reached for this well.
- Inspection of the graph for MW-55-24 (**Figure G-13**) shows a similar historical trend<sup>73</sup> as exhibited by MW-36-24 and MW-50-42, as discussed above, although the initial decrease in Tritium activity at this sampling interval is not as substantial as the two previously discussed monitoring locations. As such, the same conclusion has been reached for this well.
- Inspection of the graph for MW-32-149 (**Figure G-3**) shows a relatively well behaved decreasing trend in Tritium activity, starting at the beginning of the LTMP and continuing all the way until Q1 2010. This is as would be expected in response to termination of all the identified SFP leaks. However, a distinctly increasing trend began thereafter, as correlated with the Q4 2009 transient RWST/R.O. processing skid surface spill. As such, the shift from a decreasing trend to a no-trend Mann-Kendall status appears to most probably reflect the RWST/R.O spill and not a new leak in the Unit 2 SFP.

---

<sup>71</sup> While the Mann Kendall has many advantages for trend analysis, particularly where the number of data points is limited, it suffers from an inability to account for the magnitude of each change, only assessing the number of positive changes relative to negative changes. This shortcoming was inconsequential at early-times when large decreases in Tritium activity were observed in response to Entergy's termination of all of the identified leaks in the Unit 2 SFP. However, now that many of the graphs of Tritium activity vs. time have nearly reached a horizontal asymptote, the accumulating number of small positive and negative changes is overwhelming the relatively short, early-time string of decreasing changes, thus resulting in a switch from a decreasing trend to a no-trend status. In addition, localized, transient Tritium surface spills have impaired the ability of the trend analysis to serve as a measure of plume attenuation as related to SFP leak termination, the intended purpose of this analysis.

<sup>72</sup> MW-42 and MW-53 are located downgradient of the Unit 1 SFPs, rather than the Unit 2 SFP. However, these two wells were included in the analyses due to the long-standing hypothesis that the Unit 2 SFP contributes Tritium to the Unit 1 groundwater flow regime via vadose zone transport (see the graphic representation in **Figure 6** herein and the discussion in the Hydrogeologic Site Investigation Report). It is noted that any decreasing Tritium trend in this area due to the termination of leaks from the Unit 2 SFP are more likely to be masked by increased leakage of Tritiated water from the Unit 1 SFPs up through the completion of defueling in November 2008, and then thereafter via the Retention Mechanism(s) and localized transient releases, as described above. This conclusion is based on their distance from The Unit 2 SFP and their proximity to the Unit 1 SFPs and the Unit 1 FSB distillation tank valve leak.

<sup>73</sup> It is noted that MW-55-24 exhibits a similar trend to MW-36-24, except at very early times where it does not show as large a drop in Tritium activities.

## Section 3.0 Data Evaluation

---

Because this transient source has been terminated, the MW-32-149 Tritium activity will likely continue to return to pre-spill levels, and it is anticipated that the Mann-Kendall analysis will eventually re-designate this well as “decreasing trend”, as it has been for all quarterly monitoring reports prior to Q2 2010.

- Inspection of the graph for MW-32-173 (**Figure G-3**) shows a clear, well behaved decreasing trend through Q4 2009<sup>74</sup>. Similar to MW-32-149 discussed above, the current switch to an increasing trend is in response to the Q4 2009 transient RWST/R.O. processing skid surface spill. However, visual inspection of the data indicates that the Tritium activity is again decreasing as would be expected given the transient nature of the spill. Therefore, it is anticipated that the Mann-Kendall analysis will eventually re-designate this well as “decreasing trend,” as it has been for all quarterly monitoring reports prior to Q3 2010.
- Inspection of the graph for MW-32-59 (**Figure G-3**) shows two major spikes, one just after the Unit 1 distillation tank valve leak<sup>75</sup> and a more prolonged peak just after the RWST/R.O. processing skid surface spill. As for MW-32-149 discussed above, the behavior of this well has been substantially impacted by the RWST/R.O. processing skid surface spill.
- Inspection of the graph for MW-55-54 (**Figure G-13**) shows a similar historical trend<sup>76</sup> as discussed above for MW-32-149. As such, the same conclusion has been reached for this well.

The one “no trend” well that currently may potentially still provide a valid representation of U2 SFP behavior<sup>77</sup> is the shallowest sampling port in monitoring location MW-31. Additionally, two of the four “increasing trend” non-river boundary monitoring intervals are also located in the MW-31 monitoring installation (MW-31-63 and MW-31-85). These three intervals in MW-31 have not been clearly shown to be impacted by surface spills, and may thus be representative of SFP behavior. The MW-31 location is actually not located downgradient of the Unit 2 SFP from a saturated groundwater flow standpoint. Rather, it is generally located up-gradient<sup>78</sup>. All three intervals in MW-31 have shown clear peaks in Tritium levels over the last seven quarters (Q1 2009 through Q3 2010) with somewhat less, but still noticeable variability evident all the way back to the beginning of monitoring. The current and historic variability in these data can be explained by either: 1) an ongoing small episodic (< 10L/day) leak in the Unit 2 SFP; 2) a “Retention Mechanism” in the saturated and unsaturated zones under the SFP that can retain substantial volumes of highly Tritiated water (e.g., historic SFP leakage) for substantial amounts

---

<sup>74</sup> In fact, when applying the Mann-Kendall analysis to MW-32-173's Tritium data through Q4 2009, it produces a “decreasing trend” status at the 99.9% level of significance. Typically, only a 95% level of significance is used to designate a “decreasing trend” in environmental data using the Mann Kendall analysis. As such, this monitoring interval, MW-32-173, only switched to a “no trend” status during the current (Q3 2010) quarterly monitoring period. Other intervals at this monitoring location that exhibited similar responses to the RWST/R.O. transient spill had already switched to “no trend” designations by the Mann-Kendall analysis in prior (Q1 and Q2 2010) quarterly monitoring periods.

<sup>75</sup> While this leak preceded the peak and appears temporally correlated, a migration mechanism from the leak area to this well has not been identified.

<sup>76</sup> While MW-55-54 exhibits a similar trend to MW-32-149, it is noted that there is a small, extended increase in Tritium activity over the middle of the graph, which is not seen in MW-32-149. This increase started prior to the documented localized, transient spills discussed above. As such, it is possible that this increase is associated with the coincident increase in Unit 2 SFP leak collection device flow rate during 2008 dry cask activities. This possible relationship is currently being investigated further.

<sup>77</sup> As described above, the ability of a number of monitoring intervals to provide SFP trend monitoring has been masked, at least temporarily, by the RWST/R.O. processing skid surface spill.

<sup>78</sup> While not downgradient of the SFP from a groundwater flow perspective, Tritium leakage from the SFP can still migrate to this location via vadose zone transport above the water table along dipping bedrock fractures. During the site investigation work, a tracer test was performed which clearly demonstrated that water released proximate to the SFP foundations (adjacent to MW-30) does migrate to the east past MW-31 prior to entering the water table, and then flows with the groundwater through this well and then to the river to the west. This vadose zone migration mechanism is discussed more fully in the Hydrogeologic Site Investigation Report.

## Section 3.0 Data Evaluation

---

of time<sup>79</sup>; 3) localized, transient releases<sup>80</sup> and/or 4) a combination of the above. While Tritium concentrations in the groundwater plume could be impacted by both an ongoing leak and the Retention Mechanisms cited above, tracer concentrations in the groundwater cannot be replenished by SFP leakage. As discussed in further detail in Section 3.6 of the Q1 2009 Quarterly Monitoring Report, the original and updated tracer data strongly support the existence of a Retention Mechanism. In addition, it would be expected that Tritium release from the Retention Mechanisms would be episodic, for example as associated with periods of increased infiltration from precipitation. Such episodic releases would be expected to result in the peaks in Tritium concentrations observed. However, it is also becoming increasingly evident that relatively recent localized, transient spills are also contributing to the observed peaks in Tritium activity in a number of monitoring intervals.

The third remaining interval reported as “increasing trend”, MW-32-85, (**Figure G-3**) had not previously exhibited an increasing trend. However, the Tritium activity has been steadily increasing after the RWST/R.O. processing skid surface spill. As discussed above for MW-32-149, the same conclusion has been reached for MW-32-85 relative to a projected eventual resumption of a decreasing-trend Mann-Kendall status given the transient nature of the underlying-cause RWST/R.O. processing skid surface spill.

The fourth and final interval reported as “increasing trend”, MW-30-84, is located immediately next to the SFP and generally downgradient of MW-31-63 and MW-31-85 (intervals with increasing trend). In agreement with the Mann-Kendall analysis yielding an increasing trend for MW-30-84, this interval does exhibit a distinctly increasing, sustained trend beginning in the late fall of 2008. The specific reason for this increase is not known, but it is worth noting that the Tritium activity in this interval is approximately an order of magnitude below that measured in upgradient monitoring intervals MW-31-63 and MW-31-85, both of which are exhibiting increasing trends. As such, the increasing trend in MW-30-84 could be a response to infiltration of this higher activity water over time. In addition, there are also peaks in the Tritium over time data for MW-30-84 which are consistent with the timing of the above discussed localized, transient surface spills. Finally, the beginning of the general increasing trend in Tritium activity in this well appears to predate the identified localized spills, and is coincident with the increase in Unit 2 SFP LCD flow rate during 2008 dry cask operations. This potential relationship is currently being investigated further.

Of the seven depth intervals in river boundary well MW-67, three show no trend and three exhibit a decreasing trend using the Mann-Kendall analysis (**Figure G-16**). This is the same distribution as last quarter, but with one additional decreasing trend interval relative to the previous quarter (Q1 2010)). It is critical to note that two of the three wells showing the decreasing trend are those with the highest Tritium activities (MW-67-39 and MW-67-105); activities up to four times those in the no trend wells<sup>81</sup>. In addition, the no trend wells all have maximum Tritium activities less than 1500 pCi/L. Finally, the only depth interval that shows an

---

<sup>79</sup> This hypothesized “Retention Mechanism” is supported by our understanding of the construction methods used for the IP2-SFP and adjacent structures, evaluations of contaminant concentration variability trends over short timeframes and precipitation events, as well as the original and subsequent tracer test results, as further described in Sections 7.0 and 8.0 of the Hydrologic Site Investigation Report and the Q1 2009 monitoring report.

<sup>80</sup> That is, any other leak or spill above the upgradient portions of the Unit 2 Tritium plume (such as the previous distillate tank valve leak first discussed in the Q1 2009 Quarterly Report and the more recent RWST/R.O. processing skid spill discussed in **Section 3.4** above). While relatively infrequent and transient, these spills of radionuclides into the subsurface clearly further complicate the analyses and evaluation of long term trends as used to verify the cessation of Unit 2 SFP leakage. The impact of these releases are also becoming increasingly difficult to separate from impacts associated with the storage /Retention Mechanism(s) to which these releases also contribute. To the extent possible, these transient releases have been accounted for in the previous discussions and analyses.

<sup>81</sup> It is also noted that all three monitoring intervals exhibiting decreasing trends are the shallowest sampling intervals within MW-67.

## Section 3.0 Data Evaluation

---

increasing trend (MW-67-340) generally has the lowest Tritium activities<sup>82</sup> of all 7 intervals; it is further noted that the maximum activity measured in this interval is well below 1,000 pCi/L. It is also important to recognize that MW-67 was installed and first sampled in late 2007, well after the majority of the Unit 2 Tritium activity reduction occurred (2005 through early 2007, as exhibited by the upgradient wells). Therefore, what may have been decreasing trends in these “no trend” wells, cannot be reconstructed with the available limited late-time data sets. It is currently GZA’s opinion that the no and increasing trend wells in MW-67 should continue to be monitored, but the data and trend analyses that they currently provide via the Mann-Kendall analysis method should be of no current concern. A similar analysis and conclusions apply to the two depth intervals in MW-66 (see **Figure G-15**).

Based on the evaluation summarized above, the Mann-Kendall analyses of the individual depth intervals within the groundwater monitoring installations located proximate to and downgradient of the Unit 2 SFP previously have overwhelmingly supported a conclusion that the Tritium plume has exhibited an overall decreasing trend with time since monitoring began. This conclusion was clear at early-times when large decreases in Tritium activity were observed in response to Entergy’s termination of all of the identified leaks in the Unit 2 SFP. However, now that many of the graphs of Tritium activity vs time have reached a horizontal asymptote, the accumulating number of small positive and negative changes is overwhelming the early-time string of decreasing changes, thus resulting in a switch from a decreasing trend to a no-trend status. Therefore, identification of another, more appropriate method is being investigated, particularly as the total LTMP data set becomes more robust with time. However, localized, transient Tritium spills have also impaired the ability of the trend analysis to serve as an appropriate measure of plume attenuation as related to SFP leak termination, the intended purpose of this analysis. As such, it is also important to recognize that the increases in Tritium activity measured in the monitoring wells have been readily explained by localized, transient surface spills which are unrelated to the Unit 2 SFP. As such, there is still currently no definitive evidence of new, unidentified leaks from the monitored Systems, Structures, or Components, including the Unit 2 SFP.

### Tritium Plume Total Activity Analysis

As discussed above, the individual well trend data, when viewed collectively, support a conclusion that the Tritium plume concentrations have generally been decreasing with time since monitoring began. Another method to analyze plume behavior is to compute the total Tritium activity in the plume at multiple snapshots over time. This procedure<sup>83</sup> was implemented for each quarterly LTMP sampling round from Q2 2007 to Q3 2010. In addition, the bounding Tritium concentrations from Figure 8.1 of the Hydrogeologic Site Investigation Report<sup>84</sup> have also been included as a starting point for the graph. These data are summarized as a histogram on **Figure G-17** in **Appendix G**.

As can be seen from the figure, the total Tritium activity in the plume downgradient of the Unit 2 SFP has shown a distinctly decreasing trend over time. After a noticeable increase in total Tritium mass last quarter (Q2 2010)<sup>85</sup>, the total Tritium activity noticeably decreased during the

---

<sup>82</sup> Monitoring intervals MW-67-323 and MW-67-340 have historically exhibited similar Tritium activities; however, the activity in MW-67-323 is typically slightly less than that in MW-67-340.

<sup>83</sup> The individual sampling point Tritium concentrations were multiplied by the groundwater volumes in representative zones (discretized over area and depth), as computed using soil and bedrock effective porosities developed from the pumping and tracer tests (see the Hydrogeologic Site Investigation Report for further information).

<sup>84</sup> Hydrogeologic Site Investigation Report, January 7, 2008, prepared by GZA GeoEnvironmental, Inc. on behalf of Enercon Services, Inc., for Entergy Nuclear Northeast, Indian Point Energy Center, 450 Broadway, Buchanan, NY 10511.

<sup>85</sup> Approximately 70% of the sampling intervals used in the total Unit 2 Tritium activity calculations recorded an increase in Tritium activity from Q1 2010 to Q2 2010. It should be noted that an increase in Tritium activity for sampling locations completed in soil (backfill) have greater impacts on the total Tritium mass calculations due to difference in overburden porosity vs. bedrock porosity.

## Section 3.0 Data Evaluation

---

current quarter (Q3 2010) and resumed the historical decreasing trend over time. Similar to the increase in Unit 2 I.L. exceedances, the overall activity increase during Q2 2010 appears to have been caused by the transient surface spill related to the RWST/R.O. processing skid operations. As such, the total Tritium activity is expected to continue its overall decreasing trend, similar to the current (Q3 2010) quarterly monitoring round, given the transient nature of this spill. Based on the Q3 2010 data, the total Tritium activity in the plume has decreased 45 percent since Q2 2007, and has decreased by 89 percent when compared to the bounding level Tritium concentrations. It is noted that the time/activity data appear to be approaching a non-zero horizontal asymptote<sup>86</sup>. While the general "first order" plume decay is what would be expected for a plume undergoing Monitored Natural Attenuation after source termination, a non-zero asymptote suggests a continued input of Tritium into the groundwater flow regime. The data currently available lead us to believe this continuing Tritium input is likely associated with the Retention Mechanism(s), the localized transient releases detected to date and/or potentially a small unidentified Unit 2 SFP leak, as described in this and earlier reports.

### **Conclusion- Unit 2 Tritium Plume MNA**

Based on the data and analyses provided above, our conclusion is that the Tritium plume associated with the historic Unit 2 SFP leaks is undergoing overall, long-term reductions in activity which are consistent with Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP, this Unit 2 Tritium plume satisfies the requirements for Monitored Natural Attenuation<sup>87</sup>. Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report.

Finally, it is important to recognize that even with the somewhat increased Tritium levels currently observed due to the RWST/R.O. skid transient surface spill, the amount of tritium being released through the groundwater pathway is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

### **3.5.2 Unit 1 Strontium Plume Attenuation**

Despite the effects of partitioning, as discussed above, the overall Strontium activity within the Unit 1 plume had generally shown some attenuation in response to the West Pool demineralization conducted by Entergy in preparation for defueling. This work began in 2006 and resulted in an approximately 98% reduction in Strontium in the West Pool (see **Figure 7A**: U1-NCD, U1-SFDS, MW-42, U1-CSS). However, the final defueling of the Unit 1 SFPs had resulted in a noticeable increase in Strontium levels proximate to the SFPs (U1-NCD, U1-SFDS, MW-42, and U1-CSS; all of which have shown large sustained decreases since mid 2009 to pre-defueling levels). Farther downgradient (MW-53, MW-55, MW-54, MW-57, MW-50, and MW-37), increases in the Strontium plume activities were also measured, but generally after a time lag as compared to wells more proximate to the SFPs. The majority of these more downgradient monitoring locations have most recently shown decreases approaching pre-defueling levels. The farthest downgradient, river boundary wells (MW-67 and MW-62) have

---

<sup>86</sup> One physical cause for a horizontal asymptote would include a persistent, unidentified leak still remaining in the Unit 2 SFP. With Tritium at approximately 30,000,000 pCi/L in the SFP, a leak directly from the pool of only approximately 10 L/day would be sufficient to provide the required Tritium input to the groundwater. To date, the available data do not appear to support the existence of such a leak. The rationale underlying this continued conclusion is discussed more fully in Section 3.6 of the Q1 2009 Quarterly Monitoring Report. However, this conclusion is continually reassessed on a quarterly basis as new data becomes available. In particular, this quarter's new LCD data as well as that for MH-5 VCFD have resulted in the initiation of additional investigations.

<sup>87</sup> It is noted that the previously clear attenuation of the Unit 2 tritium plume has been confounded by a number of localized, transient surface spills. Entergy is currently in the process of reviewing and addressing work practices which may have contributed to the occurrence of these spills.

## Section 3.0 Data Evaluation

---

possibly shown Strontium activity increases in the past few quarterly sampling events. This increase, followed by a longer term decrease, is as was predicted given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing the leakage rate from the SFPs prior to fully draining the pool<sup>88</sup>.

The data for Q3 2010 indicate that the overall Strontium levels continued to exhibit a general decrease and have now generally reached pre-defueling levels in the immediate vicinity of the pool (U1-NCD, MW-42, U1-SFDS, U1-CSS and MW-53). These monitoring locations would be expected to be the first to reflect the complete decommissioning of the SFPs given their location/function. Somewhat farther downgradient, the Q3 2010 data are consistent with the "tail" portion of the perturbation as the previous increase in U1-SFPs leakage works its way towards the river. This behavior is most evident at monitoring locations MW-37, MW-50<sup>89</sup>, MW-55 and MW-57<sup>90</sup> where, for the most part, the maximum Strontium levels were recorded in 2009 and have decreased over the past few quarters, approaching pre-defueling activities. MW-54, however, appeared to have already exhibited a Strontium peak in Q4 2008, and then decreased back to previous levels, even though this monitoring installation is relatively far downgradient. This behavior serves to again emphasize that the IPEC Site is located in a bedrock fracture controlled hydrologic regime<sup>91</sup>. As such, this type of localized "distance-based inconsistency" is to be expected and likely indicates that these wells are closer to (or within) the more pervious preferential flow pathway that is hypothesized to be responsible for the convergence and narrowing of the Tritium and Strontium plumes as they move toward the river from sources centered at widely spaced locations upgradient<sup>92</sup>.

Farther downgradient, in the vicinity of the river, increases in Strontium activity in MW-62 may be reflective of the Unit 1 SFPs defueling operations. The MW-62-138 depth interval (along with, but to a lesser extent the shallower intervals in overburden) appears to show two distinct Strontium peaks in Q1 2009 and Q4 2009<sup>93</sup>. Furthermore, a third, smaller magnitude, increase in Strontium activity is observed during the current (Q3 2010) quarter, and the activity is again greater than the approximate pre-defueling levels. However, it is noted that the Strontium levels in this monitoring installation are all relatively low (below 3 pCi/l), and this location does not appear to be proximate to (or within) the preferential flow path cited above for the Strontium plume. Therefore, the peaks in Strontium observed may not be associated with the Unit 1 defueling, and may be due to nothing more than hydrogeological variability. The other riverfront monitoring installation downgradient of the unit 1 Strontium plume, MW-67, may also be exhibiting impacts from the Unit 1 SFPs defueling. The shallowest depth interval, MW-67-39 has shown a moderate increase in Strontium levels in Q4 2009 followed by slight decreases in

---

<sup>88</sup> As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.

<sup>89</sup> As noted in Section 3.4.4 above, the Q3 2010 Strontium result in MW-50-42 exceeded the I.L. at this sampling interval. On the other hand, a decrease in Strontium activity was observed in MW-50-66, consistent with the "tail" portion of the perturbation.

<sup>90</sup> Based on Q2 2010 data, both sampling intervals in this monitoring location have approximately reached pre-defueling Strontium levels. This monitoring location is sampled semi-annually, thus no sample was collected during Q3 2010.

<sup>91</sup> While groundwater flow through the fractured bedrock at the IPEC Site is highly preferential at small areal scales, it is characterized by sufficiently interconnected small bedrock fractures to allow the hydrogeologic system to function and be modeled as a non-homogeneous, anisotropic, porous media at Site-wide scales.

<sup>92</sup> By way of contrast, in a porous media flow regime, the centerlines of plumes that start at widely spaced locations (spaced perpendicular to the groundwater flow path) will typically remain widely spaced (although the edges of the plumes will likely move closer as the plumes get wider through dispersion). In the case of fracture flow at IPEC however, not only do the Strontium and Tritium plume centerlines converge, but the plumes also get narrower as they move downgradient. In addition, MW-50 displays high relative Strontium concentrations and fault gouge was encountered during the drilling of this well. These behaviors/data are hallmark signatures of a more highly fractured zone preferentially controlling groundwater flow and thus the migration of the contaminants therein (see the Site Hydrologic Investigation Report for further CSM-focused discussion of this issue).

<sup>93</sup> The increase in Q1 2009 in MW-62-138 was followed by a steady decrease over the next two quarterly monitoring events, and the peak in Q4 2009 was followed by a greater magnitude decrease in Q1 2010; the Q2 2010 Strontium activity slightly increased compared to Q1 2010.



## Section 3.0 Data Evaluation

---

Q1 2010 through Q3 2010 (trends consistent with “tailing off” portion of an adsorbing radionuclide) after an overall, clear decreasing trend since October 2007. However, the monitoring interval directly below MW-67-39 (MW-67-105) has shown increases in Strontium activity over the past two monitoring events; this interval had previously shown generally stable Strontium levels since the initiation of the LTMP. Additionally, the Q3 2010 result exceeded the Strontium I.L. at MW-67-105, as discussed in **Section 3.4.4** above. The Strontium activity in this sampling interval is expected to decrease once this perturbation passes through the system.

From an overall, long-term perspective, Strontium levels downgradient of the Unit 1 SFPs are generally behaving as expected. The monitoring installations closest to the SFPs (e.g., U1-NCD, MW-42, U1-CSS and U1-SFDS) exhibited strong peaks in Strontium activity in response to defueling, and then have generally decreased to pre-defueling levels. Monitoring installations farther downgradient are generally showing decreases in Strontium activity over the past three quarterly sampling rounds and are approaching pre-defueling levels (e.g., MW-37, MW-55, and MW-57). It is expected that Strontium activities in these wells will continue to decrease to pre-defueling levels. Monitoring installations closer to the river may still show Strontium increases (similar to the current increase at MW-67-105) as the additional leakage experienced during defueling flushes through the groundwater flow system. It is expected that completion of this flushing mechanism will be protracted given the aforementioned impact of partitioning on Strontium levels in the groundwater. However, over time it is expected that downgradient Strontium plume levels will also continue their overall downward trend once this perturbation has fully passed through the system; decreasing trends are expected and predicted given that Entergy has terminated all leaks in the Unit 1 SFPs through decommissioning and the Unit 1 Strontium plume continues to decrease in accord with Monitored Natural Attenuation. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 1 SFPs through decommissioning, the Unit 1 Strontium plume satisfies the requirements for Monitored Natural Attenuation.



#### 4.0 CONCLUSIONS AND PLANNED FUTURE WORK

Given the data collected to date, the apparent strength of the CSM to evaluate those data, and the completion of source interdictions by Entergy, we believe all Program Objectives (see **Section 3.0**) are being met. These objectives are consistent with and fully encompass the guidance provided in the NEI Groundwater Protection Initiative (GPI).

Based on the specific results and evaluation of the Q3 2010 groundwater monitoring within the context of the Long Term Monitoring Program, IPEC plans to continue routine groundwater monitoring, related monitoring network maintenance and reporting of the data and engineering analyses. In this context, it is noted that the analyses and conclusions presented in this report are based on the data and information available up to and including the subject quarter. Data that becomes available after the subject quarter, but before the finalization date of the report is sequentially reflected in the associated subsequent reports.

This work will be conducted in accordance with the IPEC Radiological Groundwater Monitoring Program IP-SMM-CY-110.

More specifically, evaluation of data collected during Q3 2010 has shown the following:

- While I.L.s have again been met at a number of Unit 2 locations this quarter, there is no compelling evidence that any new unidentified leaks have developed in the Unit 2 SFP or other monitored Systems, Structures, or Components. The rationale underlying this continued conclusion is discussed more fully in Section 3.6 of the Q1 2009 Quarterly Monitoring Report. The validity of this conclusion is also not diminished by the Q3 2010 and/or Post-Q3 2010 I.L. exceedances in multiple MW-31 and MW-32 sampling intervals (MW-31-49, MW-31-63, MW-32-59, MW-32-149, and MW-32-173) proximate to the Unit 2 SFP because these Tritium increases have been generally shown to be due to a localized, transient surface spill from a temporary, rental RWST/R.O. processing skid during Q4 2009 (see **Section 3.4.5**). Given that this Tritium release was eliminated, it is expected that the Tritium activities will decrease to pre-spill levels at these sampling intervals<sup>94</sup>; although future releases from the storage/Retention Mechanism(s), replenished by these spills and historic SFP leaks, could create additional perturbations in Tritium levels. The above conclusion is continually reassessed on a quarterly basis as new data becomes available. In particular, this quarter's new LCD data as well as that for MH-5 VCFD have resulted in the initiation of additional investigations. While all LCD water is fully contained and does not enter the groundwater regime, the increases observed in MW-31, MW-32 and MH-5 VCFD appear to be potentially correlated, on a temporal basis, with this increased LCD flow rate<sup>95</sup>.
- Previously identified, more historic transient leaks included: the additional leakage from the Unit 1 SFPs during the 2008 defueling operations, the transient leakage from the distillation tank valves in Q1 2009, and the two transient surficial Tritium releases to Unit 3 Manhole A2 in Q2 2009 and the current Q3 2010:
  - Based on past work, additional leakage was expected during the raising of water levels in the Unit 1 SFPs for final fuel removal to ISFSI storage. Unit 1 SFPs leakage

---

<sup>94</sup> An overall decrease in Tritium activity is observed in all three previously mentioned MW-32 sampling intervals (MW-32-59, MW-32-149 and MW-32-173) during Q3 2010 for the first time since the transient RWST/R.O. surface spill was first seen at this location. However, the two MW-31 sampling intervals are still exhibiting overall increasing Tritium trends through Q3 2010.

<sup>95</sup> While the data trends appear to correlate on a temporal basis, it is noted that simple correlation does not demonstrate causation.

## Section 4.0 Conclusions and Planned Activities

---

was terminated with the drainage and sealing of the pools. This previous, transient leakage was initially verified as pronounced increases in Strontium and Cesium in the monitoring locations closest to Unit 1, and continues to be monitored.

- The Q1 2009 leakage from the distillation tank valves was independently<sup>96</sup> identified based on an increase in Tritium levels in monitoring installation MW-42 proximate to the tanks, and subsequent increases in downgradient wells (MW-53-82, U1-CSS, and MW-50-42). These valves were immediately repaired and the leakage was terminated. Based on the observed data trends, it appears that the Tritium input into the groundwater flow regime from the waste distillation tank valving leak has generally dissipated through the system<sup>97</sup>. However, the potential impact of this release further downgradient will be specifically scrutinized during subsequent monitoring rounds.
- Elevated Tritium activity was detected in Unit 3 Manhole A2 during routine 80-10 Effluents Program sampling during Q2 2009. This manhole is located proximate to the Unit 3 FSB. Subsequent re-sampling of this manhole showed rapidly decreasing Tritium activity, indicating that this was a one-time transient event. This elevated Tritium was also detected in a proximate groundwater monitoring installation (MW-45), likely due to exfiltration of Tritium from the manhole. A second elevated Tritium activity was detected in Manhole A2 (as well as Manhole A4, to a lesser degree) during routine 80-10 Effluents Program sampling during the current, Q3 2010, monitoring period. Similar to the peak observed in Q2 2009, the subsequent re-sampling indicated a rapid decrease in Tritium activity within the storm drain system. Both increases in A2 Tritium levels are believed to be due to condensation of SFP evaporation on the roof when the vent fan is not operating, which then enters the building roof drain leading directly into A2 during rainfall events, as is currently being verified. Both a nearby sampling interval (MW-41-40) and two downgradient sampling intervals (MW-46 and B-1) have also shown elevated Tritium levels during Q3 2010. The Tritium activity at these locations is expected to decrease, similar to the trends observed within the storm drain system.

As such, these data support the validity of the current CSM for use as a basis for Long Term Monitoring Program design. It is further noted that, while a portion of the above five documented localized release events traveled directly to the saturated groundwater regime and resulted in the observed transient “peaks” in radionuclide levels, additional portions of these releases likely remain above the water table as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events).

- While the current Tritium I.L. levels proved helpful over the past three quarters (Q1 through Q3 2010) in identifying a localized, transient surface spill from a temporary

---

<sup>96</sup> The valve leakage was initially identified during routine visual inspection rounds and immediately terminated. Given that the leak was within the Unit 1 FSB structure, it was documented in a Condition Report under Entergy's Corrective Action Program. This valve leak and repair subsequently came to light within the GPI program during investigations into the cause of the abrupt increase in Tritium levels in MW-42. Additional emphasis has therefore been placed on routine review of these reports as they potentially relate to GPI objectives.

<sup>97</sup> Additional portions of these releases likely remain above the water table in the release area as recharge to the various Retention Mechanisms. This additional unsaturated zone source recharge will likely be manifested in the future as additional non-specific peaks in radionuclide levels due to episodic releases to the groundwater flow regime from these mechanisms (e.g., from intense/prolonged precipitation events).

## Section 4.0 Conclusions and Planned Activities

---

rental RWST/R.O. skid, data collected during previous quarters have generally demonstrated that the I.L.s originally established are somewhat too sensitive relative to natural seasonal/precipitation-driven transient variations in radionuclide activities, as well as the variability inherent in the laboratory analyses. Relative to Strontium from the Unit 1 SFPs, the previous increases in activity in a number of monitoring points, due to the previous Unit 1 defueling operations, limit our ability to establish Strontium baseline levels for assessment of new I.L.s pursuant to the Monitored Natural Attenuation (MNA) of this plume. It is anticipated that this additional Strontium activity will take a number of quarters to completely flush through the onsite groundwater flow system and attenuate to reasonably stable levels. As such, the originally established I.L.s for both Tritium and Strontium will continue to be used until sufficient data is collected to allow re-evaluation of I.L. levels for the radionuclides of interest.

- From both qualitative and quantitative perspectives, the overall quarterly monitoring data set supports the conclusion that the overall Tritium activity in the Unit 2 plume has been decreasing since termination of the identified Unit 2 SFP leaks. These overall reductions have become particularly evident on the more recent quarterly report **Figures 6 and 6A** where the shaded plume<sup>98</sup> no longer extends to the river, as it did prior to Q2 2009. It is further visually evident from **Figure 6A** that the core of the plume (with quarterly rolling average activities greater than 100,000 pCi/L and 2007 bounding core activities greater than 250,000 pCi/L) has also shown a marked decrease in activity and extent. Based on the data and analyses provided above, our conclusion is that the Tritium plume associated with the historic leaks in the Unit 2 SFP has been undergoing long-term, overall reductions in activity which are consistent with Monitored Natural Attenuation (MNA), the remedial technology selected for the IPEC Site<sup>99</sup>. Given this conclusion, and the recognition that Entergy has terminated all identified leaks in the Unit 2 SFP<sup>100</sup>, this Unit 2 Tritium plume satisfies the requirements for Monitored Natural Attenuation.
- The overall Strontium activity within the Unit 1 plume had generally been stable or decreasing in response to West Pool demineralization conducted by Entergy beginning in 2006. However, the final defueling of the Unit 1 SFPs resulted in an initial, noticeable increase, followed by a subsequent and commensurate decrease, in Strontium levels

---

<sup>98</sup> The plume shading on **Figure 6** demarks the estimated boundary that separates Tritium levels greater than 5,000 pCi/L from those below this value, and provides a reasonable demarcation level for illustrating plume geometry and temporal variation. Although this value equates to one-quarter of the drinking water standard for Tritium, GZA emphasizes that drinking water standards (USEPA MCLs) do not apply to the IPEC property given that there are no drinking water sources on or proximate to the site. Where yearly rolling average radionuclide activity data were available for multiple depths at a given location, GZA used the highest value to develop plume delineations. This is a typical approach to represent three-dimensional contaminant data sets on two-dimensional maps.

<sup>99</sup> It is noted that the previously clear attenuation of the Unit 2 tritium plume has been confounded by a number of localized, transient surface spills. Entergy is currently in the process of reviewing and addressing work practices which may have contributed to the occurrence of these spills.

<sup>100</sup> Further justification for this conclusion can be found in Section 3.6 of the Q1 2009 Quarterly Monitoring Report as well as the Hydrogeologic Site Investigation Report. The Q1 2009 Report summarizes additional, more quantitative analyses which were completed to further investigate the integrity of the Unit 2 SFP. These analyses provide further support for the original conclusion that the Unit 2 SFP is no longer leaking. However, given the more recent behavior observed in the Unit 2 Leak Collection Device and MH-5 VCFD data, additional investigations/data evaluations are underway. In this regard, it is noted that these analyses cannot definitively and completely rule out the possibility of a remaining small Unit 2 SFP leak which could then also be supplying Tritium to the groundwater flow regime in addition to the Retention Mechanism(s) and surface spill from the process skid discussed above. While it is not possible to quantify the size of the minimum detectable leak with any degree of certainty, we believe that the maximum leak rate from the Unit 2 SFP that could potentially remain undetected by the groundwater monitoring system is less than 10 to 30 gpd (0.007 to 0.021 gallons per minute). It is also likely that if a small leak exists in the Unit 2 SFP liner, it should not get worse with time, as based on liner evaluations previously conducted by Entergy. It is further emphasized that while a leak of greater than 0.02 gallons per minute should be large enough to be readily detectable with the existing Long Term Monitoring Program, this amount of Tritium release to the river is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

## Section 4.0 Conclusions and Planned Activities

---

proximate to the SFPs, with later increases in the downgradient Strontium levels (see **Figure 7 and 7A**). This is as was predicted given the requirement to temporarily raise the pool levels for fuel rod removal, thus increasing leakage rate from the SFPs<sup>101</sup>. As anticipated, the levels proximate to the pool have decreased to pre-defueling Strontium levels, and levels downgradient of the pool are generally showing continued decreases as this additional Strontium-contaminated water flushes through the groundwater flow system. It is expected that this flushing mechanism will be protracted given the aforementioned impact of partitioning on Strontium levels in the groundwater. However, over time it is expected that downgradient Strontium plume levels will also achieve an overall downward trend below pre-defueling levels once this perturbation is finished passing through the system. Given this conclusion and the recognition that Entergy has terminated all identified leaks in the Unit 1 SFPs through decommissioning, the Unit 1 Strontium plume satisfies the requirements for Monitored Natural Attenuation. However, as indicated above, the establishment of updated I.L.s for the Unit 1 Strontium plume must await return to the original Strontium baseline levels existing prior to Unit 1 defueling.

- The amount of radionuclides being released through the groundwater pathway, even with the somewhat increased Tritium levels currently observed due to the RWST/R.O. skid transient surface spill, is still small compared to permitted levels of Tritium discharge to the river through the Discharge Canal.

---

<sup>101</sup> As of late 2008, all the fuel rods have been removed from the Unit 1 SFPs and the pool water has been drained. As such, the Unit 1 SFPs is no longer an active source of radionuclides to the subsurface.



## TABLES

**Table 1 Groundwater Sampling Methods, Equipment, Frequency, and Depths**

**Table 2 Historic Quarterly Low Tide Groundwater Elevations**

**Table 3 2010 3<sup>rd</sup> Groundwater Analytical Results and Averages**

**Table 4 2010 3<sup>rd</sup> Quarter Groundwater Analytical Results and I.L.s**

**Table 5 Historic Groundwater Analytical Results**

TABLE 1  
GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID <sup>1</sup>	Sampling Method	Sampling Equipment Used	Current Sampling Frequency	SAMPLING INTERVAL <sup>2</sup>				SAMPLING DEPTH <sup>3</sup>	
				FY Below Top of Casing		Elevation in Feet msl		Feet Below TOC	
				Top	Bottom	Top	Bottom	Top	Bottom
MW-30-69	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	67.3	71.3	8.4	4.4	69.3	-6.4
MW-30-84	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	77.3	85.4	-1.6	-9.5	83.8	-8.1
MW-31-49	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	34.8	49.3	40.8	26.3	48.8	26.8
MW-31-63	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	63.8	63.8	20.3	11.8	63.3	12.3
MW-31-85	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	69.8	85.4	5.8	-9.6	84.8	-9.2
MW-32-59	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	28.3	61.3	48.8	15.8	58.8	18.3
MW-32-85	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	79.3	92.8	-2.2	-15.7	85.3	-8.3
MW-32-131	Waterloo Low Flow	Waterloo Multilevel System	Inactive	128.8	136.8	-48.7	-61.2	130.8	-53.7
MW-32-149	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	125.8	156.8	-70.2	-79.7	149.3	-72.2
MW-32-173	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	165.8	174.3	-88.7	-97.2	172.8	-95.7
MW-32-190	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	180.3	193.9	-103.2	-116.8	190.3	-113.7
MW-33	Low Flow	Peristaltic Pump	Annually	8.0	30.0	13.6	-11.7	16	2.8
MW-34	Low Flow	Peristaltic Pump	Inactive	5.0	30.0	13.5	-11.5	16.5	2.0
MW-35	Low Flow	Peristaltic Pump	Annually	6.5	30.0	12.1	-11.4	15.0	3.6
MW-36-24	Low Flow	Peristaltic Pump	Quarterly	11.0	24.0	0.8	-12.2	17.0	-5.2
MW-36-41	Modified Well Vol. Purge	Peristaltic Pump	Quarterly	36.0	41.0	-24.2	-29.2	37.0	-25.2
MW-36-52	Modified Well Vol. Purge	Peristaltic Pump	Quarterly	48.0	53.0	-36.2	-41.2	50.0	-38.2
MW-37-24	Low Flow	Peristaltic Pump	Quarterly	12.0	22.0	3.0	-7.0	17.0	-2.0
MW-37-32	Low Flow	Peristaltic Pump	Quarterly	28.0	32.5	-13.0	-17.5	29.0	-14.0
MW-37-40	Modified Well Vol. Purge	Peristaltic Pump	Quarterly	38.5	40.5	-23.5	-24.5	39.0	-24.0
MW-38	Low Flow	Peristaltic Pump	Quarterly	52.0	57.0	-37.0	-42.0	55.0	-40.0
MW-39-67	Low Flow	Peristaltic Pump	Inactive	5.0	40.0	9.3	-25.7	25.4	-11.1
MW-39-84	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	65.0	70.5	15.0	9.5	67.0	13.0
MW-39-102	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	76.5	85.0	3.5	-5.0	83.5	-3.5
MW-39-124	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	93.0	103.0	-13.0	-23.0	101.5	-21.5
MW-39-183	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	115.0	126.5	-35.0	-46.5	124.0	-44.0
MW-39-195	Waterloo Low Flow	Waterloo Multilevel System	Semi-Annually	169.5	186.0	-89.5	-106.0	182.5	-102.5
MW-40-27	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	182.0	198.6	-113.0	-118.4	195.0	-115.0
MW-40-46	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	44.2	53.7	29.0	19.5	46.2	27.0
MW-40-81	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	64.7	84.2	8.5	-11.0	80.7	-7.5
MW-40-100	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	93.2	106.7	-20.0	-33.5	100.2	-27.0
MW-40-127	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	125.2	136.7	-52.0	-63.5	127.2	-54.0
MW-40-162	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	158.7	190.3	-85.5	-116.9	161.7	-88.5
MW-41-40	Low Flow	Peristaltic Pump	Quarterly	22.0	42.0	32.9	12.9	36.0	18.9
MW-41-63	Modified Well Vol. Purge	Watera Pump	Quarterly	59.0	64.0	-4.1	-9.1	61.0	-6.1
MW-42-49	Low Flow	Bladder Pump	Quarterly	31.0	51.0	38.7	18.7	41.0	28.7
MW-42-78	Modified Well Vol. Purge	Watera Pump	Quarterly	69.0	79.0	0.7	-9.3	74.0	-4.3
MW-43-38	Low Flow	Bladder Pump	Quarterly	8.0	28.0	40.8	20.7	23.0	25.8
MW-43-62	Low Flow	Bladder Pump	Quarterly	42.0	62.0	6.8	-13.2	54.0	-5.2
MW-44-66	Modified Well Vol. Purge	Bladder Pump	Quarterly	52.0	67.0	41.5	26.5	63.0	30.5
MW-44-102	Modified Well Vol. Purge	Watera Pump	Quarterly	79.0	104.0	14.5	-10.5	80.0	13.5
MW-45-42	Modified Well Vol. Purge	Bladder Pump	Quarterly	27.5	42.5	26.2	11.2	37.0	16.6
MW-45-61	Modified Well Vol. Purge	Watera Pump	Quarterly	51.5	61.5	2.2	-7.8	58.0	-4.4
MW-46	Modified Well Vol. Purge	Peristaltic Pump	Quarterly	6.0	30.0	12.1	-11.9	10.5	7.6
MW-47-56	Low Flow	Submersible Pump	Inactive	36.0	56.0	34.3	14.3	52.0	18.3
MW-47-80	Modified Well Vol. Purge	Watera Pump	Inactive	70.0	80.0	0.3	-9.7	72.0	-1.7

J:\17-000-18-000\17869\17869-02.MG-QI-2010\FINAL\Tables\ Table 1-Groundwater Sampling Methods, Equipment, Frequency and Depths.xlsx  
Methods, Frequency, Depths

TABLE 1  
GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID <sup>1</sup>	Sampling Method	Sampling Equipment Used	Current Sampling Frequency	SAMPLING INTERVAL <sup>2</sup>				SAMPLING DEPTH <sup>3</sup>	
				FY Below Top of Casing		Elevation in Feet msl		Feet Below TOC	
				Top	Bottom	Top	Bottom	Top	Bottom
MW-48-23	Low Flow	Peristaltic Pump	Inactive	8.0	23.0	7.4	-7.6	15.8	-6.4
MW-48-37	Low Flow	Peristaltic Pump	Inactive	33.0	38.0	-17.6	22.6	35.8	-20.4
MW-49-26	Low Flow	Peristaltic Pump	Quarterly	15.0	25.0	-0.3	-16.4	26.0	-5.3
MW-49-42	Low Flow	Peristaltic Pump	Quarterly	32.0	42.0	-17.4	-27.4	37.0	-22.3
MW-49-65	Low Flow	Peristaltic Pump	Quarterly	66.0	65.0	-45.4	-50.4	61.0	-46.4
MW-50-42	Low Flow	Peristaltic Pump	Quarterly	22.0	42.0	-7.1	-27.1	27.0	-12.1
MW-50-66	Low Flow	Peristaltic Pump	Quarterly	62.0	67.0	-47.1	-52.1	66.0	-45.1
MW-51-40	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	29.7	44.2	38.0	23.5	39.7	28.0
MW-51-104	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	63.2	81.2	4.5	-13.5	78.7	-11.0
MW-51-135	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	101.2	111.2	-33.5	-43.5	103.7	-36.0
MW-51-163	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	130.2	143.7	-62.5	-76.0	135.2	-67.5
MW-51-189	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	154.7	166.2	-87.0	-98.5	162.7	-95.0
MW-52-122	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	184.2	197.8	-116.5	-129.9	189.2	-121.5
MW-52-162	Modified Well Vol. Purge	Peristaltic Pump	Annually	2.0	12.0	14.8	-4.8	16.0	6.8
MW-52-18	Waterloo Low Flow	Waterloo Multilevel System	Annually	10.0	30.0	4.9	-15.1	17.5	-2.6
MW-52-48	Waterloo Low Flow	Waterloo Multilevel System	Annually	48.0	56.0	-33.1	-41.1	48.0	-33.1
MW-52-64	Waterloo Low Flow	Waterloo Multilevel System	Annually	59.0	71.5	-44.1	-56.6	64.0	-49.1
MW-52-122	Waterloo Low Flow	Waterloo Multilevel System	Annually	110.5	123.5	-95.6	-108.6	122.0	-107.1
MW-52-162	Waterloo Low Flow	Waterloo Multilevel System	Annually	154.5	164.0	-139.6	-149.1	161.5	-146.6
MW-52-181	Waterloo Low Flow	Waterloo Multilevel System	Annually	171.0	198.1	-156.1	-183.0	181.0	-166.1
MW-53-82	Low Flow	Bladder Pump	Quarterly	62.0	82.0	8.3	-11.7	75.0	-4.7
MW-53-120	Modified Well Vol. Purge	Waterloo Pump	Quarterly	100.0	120.0	-29.7	-49.7	105.0	-34.7
MW-54-37	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	29.0	42.0	-15.9	-28.9	36.5	-23.4
MW-54-58	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	51.5	61.0	-38.4	-50.9	57.5	-41.4
MW-54-123	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	116.0	126.0	-102.9	-112.9	123.0	-109.9
MW-54-144	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	135.0	155.5	-121.9	-142.4	144.0	-130.9
MW-54-173	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	170.5	182.0	-157.4	-168.9	172.5	-159.4
MW-54-190	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	185.0	203.6	-171.9	-190.3	190.0	-176.9
MW-55-24	Low Flow	Peristaltic Pump	Quarterly	14.0	24.0	4.3	-5.8	16.0	2.3
MW-55-35	Low Flow	Peristaltic Pump	Quarterly	30.0	35.0	-11.8	-16.8	32.0	-13.8
MW-55-54	Low Flow	Peristaltic Pump	Quarterly	44.0	54.0	-25.8	-35.8	47.0	-28.8
MW-56-53	Low Flow	Bladder Pump	Semi-Annually	49.2	54.2	21.0	16.0	52.0	18.3
MW-56-83	Modified Well Vol. Purge	Waterloo Pump	Semi-Annually	69.9	84.9	0.4	-14.6	74.0	-3.7
MW-57-11	Modified Well Vol. Purge	Peristaltic Pump	Annually	6.0	11.0	9.0	4.0	16.0	5.0
MW-57-20	Modified Well Vol. Purge	Peristaltic Pump	Annually	15.5	20.5	-0.5	-5.5	19.0	-4.0
MW-57-45	Modified Well Vol. Purge	Peristaltic Pump	Annually	30.5	45.5	-15.5	-30.5	46.0	-25.0
MW-58-26	Low Flow	Peristaltic Pump	Semi-Annually	16.0	26.0	-1.4	-11.4	26.0	-5.4
MW-58-65	Low Flow	Peristaltic Pump	Semi-Annually	50.0	65.0	-35.4	-50.4	54.0	-39.4
MW-59-32	Low Flow	Peristaltic Pump	Inactive	21.0	31.0	-6.5	-16.5	27.0	-12.5
MW-59-45	Low Flow	Peristaltic Pump	Inactive	35.0	45.0	-20.5	-30.5	42.0	-27.5
MW-59-68	Low Flow	Peristaltic Pump	Inactive	53.0	68.0	-38.5	-53.5	58.0	-43.5
MW-60-35	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	24.9	39.4	-12.4	-26.9	34.9	-22.4
MW-60-53	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	45.4	59.4	-32.9	-46.9	53.4	-40.9
MW-60-72	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	66.4	78.9	-53.9	-66.4	72.4	-59.9
MW-60-135	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	124.9	141.4	-112.4	-128.9	134.9	-122.4
MW-60-154	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	147.4	164.9	-134.9	-152.4	154.4	-141.9
MW-60-176	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	176.9	200.4	-158.4	-187.8	175.9	-163.4

J:\17-000-18-000\17869\17869-02.MG-Q0-2010\FINAL\Tables\ Table 1-Groundwater Sampling Methods, Equipment, Frequency and Depths.xlsx; Methods, Frequency, Depths



TABLE 1  
GROUNDWATER SAMPLING METHODS, EQUIPMENT, FREQUENCY AND DEPTHS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID <sup>1</sup>	Sampling Method	Sampling Equipment Used	Current Sampling Frequency	SAMPLING INTERVAL <sup>2</sup>				SAMPLING DEPTH <sup>3</sup>	
				FY Below Top of Casing		Elevation in Feet msl		Feet Below TOC	Elevation in Feet msl
				Top	Bottom	Top	Bottom		
MW-65-18	Low Flow	Peristaltic Pump	Quarterly	4.7	14.7	10.0	6.0	15.5	1.2
MW-65-37	Low Flow	Peristaltic Pump	Quarterly	33.3	38.3	-18.6	-23.6	34.5	-19.8
MW-62-53	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	49.6	54.1	-36.8	-41.3	53.1	-40.3
MW-62-71	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	61.1	82.6	-48.3	-69.8	71.1	-58.3
MW-62-92	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	88.6	99.1	-75.8	-86.3	91.6	-78.8
MW-62-138	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	126.1	143.6	-113.3	-130.8	138.1	-125.3
MW-62-182	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	177.6	198.7	-164.8	-185.7	182.1	-169.3
MW-63-18	Low Flow	Peristaltic Pump	Quarterly	8.0	18.0	-3.8	-13.8	14.9	0.7
MW-63-34	Low Flow	Peristaltic Pump	Quarterly	30.0	35.0	-15.8	-20.8	31.5	-17.3
MW-63-50	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	41.5	58.0	-29.2	-45.7	49.5	-37.2
MW-63-93	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	81.5	100.5	-69.2	-88.2	93.0	-80.7
MW-63-112	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	106.5	112.0	-94.2	-99.7	111.5	-99.2
MW-63-121	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	118.0	127.5	-105.7	-115.2	121.0	-108.7
MW-63-163	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	150.5	165.0	-138.2	-152.7	162.5	-150.2
MW-63-174	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	168.0	191.1	-155.7	-178.6	174.0	-161.7
MW-66-21	Low Flow	Peristaltic Pump	Quarterly	7.0	27.0	6.0	-7.0	14.1	0
MW-66-36	Low Flow	Peristaltic Pump	Quarterly	31.0	36.0	-17.0	-22.0	33.6	-19.5
MW-67-39	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	28.8	54.3	-15.8	-41.3	38.3	-25.8
MW-67-105	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	90.3	110.8	-77.3	-97.8	104.8	-92.3
MW-67-173	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	164.8	188.3	-151.8	-175.3	172.3	-159.8
MW-67-219	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	209.3	229.8	-196.3	-216.8	218.8	-206.3
MW-67-276	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	250.8	281.3	-237.8	-268.3	275.3	-262.8
MW-67-323	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	317.8	328.3	-304.8	-315.3	322.3	-309.8
MW-67-340	Waterloo Low Flow	Waterloo Multilevel System	Quarterly	335.3	347.9	-322.3	-334.9	339.8	-327.3
MW-107	Low Flow	Bladder Pump	Annually	105.1	126.1	34.9	13.9	32.7	110.1
MW-111	Low Flow	Peristaltic Pump	Semi-Annually	11.6	17.4	7.0	1.5	16.5	2.4
U3-4D	Modified Well Vol. Purge	Peristaltic Pump	Quarterly	25.0	27.6	-10.2	-12.8	25.6	-10.8
U3-4S	Low Flow	Peristaltic Pump	Quarterly	0.2	1.2	8.3	-2.7	2.8	2.8
U3-11	Low Flow	Peristaltic Pump	Quarterly	0.6	1.6	3.1	2.1	5.7	2.6
U3-12	Low Flow	Peristaltic Pump	Quarterly	0.6	1.6	2.7	1.7	5.7	2.6
U1-CSS	Low Flow	Bladder Pump	Semi-Annually	NA	10.2	NA	NA	14.0	6.1
LAF-002	Low Flow	NA	Semi-Annually	NA	NA	NA	NA	NA	-22.3
U1-NCID	Grab	NA	Quarterly	NA	NA	NA	NA	NA	NA
U1-SFDS	Grab	NA	Quarterly	NA	NA	NA	NA	NA	NA
U2	Low Flow	Peristaltic Pump	Quarterly	NA	NA	NA	NA	NA	NA
MH-5 VCFD <sup>5</sup>	Grab	NA	Quarterly	NA	NA	NA	NA	NA	NA
B-1 <sup>6</sup>	Grab	NA	Quarterly	NA	NA	NA	NA	NA	NA
B-6 <sup>6</sup>	Grab	NA	Quarterly	NA	NA	NA	NA	NA	NA

- Notes:
- For nested multi-level monitoring wells, suffix of well ID indicates depth (rounded to nearest foot) from reference point on casing to bottom of well screen. For Waterloo multi-level systems, suffix indicates depth (rounded to nearest foot) from reference point on casing to top of sampling port. Well IDs without a suffix are open bedrock wellbores.
  - For nested multi-level monitoring wells, interval includes well screen and sand pack. For Waterloo multi-level systems, interval includes open wellbore between bottom of 1st packer above and top of 1st packer below sampling port. For open bedrock wellbores, interval extends from bottom of casing to bottom of hole.
  - Sampling depths within sampling intervals (i.e. location of pump intake) have been located adjacent to a transmissive zone where possible.
  - Dw pattern denotes sampling interval is positioned within overburden. Open box indicates sampling interval is in bedrock.
  - These locations are storm drains.

TABLE 2  
HISTORIC QUARTERLY LOW TIDE GROUNDWATER ELEVATIONS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID	LOW RIVER TIDE GROUNDWATER ELEVATIONS (feet msl)															
	Quarter 2 <sup>1</sup> , 2007	Quarter 3 <sup>1</sup> , 2007	Quarter 4 <sup>1</sup> , 2007	Quarter 1 <sup>1</sup> , 2008	Quarter 2 <sup>1</sup> , 2008	Quarter 3 <sup>1</sup> , 2008	Quarter 4 <sup>1</sup> , 2008	Quarter 1 <sup>1</sup> , 2009	Quarter 2 <sup>1</sup> , 2009	Quarter 3 <sup>1</sup> , 2009	Quarter 4 <sup>1</sup> , 2009	Quarter 1 <sup>1</sup> , 2010	Quarter 2 <sup>1</sup> , 2010	Quarter 3 <sup>1</sup> , 2010	Quarter 4 <sup>1</sup> , 2010	
HR-1	NA	-0.86	11.57	-2.15	-1.13	-1.05	-1.69	-3.28	-1.52	-0.27	-3.59	-0.36	-0.56	-0.71	-0.71	
I-2	50.23	48.62	51.87	53.73	52.11	52.90	50.75	NA	NA	NA	51.60	52.46	53.33	50.49	NA	
MW-30-69	11.83	11.53	12.00	NA	12.28	11.77	11.71	12.33	11.84	13.76	NA	NA	NA	NA	NA	
MW-30-84	12.77	12.47	12.83	NA	13.06	12.68	12.36	13.13	12.82	12.48	12.27	13.26	12.76	11.31	NA	
MW-31-49	44.09	NA	45.40	47.50	46.14	45.59	44.13	46.44	45.40	-	-	-	-	-	-	
MW-31-63	41.56	NA	42.71	43.96	42.17	41.52	41.21	44.12	43.20	-	-	-	-	-	-	
MW-31-85	39.59	NA	40.81	43.19	41.89	41.52	39.64	42.10	40.64	-	-	-	-	-	-	
MW-32-48	NA	46.73	48.81	48.81	42.77	46.98	45.79	48.08	47.31	-	-	-	-	-	-	
MW-32-59	NA	41.44	45.99	47.90	46.75	45.72	44.48	46.83	45.62	-	-	-	-	-	-	
MW-32-85 (MW-32-92) <sup>17</sup>	10.27	12.35	12.78	13.30	13.17	12.30	12.16	12.60	11.61	-	-	-	-	-	-	
MW-32-131 (MW-32-140) <sup>12</sup>	13.11	11.96	13.21	25.01	15.67	11.34	11.53	11.86	11.06	-	-	-	-	-	-	
MW-32-149 (MW-32-165) <sup>12</sup>	8.18	9.87	10.06	10.20	10.04	9.71	9.77	10.00	9.18	-	-	-	-	-	-	
MW-32-173	NA	9.73	9.86	9.92	9.70	9.45	9.45	9.68	8.81	-	-	-	-	-	-	
MW-32-190 (MW-32-196) <sup>17</sup>	6.74	8.05	7.88	7.88	7.52	7.16	7.05	7.24	6.26	-	-	-	-	-	-	
MW-33	10.08	9.80	10.38	11.49	11.66	10.55	10.60	11.23	10.52	-	-	-	-	-	-	
MW-34	9.87	9.82	10.14	11.63	12.03	10.54	10.54	11.25	10.54	-	-	-	-	-	-	
MW-35	10.03	9.67	10.37	11.65	12.06	10.68	10.68	11.36	NA	-	-	-	-	-	-	
MW-36-24	8.89	7.31	7.67	6.85	6.86	5.58	9.05	NA	7.25	-	-	-	-	-	-	
MW-36-41	8.22	NA	NA	NA	NA	NA	NA	NA	NA	-	-	-	-	-	-	
MW-36-52	7.43	6.43	6.45	6.12	6.29	6.99	7.15	8.12	6.62	-	-	-	-	-	-	
MW-37-22	5.51	5.13	4.83	4.66	5.13	4.18	4.45	5.34	5.24	-	-	-	-	-	-	
MW-37-32	5.51	5.07	4.82	4.63	4.05	5.36	5.64	4.55	5.32	-	-	-	-	-	-	
MW-37-40	5.40	6.83	6.19	6.83	5.95	6.18	6.04	6.19	6.19	-	-	-	-	-	-	
MW-37-57	7.07	6.23	6.39	6.28	6.07	6.64	7.20	6.50	6.56	-	-	-	-	-	-	
MW-38	3.01	2.19	1.46	2.22	1.53	2.12	2.22	2.24	2.24	-	-	-	-	-	-	
MW-39-67	NA	26.84	NA	32.20	31.69	25.96	25.21	28.74	NA	-	-	-	-	-	-	
MW-39-81	NA	26.64	NA	31.94	31.48	25.78	25.12	28.62	NA	-	-	-	-	-	-	
MW-39-100	NA	26.38	NA	30.99	31.34	25.52	24.79	28.32	NA	-	-	-	-	-	-	
MW-39-102	NA	26.31	NA	31.56	NA	NA	NA	NA	NA	-	-	-	-	-	-	
MW-39-124	NA	26.05	28.37	30.67	25.07	25.07	27.74	27.74	NA	-	-	-	-	-	-	
MW-39-183	NA	25.28	29.74	29.83	29.83	23.35	23.79	26.78	NA	-	-	-	-	-	-	
MW-39-195	NA	24.36	28.80	28.89	28.89	23.35	22.70	25.63	NA	-	-	-	-	-	-	
MW-40-27	NA	55.16	60.39	56.99	56.99	54.70	51.22	59.53	57.25	38.75	55.71	59.08	59.86	52.85	-	
MW-40-46	NA	47.27	53.19	59.35	56.09	52.57	52.35	59.13	56.56	-	-	-	-	-	-	
MW-40-81	NA	41.63	47.45	56.06	55.78	47.28	46.83	55.67	53.13	-	-	-	-	-	-	
MW-40-100	NA	39.47	45.18	54.10	53.75	44.83	44.32	53.59	51.24	-	-	-	-	-	-	
MW-40-127	NA	38.89	44.50	53.61	44.33	44.33	43.87	53.29	50.59	-	-	-	-	-	-	
MW-40-162	NA	36.67	41.09	50.49	50.26	41.32	40.66	49.76	46.80	48.42	12.85	49.55	50.03	38.96	-	
MW-41-40	29.87	NA	32.48	36.37	33.81	31.28	30.71	33.62	32.05	-	-	-	-	-	-	
MW-41-63	25.94	NA	27.77	33.31	32.76	27.53	26.96	30.38	28.39	-	-	-	-	-	-	
MW-42-49	NA	34.55	34.55	34.96	34.81	34.52	34.43	34.78	34.47	-	-	-	-	-	-	
MW-42-78	NA	35.71	35.71	36.63	36.28	35.38	35.07	36.03	35.75	-	-	-	-	-	-	
MW-43-28	32.75	31.08	31.98	33.47	33.95	32.51	32.15	33.43	32.54	32.66	NA	NA	34.23	37.14	-	
MW-43-62	30.83	NA	NA	NA	32.16	30.48	31.76	34.13	30.88	NA	30.28	32.00	32.00	30.20	-	
MW-44-67	33.36	NA	34.36	37.99	35.47	35.29	34.00	34.96	34.50	-	-	-	-	-	-	
MW-44-102	23.10	NA	24.84	NA	30.88	25.86	25.16	28.09	27.41	-	-	-	-	-	-	
MW-45-42	NA	24.82	28.47	34.19	37.16	28.63	25.43	32.02	29.03	-	-	-	-	-	-	
MW-45-61	NA	24.33	27.57	32.91	32.46	27.16	26.68	29.99	25.25	-	-	-	-	-	-	
MW-46	12.80	11.95	12.57	15.05	14.97	12.62	12.81	14.29	12.47	12.83	NA	NA	16.49	12.45	-	
MW-47-56	21.83	20.77	23.05	23.76	20.77	22.84	22.37	26.51	23.43	-	-	-	-	-	-	
MW-47-80	22.29	21.41	21.82	26.53	26.33	21.52	21.08	26.37	24.18	-	-	-	-	-	-	
MW-48-23	-0.08	-0.27	-0.18	-1.14	-0.23	-0.18	-0.18	-0.18	-0.19	-	-	-	-	-	-	
MW-48-37	0.64	0.26	-0.06	-0.18	0.32	0.06	-0.15	-0.50	0.04	-	-	-	-	-	-	
MW-49-26	1.04	NA	-0.37	-0.62	0.51	0.37	0.37	-0.25	0.54	-	-	-	-	-	-	
MW-49-42	0.31	0.50	0.40	-0.44	0.92	1.02	0.88	-0.06	0.51	-	-	-	-	-	-	

FW17000418.9991786917869-92.MGCO-2010(FINAL)Tables  
Table 2-Historic Quarterly Low Tide Groundwater Elevations.xlsx  
gw elevations

TABLE 2  
HISTORIC QUARTERLY LOW TIDE GROUNDWATER ELEVATIONS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID	LOW RIVER TIDE GROUNDWATER ELEVATIONS (Feet msl)														
	Quarter 2 <sup>1</sup> , 2007	Quarter 3 <sup>1</sup> , 2007	Quarter 4 <sup>1</sup> , 2007	Quarter 1 <sup>1</sup> , 2008	Quarter 2 <sup>1</sup> , 2008	Quarter 3 <sup>1</sup> , 2008	Quarter 4 <sup>1</sup> , 2008	Quarter 1 <sup>1</sup> , 2009	Quarter 2 <sup>1</sup> , 2009	Quarter 3 <sup>1</sup> , 2009	Quarter 4 <sup>1</sup> , 2009	Quarter 1 <sup>1</sup> , 2010	Quarter 2 <sup>1</sup> , 2010	Quarter 3 <sup>1</sup> , 2010	Quarter 4 <sup>1</sup> , 2010
MW-49-65	0.89	1.01	0.34	0.07	0.70	0.68	0.47	-0.08	0.57	-	-	-	-	-	-
MW-50-12	7.21	NA	NA	NA	5.24	6.40	7.06	5.66	6.09	-	-	-	-	-	-
MW-50-66	3.71	NA	NA	NA	2.24	2.83	2.82	1.95	2.82	-	-	-	-	-	-
MW-51-40	NA	48.69	50.07	51.95	52.35	49.44	49.24	49.32	45.15	46.45	42.45	43.37	41.72	-	41.89
MW-51-79	NA	39.92	41.07	42.91	44.17	40.71	40.36	42.75	42.15	-	-	-	-	-	-
MW-51-102	NA	35.98	38.07	38.46	35.04	35.56	36.1*	33.18	37.8	-	-	-	-	-	-
MW-51-104	NA	NA	37.93	38.41	35.02	36.49	36.03	37.99	37.49	-	-	-	-	-	-
MW-51-135	NA	37.42	39.47	39.99	40.71	38.10	37.68	39.75	39.34	-	-	-	-	-	-
MW-51-163	NA	33.79	34.83	36.15	36.77	34.30	33.90	35.74	35.44	-	-	-	-	-	-
MW-51-189	NA	29.33	30.16	31.34	31.79	29.65	29.36	30.81	30.48	32.18	29.93	31.85	31.42	29.07	-
MW-52-11	6.04	5.61	8.12	8.47	8.85	8.65	8.44	8.19	9.20	-	-	-	-	-	-
MW-52-18	6.64	NA	8.63	6.04	6.07	5.89	6.02	5.78	5.87	-	-	-	-	-	-
MW-52-48	7.08	NA	6.55	6.53	5.95	6.20	6.14	6.05	5.75	-	-	-	-	-	-
MW-52-64	5.96	NA	5.90	5.25	5.03	5.21	5.16	5.20	4.89	-	-	-	-	-	-
MW-52-118	5.34	NA	4.41	4.44	4.32	4.36	4.48	4.23	4.23	-	-	-	-	-	-
MW-52-122	5.25	NA	4.26	4.32	4.18	4.21	4.55	4.11	4.20	-	-	-	-	-	-
MW-52-162	0.67	NA	-0.80	-1.31	-0.80	-0.58	-1.30	-2.07	-1.18	-	-	-	-	-	-
MW-52-181	0.41	NA	-1.08	-1.56	-1.00	-1.30	-1.64	-2.38	-1.54	-	-	-	-	-	-
MW-53-82	NA	9.59	10.03	11.99	12.60	10.35	NA	11.11	NA	11.11	9.87	11.15	11.67	9.98	-
MW-53-120	9.91	9.18	9.59	10.87	11.49	9.76	NA	10.55	9.78	10.43	9.13	10.53	11.02	9.60	-
MW-54-35	NA	NA	6.40	6.27	6.36	6.16	6.41	5.75	6.14	-	-	-	-	-	-
MW-54-37	7.52	NA	6.58	6.45	6.30	6.30	6.53	5.90	6.04	-	-	-	-	-	-
MW-54-58	6.86	NA	5.82	5.60	5.55	5.53	5.76	5.49	5.17	-	-	-	-	-	-
MW-54-123	5.69	NA	4.16	3.65	3.52	4.01	4.06	2.99	3.56	-	-	-	-	-	-
MW-54-144	8.85	NA	7.13	6.90	6.48	6.92	6.97	6.53	6.53	-	-	-	-	-	-
MW-54-173	5.17	NA	3.52	2.99	2.85	3.27	3.29	2.19	2.72	-	-	-	-	-	-
MW-54-190	5.08	NA	3.46	2.91	2.76	3.16	3.13	2.00	2.49	-	-	-	-	-	-
MW-55-24	8.56	7.82	7.97	8.17	8.16	8.18	8.35	8.18	8.06	8.39	7.80	8.58	8.56	8.02	-
MW-55-35	8.10	7.29	7.50	7.80	7.59	7.62	8.30	7.63	7.63	9.49	-	-	-	-	-
MW-55-54	8.47	7.65	7.75	8.08	8.32	8.22	8.82	8.14	7.89	8.14	7.66	8.39	8.34	7.97	-
MW-56-53	21.01	20.16	NA	NA	26.93	NA	21.90	27.33	22.06	-	-	-	-	-	-
MW-56-83	21.10	20.10	22.18	26.41	26.16	NA	21.51	25.13	22.60	-	-	-	-	-	-
MW-57-11	9.57	8.83	9.36	10.99	NA	10.03	10.27	11.11	10.09	-	-	-	-	-	-
MW-57-20	9.38	NA	NA	12.07	NA	10.02	9.92	10.63	9.84	-	-	-	-	-	-
MW-57-45	9.08	NA	NA	NA	10.59	NA	NA	10.71	NA	-	-	-	-	-	-
MW-58-26	8.03	6.49	6.58	8.32	7.36	7.29	7.19	7.56	7.40	-	-	-	-	-	-
MW-58-65	6.03	6.83	6.22	NA	6.83	7.13	6.46	6.68	6.70	-	-	-	-	-	-
MW-58-32	1.06	NA	0.67	0.42	0.77	0.81	0.47	0.31	1.37	-	-	-	-	-	-
MW-58-45	1.06	1.27	0.42	NA	9.23	NA	2.52	0.44	NA	-	-	-	-	-	-
MW-59-68	2.91	2.51	1.97	0.90	-0.11	NA	-1.79	-5.56	-5.89	-	-	-	-	-	-
MW-60-35	2.19	1.28	1.32	1.38	1.63	0.82	2.04	1.99	3.07	-	-	-	-	-	-
MW-60-53	-0.63	-1.21	-1.67	-2.01	-1.37	-1.76	-2.03	-2.70	NA	-	-	-	-	-	-
MW-60-55	NA	-0.28	-0.73	-1.10	-0.47	-0.50	-1.21	-1.91	NA	-	-	-	-	-	-
MW-60-72	0.74	-0.09	-0.45	-0.68	-0.14	-0.64	NA	-1.43	0.28	-	-	-	-	-	-
MW-60-135	0.94	0.11	-0.44	-0.90	-0.27	-0.71	-1.02	-1.72	0.11	-	-	-	-	-	-
MW-60-154	0.08	0.96	-1.61	-0.96	-1.49	-1.91	-2.25	-2.99	NA	-	-	-	-	-	-
MW-60-176	-0.48	-1.38	-2.03	-2.47	-1.82	-2.16	-2.59	-3.41	NA	-	-	-	-	-	-
MW-62-18	0.25	0.25	-0.37	-0.79	0.13	0.06	-0.12	-0.82	NA	-	-	-	-	-	-
MW-62-37	0.59	0.61	-0.03	-0.46	0.49	0.59	-0.15	-1.13	0.11	-	-	-	-	-	-
MW-62-52	NA	0.48	-0.30	-1.13	-0.19	-0.29	-0.93	-1.64	-0.42	-	-	-	-	-	-
MW-62-53	0.95	0.54	-0.25	-1.01	-0.10	-0.16	-0.84	-2.03	-0.44	-	-	-	-	-	-
MW-62-71	0.89	0.22	-0.56	-1.26	-0.55	-0.56	-1.26	-2.15	-1.03	-	-	-	-	-	-
MW-62-92	1.07	0.58	-0.09	-0.76	-0.11	-0.10	-0.85	-1.68	-0.70	-	-	-	-	-	-
MW-62-138	1.40	0.77	0.09	-0.49	0.13	0.25	-0.37	-1.33	-0.40	-	-	-	-	-	-
MW-62-181	1.33	-0.33	-0.99	-0.99	-0.32	-0.36	-0.92	-1.88	-0.88	-	-	-	-	-	-
MW-62-182	NA	-0.33	-1.83	-0.78	-1.29	-1.25	-1.85	-2.66	-1.82	-	-	-	-	-	-

P:\17\0064\8\99917869\1869-92.MG\CO-2010\FINAL\Tables  
gw elevations  
Table 2-Historic Quarterly Low Tide Groundwater Elevations.xlsx

TABLE 2  
HISTORIC QUARTERLY LOW TIDE GROUNDWATER ELEVATIONS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID	LOW RIVER TIDE GROUNDWATER ELEVATIONS (Feet msl)													
	Quarter 2 <sup>nd</sup> , 2007	Quarter 3 <sup>rd</sup> , 2007	Quarter 4 <sup>th</sup> , 2007	Quarter 1 <sup>st</sup> , 2008	Quarter 2 <sup>nd</sup> , 2008	Quarter 3 <sup>rd</sup> , 2008	Quarter 4 <sup>th</sup> , 2008	Quarter 1 <sup>st</sup> , 2009	Quarter 2 <sup>nd</sup> , 2009	Quarter 3 <sup>rd</sup> , 2009	Quarter 4 <sup>th</sup> , 2009	Quarter 1 <sup>st</sup> , 2010	Quarter 2 <sup>nd</sup> , 2010	Quarter 3 <sup>rd</sup> , 2010
MW-63-18	0.14	0.09	-0.10	-0.37	0.09	0.32	-0.08	-0.64	0.02	-	-	-	-	-
MW-63-34	0.51	0.19	-0.09	-0.40	0.13	0.05	-0.13	-0.74	0.18	-	-	-	-	-
MW-63-50	0.86	0.29	-0.38	-1.03	-0.47	-0.55	-1.24	-2.08	-0.45	-	-	-	-	-
MW-63-91	1.16	0.48	-0.19	-0.87	-0.25	-0.16	-0.88	NA	-0.01	-	-	-	-	-
MW-63-93	NA	0.55	-0.20	-0.87	-0.30	-0.30	-0.98	-1.68	-0.13	-	-	-	-	-
MW-63-112	0.03	-0.82	-1.46	-2.05	-1.69	-1.60	-2.26	-3.14	-1.45	-	-	-	-	-
MW-63-121	1.41	0.60	-0.18	-0.78	-0.24	-0.05	-1.49	-0.86	0.11	-	-	-	-	-
MW-63-163	0.70	-0.09	-0.83	-1.48	-0.86	-0.50	-1.54	-2.46	-0.98	-	-	-	-	-
MW-63-174	0.88	0.05	-0.65	-1.29	-0.62	-0.61	-1.19	-1.97	-0.59	-	-	-	-	-
MW-65-48	NA	NA	NA	NA	38.69	43.22	NA	48.19	36.98	40.08	38.06	39.94	42.26	59.97
MW-65-80	NA	NA	NA	NA	34.97	32.95	32.72	33.71	33.30	33.79	32.81	33.69	33.98	49.35
MW-66-21	0.26	0.17	-0.22	-0.74	0.05	0.17	0.29	-0.33	0.50	0.52	0.10	-0.01	1.82	1.05
MW-66-36	0.81	0.48	-0.04	-0.51	0.35	0.15	0.10	-0.86	0.51	-	-	-0.43	1.75	1.49
MW-67-39	NA	1.02	0.34	-0.33	0.36	0.41	-0.02	-0.07	-0.56	0.81	-1.25	-0.76	-0.13	-0.09
MW-67-105	NA	1.39	0.61	-0.04	0.57	0.65	0.16	-0.67	-0.43	-	-	-	-	-
MW-67-173	NA	0.75	-0.14	-0.83	-0.28	-0.26	-0.82	-1.62	-1.55	-	-	-	-	-
MW-67-219	NA	0.74	-0.19	-0.91	-0.32	-0.32	-0.86	-1.87	-1.59	-	-	-	-	-
MW-67-276	NA	1.61	0.60	-0.13	0.46	0.41	-0.14	-1.03	-0.91	-	-	-	-	-
MW-67-323	NA	0.18	-0.96	-1.75	-1.13	-1.35	-1.93	-2.86	-2.73	-	-	-	-	-
MW-67-340	NA	0.63	-0.52	-1.31	-0.87	-0.96	-1.56	-2.42	-2.40	-0.76	-3.27	-2.63	-2.26	-1.97
MW-107	116.85	113.87	117.48	121.79	118.94	115.00	115.72	120.28	117.52	-	-	-	-	-
MW-108	9.58	8.61	8.77	9.98	10.07	NA	9.02	9.65	9.26	-	-	-	-	-
MW-109	9.52	6.80	7.22	9.50	7.82	7.82	7.88	NA	4.95	-	-	-	-	-
MW-111	9.56	9.65	9.74	10.74	11.24	9.74	10.87	10.87	9.47	-	-	-	-	-
OUT-1	NA	1.31	1.16	0.76	0.81	NA	NA	NA	1.08	-	-0.77	1.02	5.06	NA
RW-1	NA	NA	30.15	NA	30.04	29.52	29.05	29.10	NA	-	-	-	-	-
EL-CSS	NA	8.98	NA	NA	15.11	15.39	NA	20.46	13.80	-	-	-	-	-
U3-1	NA	4.20	NA	NA	NA	NA	NA	NA	NA	-	-	-	-	-
U3-2	NA	5.34	NA	NA	NA	NA	NA	NA	NA	-	-	-	-	-
U3-3	7.53	6.52	6.63	8.57	9.25	8.25	8.94	9.13	7.29	-	-	-	-	-
U3-ID	4.25	NA	3.35	3.22	2.74	3.49	3.41	3.75	3.41	-	-	-	-	-
U3-4S	3.91	4.13	3.80	3.74	3.97	4.31	3.81	4.01	4.23	-	-	-	-	-
U3-C1	NA	1.64	3.58	3.36	0.99	2.36	0.81	0.64	1.92	2.43	0.12	2.98	NA	-
U3-T1	4.51	4.12	3.67	3.99	3.86	4.33	3.69	3.83	4.12	-	-	-	-	-
U3-T2	4.33	4.02	3.79	4.20	3.94	4.28	3.76	4.05	4.20	-	-	-	-	-

Notes:  
 NA = Data Not Available  
 1. Quarter 2 groundwater elevations were measured on 6/1/07 at 6:20 am.  
 2. Quarter 3 groundwater elevations were measured on 9/25/07 at 4:32 am.  
 3. Quarter 4, 2007 groundwater elevations were measured on 12/9/07 at 4:15 am.  
 4. Quarter 1, 2008 groundwater elevations were measured on 1/3/08 at 1:14 a.m.  
 5. Quarter 2, 2008 groundwater elevations were measured on 4/4/08 at 5:14 pm.  
 6. Quarter 3, 2008 groundwater elevations were measured on 7/10/08 at 11:35 am.  
 7. Quarter 4, 2008 groundwater elevations were measured on 11/11/08 at 2:54 am.  
 8. Quarter 1, 2009 groundwater elevations were measured on 1/9/09 at 2:42 am.  
 9. Quarter 2, 2009 groundwater elevations were measured on 5/22/09 at 2:41 pm.  
 10. Quarter 3, 2009 groundwater elevations were measured on 8/9/09 at 8:18 am.  
 11. Subsequent to Quarter 2, 2009, as described in our June 14, 2010 memorandum which was included as Appendix J in the Quarter 1, 2009 Report, a reduced number of transducers will be maintained in long term operation. The rationale for this reduced transducer redeployment is included in the June 14, 2010 memorandum.  
 12. MW-32 groundwater elevations from 2<sup>nd</sup> quarter, 2007 were based on an initial Waterloo Multi-Level configuration, which was subsequently reconfigured, initial depth intervals approximately corresponding to current configuration are listed in parentheses. The current configuration intervals MW-32-48 and MW-32-173 have no representative equivalent within the old configuration.  
 13. Quarter 4, 2009 groundwater elevations were measured on 11/28/09 at 3:45 pm.  
 14. Quarter 1, 2010 groundwater elevations were measured on 1/30/10 at 6:00 am.  
 15. Quarter 2, 2010 groundwater elevations were measured on 4/09/10 at 12:06 pm.  
 16. Quarter 3, 2010 groundwater elevations were measured on 7/31/10 at 12:30 am.

















TABLE 6  
HISTORIC GROUNDWATER ANALYTICAL RESULTS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, TN

Table with columns: Well ID, Sample ID, Sample Zone, Sample Zone Center, Sample Zone Center Depth Below Top of casing, Sample Collection Date, Time, Analyte Results (FRITULUM, TRITOLIUM, STRONG, C-137, Co-60, MDC, Result, Std. Dev., MDC). Rows include wells MW-306-69 and MW-306-84.

117,000-B-9901726017365-60-MDC-3010125621-121414  
Table 6: Historic Groundwater Analytical Results  
Table 6:

























TABLE 5 HISTORIC GROUNDWATER ANALYTICAL RESULTS INDIAN POINT ENERGY CENTER BUCHANAN, NY

Table with columns for Well ID, Sample ID, Sample Zone, Center Depth Below Top of casing, Sample Zone Center Elevation in feet, Date, Time, and analytical results for various parameters: FRITIUM (µg/L), Sr-90 (pCi/L), Cs-137 (pCi/L), Cs-134 (pCi/L), and N-63 (pCi/L). The table includes data for wells MW-48-23, MW-48-37, MW-49-26, and MW-49-42, with multiple rows of results per well.



TABLE 6  
HISTORIC GROUNDWATER ANALYTICAL RESULTS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, TN

Table with columns: Well ID, Sample ID, Sample Zone, Sample Zone Center, Sample Zone Depth Below Top of casing, Date, Time, Sample Collection, Tritium (pCi/L), Sr-90 (pCi/L), C-137 (pCi/L), Co-60 (pCi/L), MDC, Result, MDC, Result, MDC, Result, MDC, Result, MDC, Result, Well ID.

117,000,000,1766117665,60,MC,C3,2010,F5A,C,T,USA  
Table 6: Historic Groundwater Analytical Results





TABLE 6  
HISTORIC GROUNDWATER ANALYTICAL RESULTS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID <sup>1</sup>	SAMPLE ID	SAMPLE ZONE CENTER Depth Below top of casing	SAMPLE ZONE CENTER elevation (ft)	SAMPLE COLLECTION				ANALYSIS RESULTS												Well ID <sup>1</sup>
				Date	Time	TRITIUM (pCi/L)			\$^{89}\$SR (pCi/L)			C-137 (pCi/L)			Co-60 (pCi/L)			MDC		
						Result	MDC	Unit	Result	MDC	Unit	Result	MDC	Unit	Result	MDC	Unit		Result	
MW-54120	005	10/21/2007	3:58	7.40E-03	0.92E+02	4.02E+02	3.81E+01	2.27E+00	4.23E+01	4.35E+01	3.92E+00	2.32E+01	3.15E+00	3.72E+00	7.06E+00	1.10E+01	2.38E+01	NW-54120		
	006	12/12/2008	10:53	7.48E-03	3.48E+02	1.72E+02	3.12E+01	2.00E+00	6.60E+01	1.39E+00	3.18E+00	1.11E+01	1.11E+01	3.71E+00	1.71E+01	1.82E+01	2.02E+01			
	008	10/9/08	39:5	5.91E-03	3.28E+02	1.42E+02	3.11E+01	1.73E+00	6.30E+01	1.30E+00	3.02E+00	1.08E+00	2.15E+00	2.22E+01	2.22E+01	2.38E+01	2.38E+01			
	009	10/9/08	10:15	5.80E-03	3.66E+02	1.91E+02	3.03E+01	1.52E+00	5.71E+01	1.59E+00	3.04E+00	1.15E+01	2.33E+00	3.20E+00	1.92E+01	1.30E+01	2.11E+01			
	010	10/9/08	39:5	5.70E-03	5.90E+02	5.07E+02	3.34E+01	1.92E+00	4.10E+01	3.34E+01	4.41E+00	7.78E+00	1.51E+00	1.94E+01	1.94E+01	3.88E+01	3.88E+01			
	011	10/9/08	39:5	5.07E-03	2.59E+02	1.66E+02	2.53E+01	2.02E+00	3.00E+01	2.73E+00	5.78E+00	0.00E+00	1.50E+02	4.20E+00	1.12E+01	1.60E+01	1.93E+01			
	012	10/9/08	39:5	5.07E-03	3.29E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	013	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	014	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	015	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
MW-54137	001	10/21/2007	3:58	7.40E-03	0.92E+02	4.02E+02	3.81E+01	2.27E+00	4.23E+01	4.35E+01	3.92E+00	2.32E+01	3.15E+00	3.72E+00	7.06E+00	1.10E+01	2.38E+01			
	002	12/12/2008	10:53	7.48E-03	3.48E+02	1.72E+02	3.12E+01	2.00E+00	6.60E+01	1.39E+00	3.18E+00	1.11E+01	1.11E+01	3.71E+00	1.71E+01	1.82E+01	2.02E+01			
	004	10/9/08	39:5	5.91E-03	3.28E+02	1.42E+02	3.11E+01	1.73E+00	6.30E+01	1.30E+00	3.02E+00	1.08E+00	2.15E+00	2.22E+01	2.22E+01	2.38E+01	2.38E+01			
	005	10/9/08	10:15	5.80E-03	3.66E+02	1.91E+02	3.03E+01	1.52E+00	5.71E+01	1.59E+00	3.04E+00	1.15E+01	2.33E+00	3.20E+00	1.92E+01	1.30E+01	2.11E+01			
	006	10/9/08	39:5	5.70E-03	5.90E+02	5.07E+02	3.34E+01	1.92E+00	4.10E+01	3.34E+01	4.41E+00	7.78E+00	1.51E+00	1.94E+01	1.94E+01	3.88E+01	3.88E+01			
	007	10/9/08	39:5	5.07E-03	2.59E+02	1.66E+02	2.53E+01	2.02E+00	3.00E+01	2.73E+00	5.78E+00	0.00E+00	1.50E+00	4.20E+00	1.12E+01	1.60E+01	1.93E+01			
	008	10/9/08	39:5	5.07E-03	3.29E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	009	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	010	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	MW-54158	001	10/21/2007	3:58	7.40E-03	0.92E+02	4.02E+02	3.81E+01	2.27E+00	4.23E+01	4.35E+01	3.92E+00	2.32E+01	3.15E+00	3.72E+00	7.06E+00	1.10E+01	2.38E+01		
002		12/12/2008	10:53	7.48E-03	3.48E+02	1.72E+02	3.12E+01	2.00E+00	6.60E+01	1.39E+00	3.18E+00	1.11E+01	1.11E+01	3.71E+00	1.71E+01	1.82E+01	2.02E+01			
004		10/9/08	39:5	5.91E-03	3.28E+02	1.42E+02	3.11E+01	1.73E+00	6.30E+01	1.30E+00	3.02E+00	1.08E+00	2.15E+00	2.22E+01	2.22E+01	2.38E+01	2.38E+01			
005		10/9/08	10:15	5.80E-03	3.66E+02	1.91E+02	3.03E+01	1.52E+00	5.71E+01	1.59E+00	3.04E+00	1.15E+01	2.33E+00	3.20E+00	1.92E+01	1.30E+01	2.11E+01			
006		10/9/08	39:5	5.70E-03	5.90E+02	5.07E+02	3.34E+01	1.92E+00	4.10E+01	3.34E+01	4.41E+00	7.78E+00	1.51E+00	1.94E+01	1.94E+01	3.88E+01	3.88E+01			
007		10/9/08	39:5	5.07E-03	2.59E+02	1.66E+02	2.53E+01	2.02E+00	3.00E+01	2.73E+00	5.78E+00	0.00E+00	1.50E+00	4.20E+00	1.12E+01	1.60E+01	1.93E+01			
008		10/9/08	39:5	5.07E-03	3.29E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
009		10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
010		10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
MW-54144		001	10/21/2007	3:58	7.40E-03	0.92E+02	4.02E+02	3.81E+01	2.27E+00	4.23E+01	4.35E+01	3.92E+00	2.32E+01	3.15E+00	3.72E+00	7.06E+00	1.10E+01	2.38E+01		
	002	12/12/2008	10:53	7.48E-03	3.48E+02	1.72E+02	3.12E+01	2.00E+00	6.60E+01	1.39E+00	3.18E+00	1.11E+01	1.11E+01	3.71E+00	1.71E+01	1.82E+01	2.02E+01			
	004	10/9/08	39:5	5.91E-03	3.28E+02	1.42E+02	3.11E+01	1.73E+00	6.30E+01	1.30E+00	3.02E+00	1.08E+00	2.15E+00	2.22E+01	2.22E+01	2.38E+01	2.38E+01			
	005	10/9/08	10:15	5.80E-03	3.66E+02	1.91E+02	3.03E+01	1.52E+00	5.71E+01	1.59E+00	3.04E+00	1.15E+01	2.33E+00	3.20E+00	1.92E+01	1.30E+01	2.11E+01			
	006	10/9/08	39:5	5.70E-03	5.90E+02	5.07E+02	3.34E+01	1.92E+00	4.10E+01	3.34E+01	4.41E+00	7.78E+00	1.51E+00	1.94E+01	1.94E+01	3.88E+01	3.88E+01			
	007	10/9/08	39:5	5.07E-03	2.59E+02	1.66E+02	2.53E+01	2.02E+00	3.00E+01	2.73E+00	5.78E+00	0.00E+00	1.50E+00	4.20E+00	1.12E+01	1.60E+01	1.93E+01			
	008	10/9/08	39:5	5.07E-03	3.29E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	009	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	010	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			
	011	10/9/08	39:5	5.07E-03	3.28E+02	1.72E+02	4.25E+01	3.02E+00	6.74E+01	3.25E+01	2.28E+00	1.50E+00	1.50E+00	4.20E+00	1.12E+01	2.02E+01	2.21E+01			

117.000.00 8901726017265.60.MDC.Co-60.CS.2010.FS&A.C1164A  
Table 6-Batch: Groundwater Analytical Results















TABLE 6  
HISTORIC GROUNDWATER ANALYTICAL RESULTS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, TN

Well ID <sup>1</sup>	SAMPLE ID	SAMPLE CENTER Depth Below top of casing	SAMPLE ZONE CENTER elevation in feet	SAMPLE COLLECTION				ANALYSIS RESULTS															Well ID <sup>2</sup>												
				Date	Time	TRITIUM (pCi/L)				\$^89\$SR (pCi/L)					C-137 (pCi/L)					Co-60 (pCi/L)															
						Result	Sol. Dev.	MDC	Result	Result	Sol. Dev.	MDC	Result	Sol. Dev.	MDC	Result	Sol. Dev.	MDC	Result	Sol. Dev.	MDC	Result		Sol. Dev.	MDC										
						416E-02	511E-02	177E+02	318E+01	645E+01	7.0E+01	3.02E-02	4.90E+00	-2.88E+01	5.31E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00		4.92E+00	4.92E+00	4.92E+00									
NW-65121	012	121	-108.7	2/8/2010	13:18	416E-02	511E-02	177E+02	318E+01	645E+01	7.0E+01	3.02E-02	4.90E+00	-2.88E+01	5.31E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	4.92E+00	NW-65121	
NW-65169	001	121	-108.7	6/26/2010	12:59	608E-02	180E+02	146E+02	417E+01	609E+01	6.7E+01	6.02E-01	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	NW-65169	
NW-65174	001	121	-108.7	5/15/2007	11:58	479E-02	210E+02	173E+02	367E+01	503E+01	6.5E+01	5.03E-01	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	5.03E+00	NW-65174	
NW-65248	001	121	-108.7	7/25/2007	12:00	238E-02	194E+02	197E+02	295E+01	421E+01	5.99E+01	5.99E-01	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	5.99E+00	NW-65248	
NW-65250	001	121	-108.7	10/11/2007	14:18	349E-02	165E+02	173E+02	264E+01	503E+01	6.7E+01	6.7E-01	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	NW-65250
NW-65251	001	121	-108.7	2/22/2009	14:18	481E-02	240E+02	197E+02	345E+01	471E+01	6.7E+01	6.7E-01	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	6.7E+00	NW-65251
NW-6636	001	33.6	-19.5	3/9/2010	13:57	107E+03	201E+02	128E+02	172E+02	387E+01	531E+01	5.31E-01	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	5.31E+00	NW-6636
NW-6739	001	38.3	-25.8	8/31/2007	12:45	486E-03	443E+02	124E+02	186E+01	260E+01	3.43E+01	3.43E-01	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	3.43E+00	NW-6739
NW-68174	001	38.3	-25.8	7/25/2008	15:58	417E-03	375E+02	192E+02	271E+01	369E+01	4.11E+01	4.11E-01	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	4.11E+00	NW-68174
NW-683174	001	38.3	-25.8	7/28/2008	14:07	318E-03	266E+02	171E+02	162E+01	116E+01	1.60E+01	1.60E-01	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	1.60E+00	NW-683174
NW-68421	001	38.3	-25.8	12/7/2009	16:15	267E-03	291E+02	192E+02	192E+01	262E+01	3.04E+01	3.04E-01	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	3.04E+00	NW-68421

Table 5-Bucarc Groundwater Analytical Results









TABLE 5  
HISTORIC GROUNDWATER ANALYTICAL RESULTS  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY

Well ID <sup>1</sup>	SAMPLE ID	SAMPLE ZONE CENTER, depth below top of casing	SAMPLE ZONE CENTER, elevation (ft amsl) <sup>2</sup>	SAMPLE COLLECTION					ANALYSIS RESULTS												
				Date	Time	Result	TRITIUM (pCi/L)			SR-90 (pCi/L)			C-137 (pCi/L)			Co-60 (pCi/L)			N-63 (pCi/L)	MDC	Well ID <sup>1</sup>
							Sat. Lev.	MDC	Result	Sat. Lev.	MDC	Result	Sat. Lev.	MDC	Result	Sat. Lev.	MDC	Result			
	011			8/30/2010	13:50	9.96E+03	5.48E+02	1.24E+02	1.75E+01	3.71E+01	3.81E+01	1.50E+00	5.58E+00	6.48E+00	8.08E+01	7.50E+00	NA	NA	NE-3-V-2FD		
	012			9/16/2010	15:20	8.80E+02	1.89E+02	1.83E+02	3.40E+01	6.25E+01	7.11E+01	7.21E+01	6.43E+00	7.14E+00	1.23E+00	5.71E+00	6.83E+00	NA	NA	NA	
	001	LAE-002		6/6/2006	12:47	5.20E+01	1.71E+02	1.82E+02	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	LAE-002		
	003			5/19/2006	13:14	4.71E+01	1.50E+02	1.70E+02	5.88E+01	9.50E+01	1.07E+00	6.45E+02	9.95E+00	1.59E+00	1.34E+01	1.34E+01	2.13E+01	2.34E+01	NA		
	004			12/22/2006	13:36	1.23E+01	1.62E+02	1.64E+02	-1.20E+01	7.80E+00	1.60E+00	NA	NA	NA	NA	NA	NA	NA	6.10E+00		
	005			3/7/2007	14:55	5.33E+01	1.56E+02	1.30E+02	8.20E+01	1.50E+00	1.60E+00	3.10E+00	4.85E+00	5.10E+00	1.20E+00	5.40E+00	7.20E+00	NA	NA		
	006			6/7/2007	13:18	5.83E+00	1.31E+02	1.54E+02	3.19E+01	5.02E+01	5.02E+01	3.60E+00	2.63E+00	3.04E+00	6.53E+01	2.92E+00	3.94E+00	NA	NA		
	007			8/16/2007	14:50	4.81E+00	1.46E+02	1.46E+02	4.80E+01	4.30E+00	4.30E+00	4.30E+00	4.30E+00	4.30E+00	4.30E+00	4.30E+00	4.30E+00	NA	NA		
	008			12/22/2007	16:50	8.00E+01	1.46E+02	1.44E+02	4.80E+01	6.02E+01	6.02E+01	3.49E+00	3.49E+00	3.49E+00	3.49E+00	3.49E+00	3.49E+00	NA	NA		
	009			4/16/2008	8:00	4.63E+01	1.44E+02	1.44E+02	4.75E+01	3.03E+01	4.68E+01	1.91E+00	2.13E+00	3.93E+00	1.61E+00	2.46E+00	4.56E+00	NA	NA		
	010			10/17/2008	10:32	8.19E+01	1.53E+02	1.74E+02	4.05E+01	5.70E+01	6.01E+01	2.48E+01	2.78E+00	3.16E+00	3.18E+00	3.09E+00	3.46E+00	NA	NA		
	011			4/21/2009	14:54	1.80E+02	1.77E+02	1.85E+02	1.77E+01	5.70E+01	6.58E+01	4.74E+00	5.94E+00	3.96E+00	3.17E+01	4.50E+00	4.50E+00	1.92E+01	2.19E+01		
	012			11/19/2009	12:53	7.51E+01	1.40E+02	1.62E+02	-1.84E+02	5.43E+01	7.29E+01	4.01E+01	8.91E+00	1.02E+01	6.99E+00	9.31E+00	1.27E+00	2.20E+00	1.68E+01		
	013			5/11/2010	13:54	4.21E+01	1.24E+02	1.89E+02	6.35E+01	7.71E+01	7.78E+01	4.40E+00	5.90E+00	7.60E+00	1.04E+00	6.08E+00	7.44E+00	NA	NA		
	001	E-1		6/29/2007	12:55	7.93E+02	2.07E+02	1.89E+02	-3.83E+01	6.71E+01	9.80E+01	0.00E+00	7.00E+00	4.44E+00	9.13E+01	3.30E+00	3.40E+00	NA	E-1		
	002			8/14/2007	11:20	1.10E+03	2.25E+02	1.90E+02	-1.29E+02	5.93E+01	7.38E+01	1.68E+00	6.71E+00	3.92E+00	9.94E+01	3.54E+00	4.16E+00	NA	NA		
	003			10/21/2007	14:49	1.10E+03	4.68E+02	4.01E+02	-1.56E+01	3.72E+01	5.31E+01	1.68E+00	5.83E+00	3.82E+00	1.33E+00	3.23E+00	3.53E+00	NA	NA		
	004			1/22/2008	13:08	2.27E+02	1.61E+02	1.71E+02	1.29E+01	5.00E+01	6.12E+01	3.13E+01	3.54E+00	2.83E+00	9.46E+02	2.72E+00	3.01E+00	NA	NA		
	005			4/18/2008	18:55	1.17E+03	1.57E+02	2.01E+02	-1.14E+01	3.81E+01	3.81E+01	2.00E+01	3.70E+00	3.07E+00	-2.88E+01	1.70E+00	2.97E+00	NA	NA		
	006			5/3/2009	13:50	8.81E+02	1.83E+02	1.62E+02	7.01E+02	7.89E+01	9.15E+01	9.21E+00	1.11E+01	7.41E+00	3.23E+00	6.23E+00	5.86E+00	NA	NA		
	007			2/22/2010	14:10	4.49E+03	2.13E+02	1.69E+02	4.61E+02	3.04E+01	3.88E+01	4.52E+00	5.43E+00	6.44E+00	4.69E+01	7.14E+00	5.88E+00	NA	NA		
	008			5/17/2010	15:50	3.11E+02	6.34E+02	1.85E+02	2.79E+02	5.50E+01	5.03E+01	3.92E+00	7.91E+00	5.33E+00	5.33E+00	6.24E+00	7.14E+00	7.14E+00	NA	NA	
	009			5/17/2010	15:50	6.04E+02	6.34E+02	1.85E+02	2.79E+02	5.50E+01	5.03E+01	3.92E+00	7.91E+00	5.33E+00	5.33E+00	6.24E+00	7.14E+00	7.14E+00	NA	NA	
	010			8/17/2007	9:50	4.09E+02	1.67E+02	1.66E+02	1.81E+02	4.97E+01	4.77E+01	5.79E+00	3.46E+00	4.88E+00	1.89E+00	3.81E+00	4.15E+00	NA	NA		
	002			8/17/2007	8:20	5.46E+01	1.63E+02	1.93E+02	3.94E+01	6.20E+01	8.33E+01	5.43E+01	3.97E+00	3.13E+00	3.58E+06	2.31E+00	2.53E+00	NA	NA		
	003			10/21/2007	11:20	1.07E+02	1.70E+02	1.90E+02	-2.43E+02	4.31E+01	8.31E+01	3.92E+00	3.07E+00	3.13E+00	1.01E+00	2.16E+00	3.03E+00	NA	NA		
	004			11/6/2008	16:50	4.23E+02	2.04E+02	1.59E+02	1.05E+01	7.91E+01	8.81E+01	3.98E+00	4.41E+00	3.32E+00	1.29E+00	3.15E+00	3.66E+00	NA	NA		
	005			6/22/2008	14:15	5.33E+01	8.45E+00	1.43E+02	1.20E+01	2.59E+01	5.55E+01	1.96E+00	1.96E+00	3.24E+00	-7.50E+01	3.43E+00	4.21E+00	NA	NA		
	006			6/3/2009	9:40	1.08E+02	1.46E+02	1.62E+02	1.71E+01	7.88E+01	8.14E+01	1.50E+01	1.19E+01	7.94E+01	1.26E+01	5.79E+00	6.80E+00	NA	NA		
	007			2/19/2010	9:56	3.78E+02	1.65E+02	1.65E+02	1.34E+02	3.57E+01	4.59E+01	1.43E+01	4.33E+00	4.84E+00	2.21E+01	2.96E+00	4.84E+00	NA	NA		
	008			5/18/2010	9:40	4.48E+01	1.62E+02	1.84E+02	-1.02E+01	4.47E+01	5.71E+01	5.99E+01	5.58E+00	6.34E+00	2.39E+01	5.30E+00	6.27E+00	NA	NA		
	009			8/3/2010	13:53	1.49E+02	1.62E+02	1.75E+02	1.12E+01	8.02E+01	9.78E+01	2.32E+01	6.57E+00	8.03E+00	-9.21E+02	8.23E+00	9.33E+00	NA	NA		

Note:

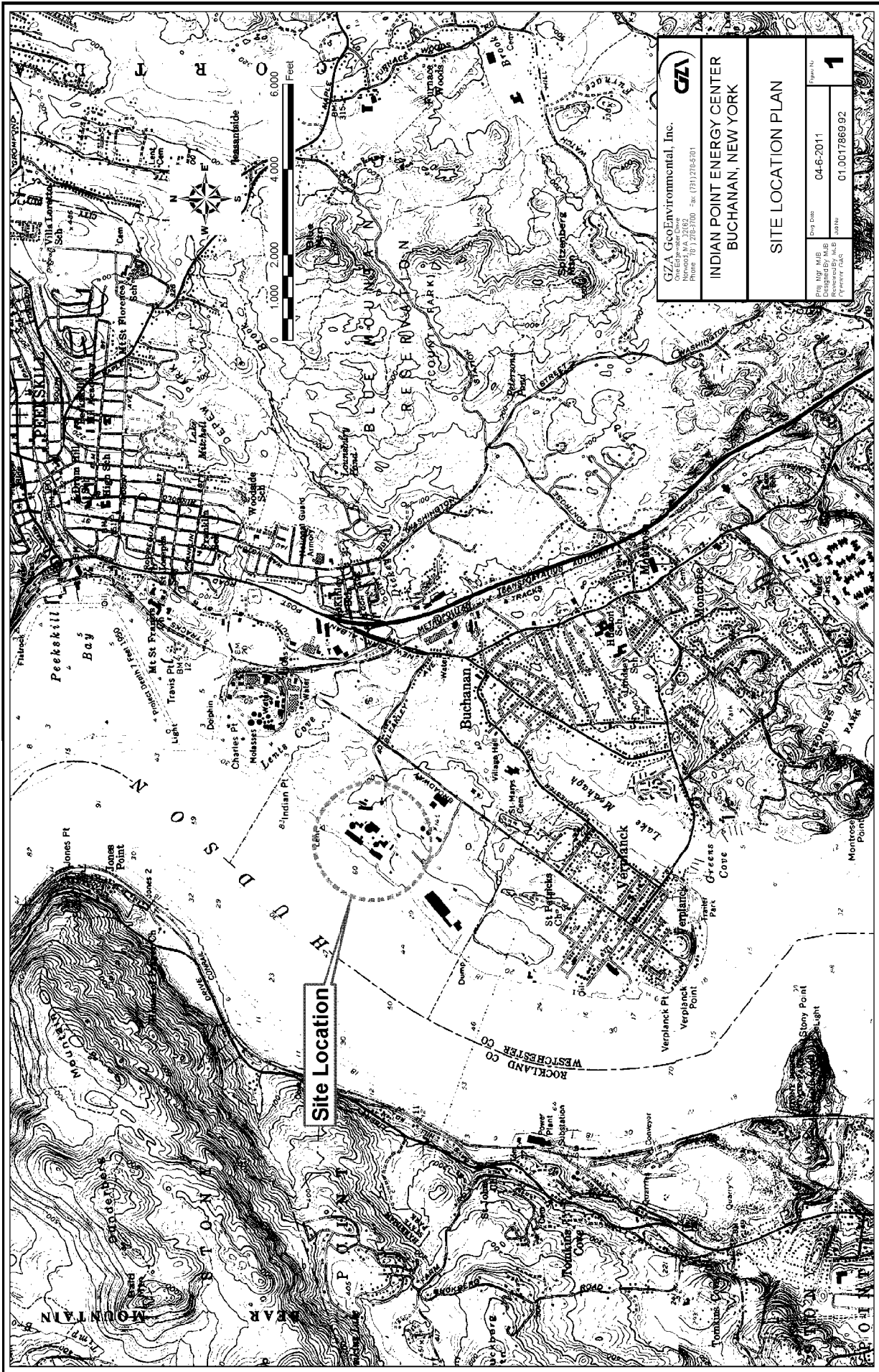
- For unfiltered multi-level conformance wells, mix of well ID indicators (depth, location to nearest foot) from reference point on casing to bottom of well screen. For Water-co multi-level systems, indicate the depth (rounded to nearest foot) from reference point on casing to top of sampling zone. Well ID's without a suffix are open bedrock wells.
- Sampling depth: when sampling intervals (because of pump intake) have been established at location of monitoring system, refer to the exact pump intake.
- Current well identification are shown for each location. Minor name changes have been made based on altered transducer installation.
- Original well identification are shown for each location. Minor name changes have been made based on altered transducer installation.
- Dehydration services sampling interval is positioned within overburden with. Open box indicates sampling interval is in a back-log.
- Monitoring well 73571, sample ID: 019 E, 019 D, and 319 S were collected for laboratory and field QA/QC (B-E) in duplicate. S-Sample. Only one sample result is included in this calculation for drilling averages.
- These locations are from drawdown monitoring wells.






## FIGURES

- Figure 1 Site Location Plan**
- Figure 2 Site Plan**
- Figure 3 Lower Hudson Valley Geologic Map**
- Figure 4 3<sup>rd</sup> Quarter 2010 Current and Potential Future SSC Source Locations**
- Figure 5A 3<sup>rd</sup> Quarter 2010 Longterm Transducer Monitoring Evaluation Map**
- Figure 6 3<sup>rd</sup> Quarter 2010 Rolling Average Tritium Activity Map**
- Figure 6A Temporal Trends in Unit 2 Rolling Average Tritium Activity Maps**
- Figure 6B Unit 2 Leak Collection Device Evaluation 3<sup>rd</sup> Quarter 2010**
- Figure 7 3<sup>rd</sup> Quarter 2010 Rolling Average Strontium-90 Activity Map**
- Figure 7A Sr-90 Baseline Analysis–Unit 1 Defueling Evaluation 3<sup>rd</sup> Quarter 2010**
- Figure 8 3<sup>rd</sup> Quarter 2010 Rolling Average Cesium, Cobalt, and Nickel Activity Map**

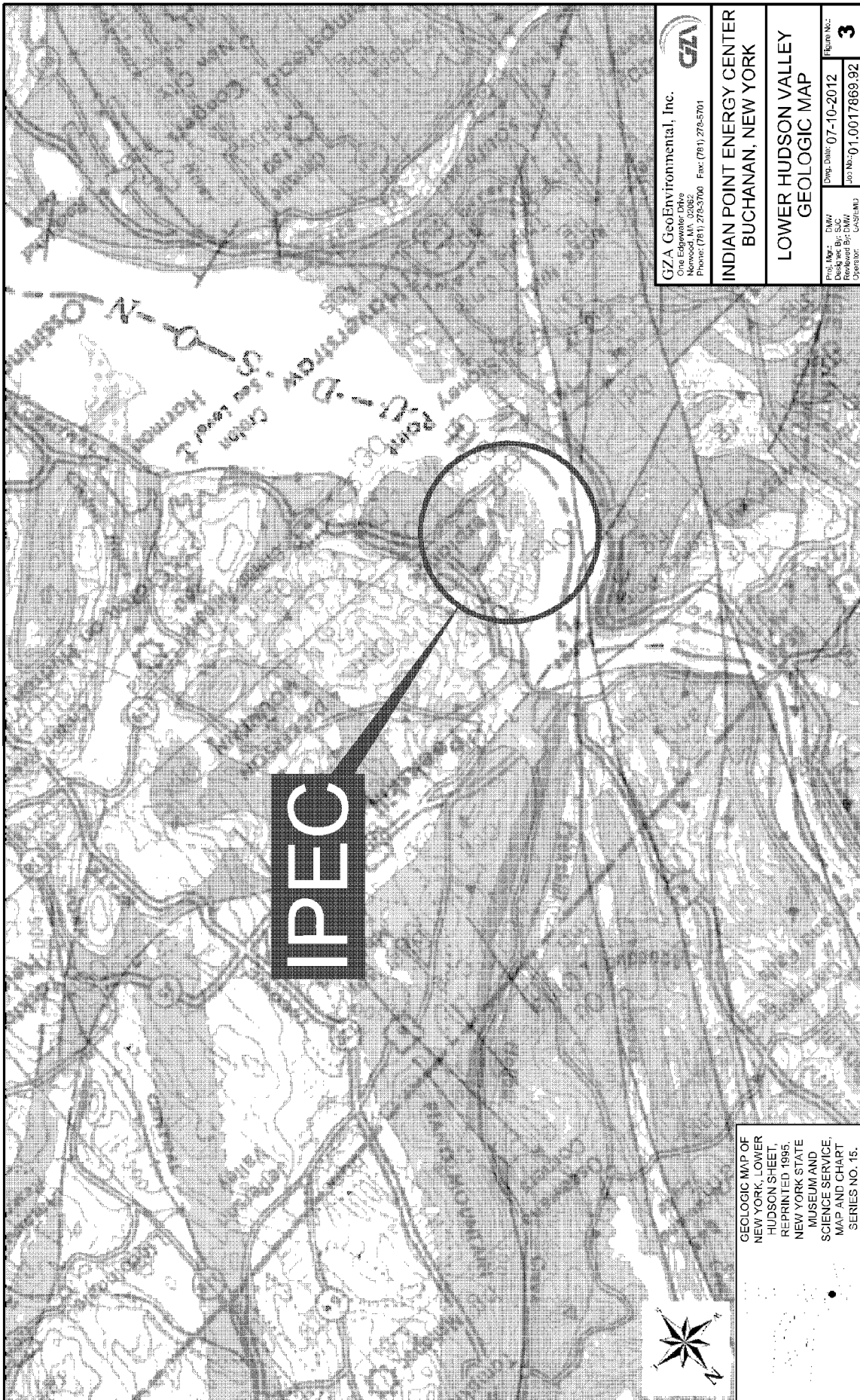


 <b>GZA GeoEnvironmental, Inc.</b> 110 West 19th Street New York, NY 10011 Phone: 212-693-3700 Fax: 212-693-3701	
<b>INDIAN POINT ENERGY CENTER</b> <b>BUCHANAN, NEW YORK</b>	
<b>SITE LOCATION PLAN</b>	
Project No. 04-G-2011	Sheet No. <b>1</b>
Date 01/01/2011	Revision 01/01/2011

**Site Location**

© 2011 - GZA GeoEnvironmental, Inc. - 117,000-18,999/17968/17969-91 MG/figures/GIS/MXD Documents/03\_2010/11-04-05 F01 Site Location Plan 17969-92 - FINAL.mxd, 4/6/2011, 3:54:29 PM, gregory.scott





**IPEC**

GZA GeoEnvironmental, Inc.  
 One Edgewater Drive  
 Woodstock, NY 12424  
 Project: (781) 275-3700 Fax: (781) 275-5701

**INDIAN POINT ENERGY CENTER  
 BUCHANAN, NEW YORK**

**LOWER HUDSON VALLEY  
 GEOLOGIC MAP**

Proj. No.: DMW	Figure No.:
Design By: S.C.	07-10-2012
Operator: CAS/MD	01.0017869.92
	<b>3</b>

GEOLOGIC MAP OF  
 NEW YORK, LOWER  
 HUDSON SHEET,  
 REPRINTED, 1985  
 NEW YORK STATE  
 MUSEUM AND  
 SCIENCE SERVICE,  
 MAP AND CHART  
 SERIES NO. 45.

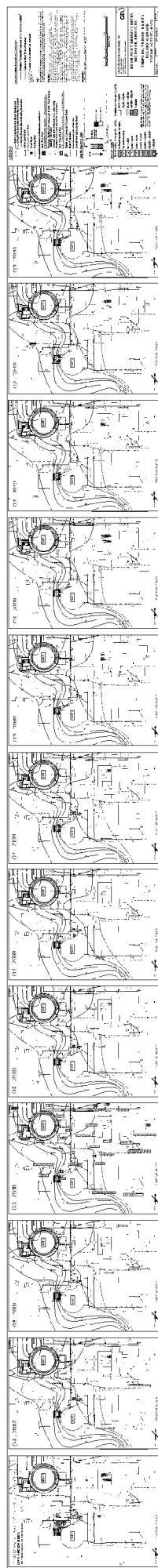


GZA--C:\17,000--18,999\17869-92\17869-92\Figures\G001\302010\12-07-10\_F03\_Lower Hudson Valley Geologic Map\_17869-92.ewg [Fig-3] July 10, 2012 - 3:17pm eblinc.donohue



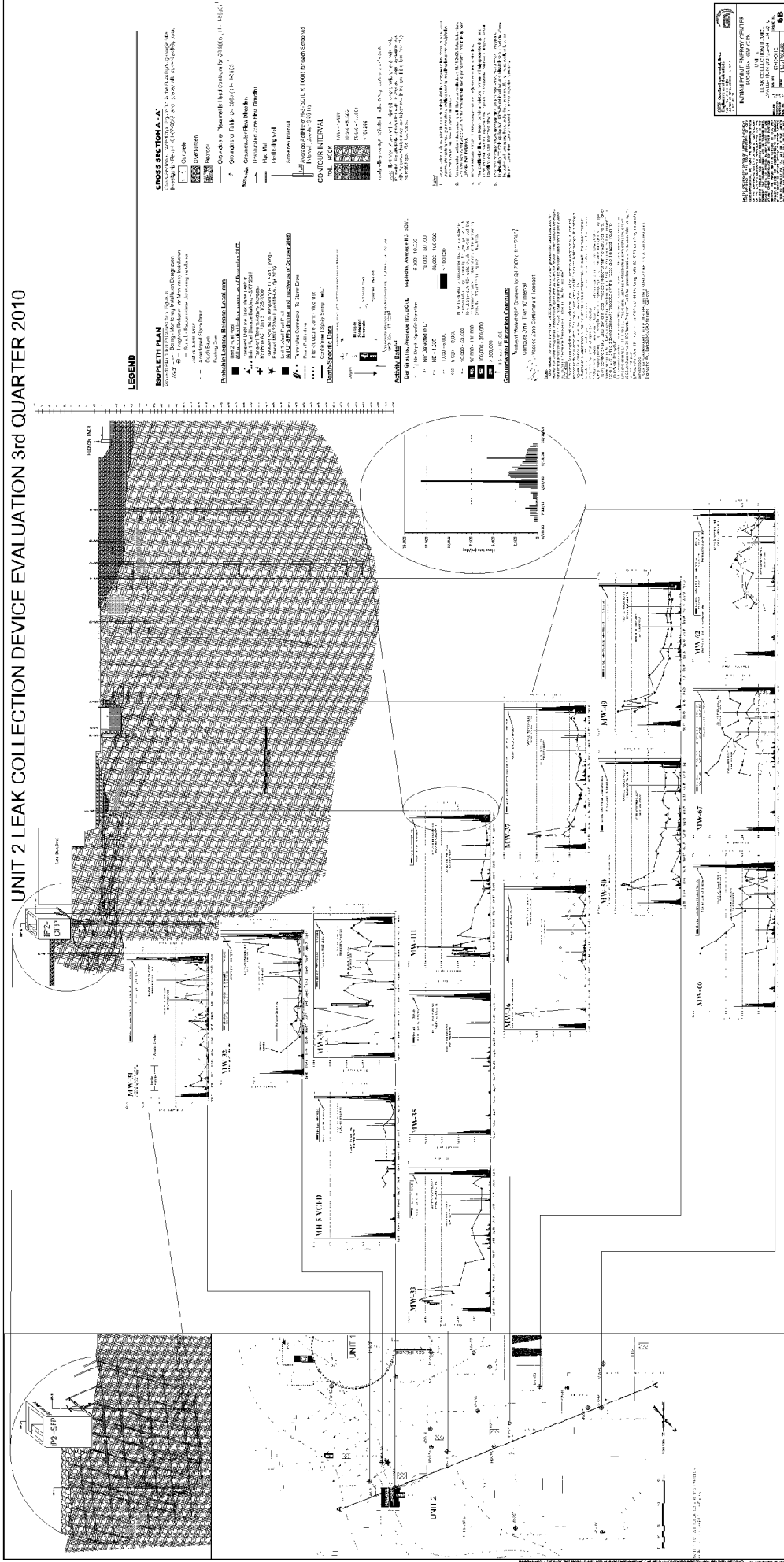








UNIT 2 LEAK COLLECTION DEVICE EVALUATION 3rd QUARTER 2010



**UNIT 2 LEAK COLLECTION DEVICE EVALUATION 3rd QUARTER 2010**  
 PROJECT NO. 10-00000000-0000  
 DATE: 10/15/10  
 SCALE: 1" = 10'

**MONITORING WELL DATA**  
 MW-31: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-32: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-33: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-34: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-35: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-36: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-37: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-38: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-39: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-40: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-41: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]  
 MW-42: [Graph showing water level fluctuations between 100 and 150 feet from 10/1/10 to 10/31/10]









## APPENDIX A LIMITATIONS

## **HYDROGEOLOGICAL LIMITATIONS**

1. The conclusions and recommendations submitted in this report are based in part upon the radiological, chemical and physical data from water analyses. These data were obtained from specific sampling locations at specific times. The full nature and extent of variations in the data between these specific locations and times are not known. The conditions existing between these specific locations and times have only been inferred using interpolation and extrapolation based on judgment.
2. The subsurface profiles described in the text and presented in the report figures are intended to convey anticipated trends in subsurface conditions. The conditions shown are approximate and generalized and were developed, in part, based on judgment. For specific information at specific locations, refer to the individual subsurface investigation logs.
3. Water level readings (piezometric pressures) have been made in the specific borings, monitoring wells, and Waterloo installations at times and under conditions stated. These data have been reviewed and interpretations have been made in the text and on the figures of this report. However, it must be noted that temporal and spatial fluctuations in the level of the groundwater may occur due to variations in rainfall and other factors different from those prevailing at the time and location measurements were made.
4. Where quantitative laboratory testing has been conducted by an outside laboratory, GZA has relied upon the validity of the data provided, and has not conducted an independent laboratory evaluation of the reliability of these data.
5. Radiological and chemical analyses have been performed for specific parameters during the course of this study, as summarized in the text. Additional constituents not searched for may be present in soil and groundwater at the site.
6. Variations in the types and concentrations of contaminants and variations in their flow paths may occur due to seasonal water table fluctuations, past and current plant operational practices, the passage of time, and other factors. Should additional data (water analyses, water elevations, subsurface deposits, plant construction and operation, etc.) become available in the future, these data should be reviewed by GZA, and the conclusions and recommendations presented herein modified accordingly.
7. This monitoring report was developed by GZA GeoEnvironmental Inc for the exclusive of Entergy Nuclear Northeast (Entergy) at the Indian Point Energy Center. Any use of data or information provided in the report, by parties other than Entergy, is prohibited without the prior written permission of Entergy and GZA.



## **APPENDIX B TRANSDUCER INSTALLATION LOGS**

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	U3-4Dn
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

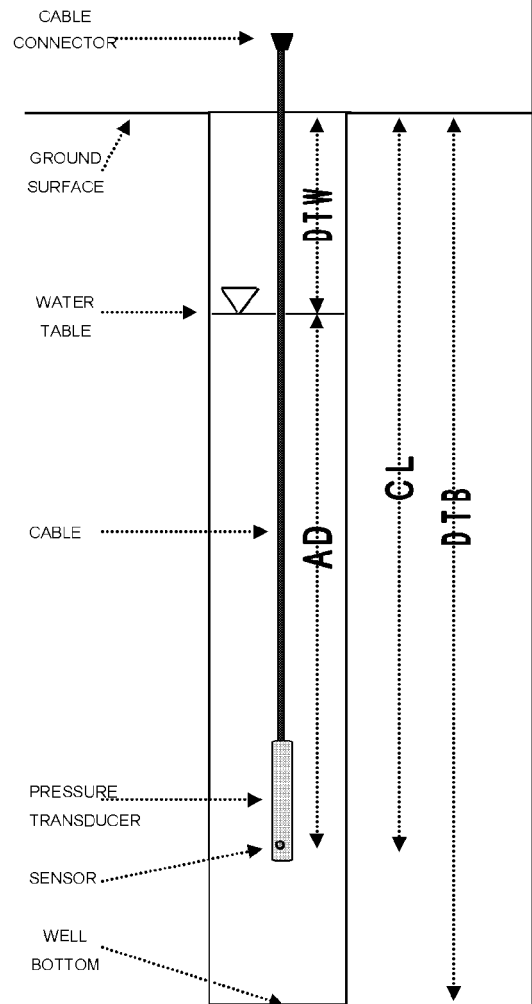
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>27.25</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.849</u>	DATE	<u>7/23/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>14.519</u>		
SERIAL NUMBER	<u>14301</u>	CASING DIAMETER (INCH)	<u>4</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>4.37</u>
	<u>S. Lee</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>27.25</u>	FT
GROUND ELEVATION:	<u>14.849</u>	FT M.S.L.
CASING ELEVATION:	<u>14.519</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.330</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>10:06</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>10.15</u>	FT
ACTUAL DEPTH:	<u>+ 50.874</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 61.024</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>14.519</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 10.15</u>	FT
REFERENCE ELEVATION:	<u>= 4.369</u>	FT M.S.L.
TEST NAME:	<u>U3-4Dn</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>10:06</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES: Difference 0.332. Reset.



**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	HR-1 #2n
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

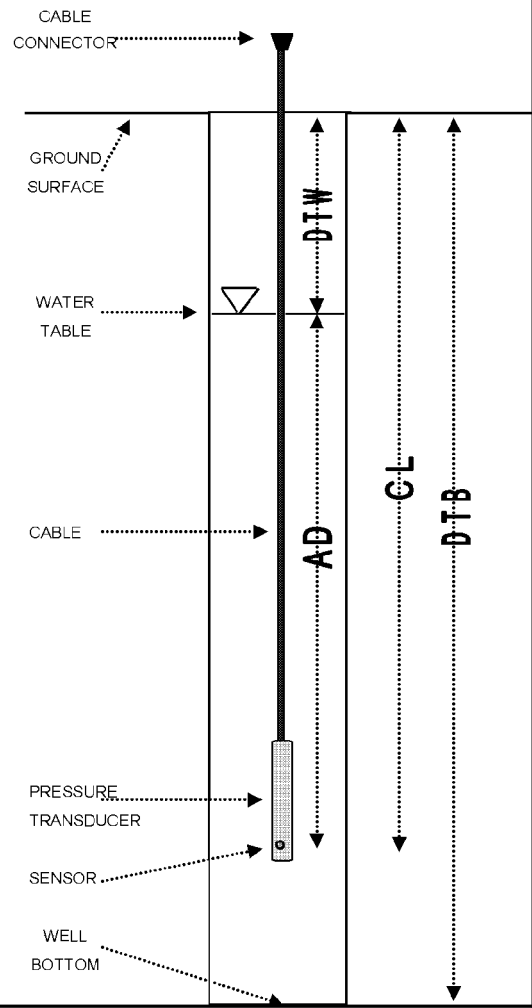
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>--</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.99</u>	DATE	<u>8/4/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.50</u>		
SERIAL NUMBER	<u>9401</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>0.78</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>--</u>	FT
GROUND ELEVATION:	<u>14.99</u>	FT M.S.L.
CASING ELEVATION:	<u>18.50</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.50</u>	FT
MEASURED CABLE LENGTH	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>14:17</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>17.72</u>	FT
ACTUAL DEPTH:	<u>+ -8.563</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 9.157</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.50</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 17.72</u>	FT
REFERENCE ELEVATION:	<u>= 0.78</u>	FT M.S.L.
TEST NAME:	<u>HR-1#2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>14:18</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES: Difference -0.649. Reset.

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	HR-1
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

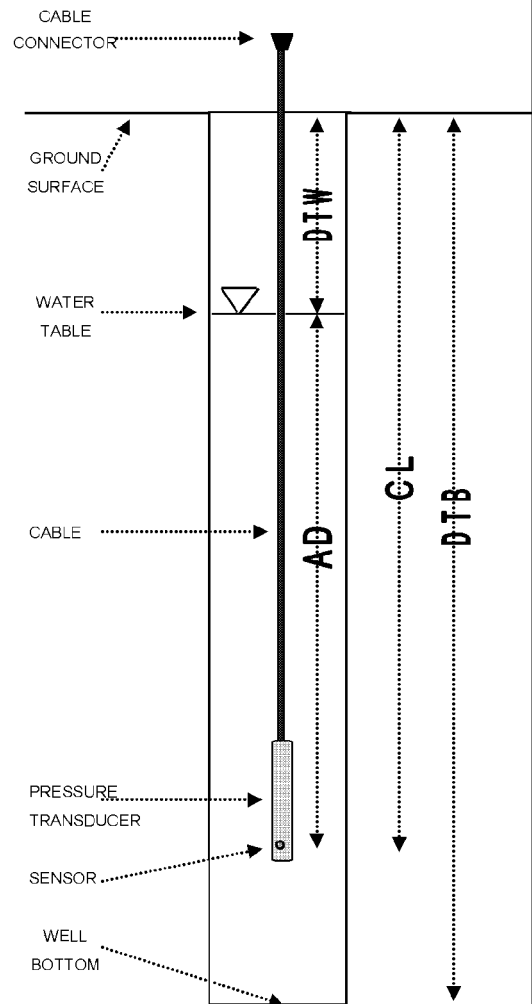
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>--</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.99</u>	DATE	<u>8/13/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.50</u>		
SERIAL NUMBER	<u>9401</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>3.85</u>
	<u>M. Britos</u>		

**ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)**

**DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)**

DEPTH TO BOTTOM:	<u>--</u>	FT
GROUND ELEVATION:	<u>14.99</u>	FT M.S.L.
CASING ELEVATION:	<u>18.50</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.50</u>	FT
MEASURED CABLE LENGTH	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>14:38</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>14.65</u>	FT
ACTUAL DEPTH:	<u>+ 7.517</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 22.167</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.50</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 14.65</u>	FT
REFERENCE ELEVATION:	<u>= 3.85</u>	FT M.S.L.
TEST NAME:	<u>HR-1#2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>14:38</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:  
 Pull out non-vented transducer, 16593.  
 Install transducer 9401, taken from U3-4S.  
 Install new batteries.  
 Start new test.

**GZA** WELL ID: HR-1

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-36-24
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

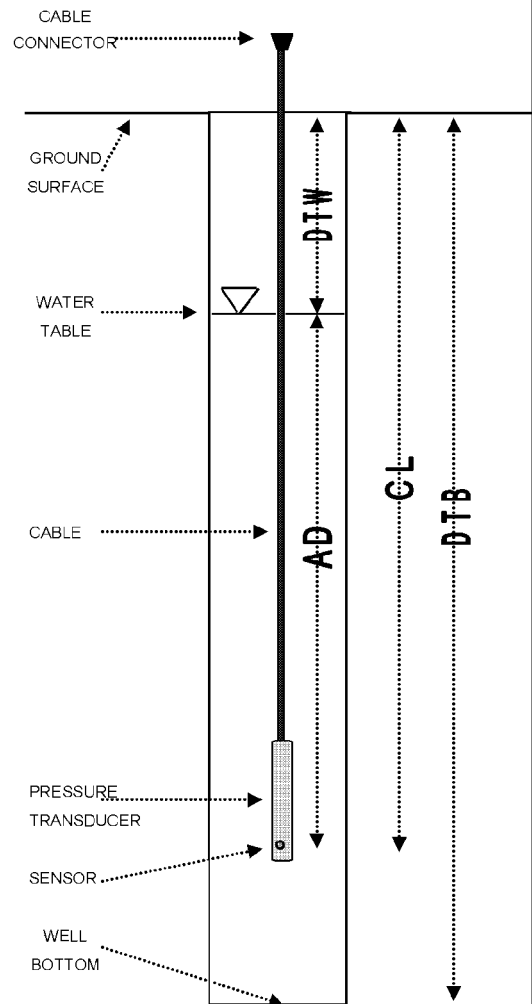
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>54.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>11.799</u>	DATE	<u>7/29/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>11.598</u>		
SERIAL NUMBER	<u></u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>11.60</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>24.00</u>	FT
GROUND ELEVATION:	<u>11.799</u>	FT M.S.L.
CASING ELEVATION:	<u>11.598</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.201</u>	FT
	<u>--</u>	FT
TIME OF MEASUREMENT:	<u></u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u></u>	FT
ACTUAL DEPTH:	<u>+</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 0.000</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>11.598</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 0.00</u>	FT
REFERENCE ELEVATION:	<u>= 11.598</u>	FT M.S.L.
TEST NAME:	<u>MW-36-24</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u></u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-41-40
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

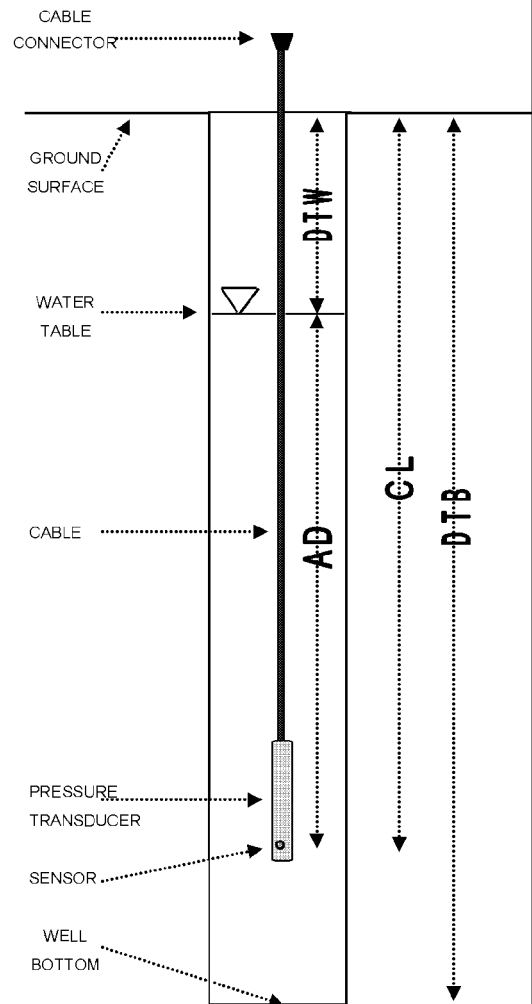
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>64.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>54.87</u>	DATE	<u>7/21/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>54.13</u>		
SERIAL NUMBER	<u>6321</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>29.83</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>40.00</u>	FT
GROUND ELEVATION:	<u>54.87</u>	FT M.S.L.
CASING ELEVATION:	<u>54.13</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.74</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>08:56</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>24.30</u>	FT
ACTUAL DEPTH:	<u>+ 41.584</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 65.884</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>54.13</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 24.30</u>	FT
REFERENCE ELEVATION:	<u>= 29.83</u>	FT M.S.L.
TEST NAME:	<u>MW-41-40</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>08:56</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

### TRANSDUCER INSTALLATION LOG

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	Entergy Indian Point Energy Center	WELL ID	MW-41-40
			SHEET	1 of 1
			FILE NO.	01.0017869.92
			PROJECT LOCATION	Indian Point

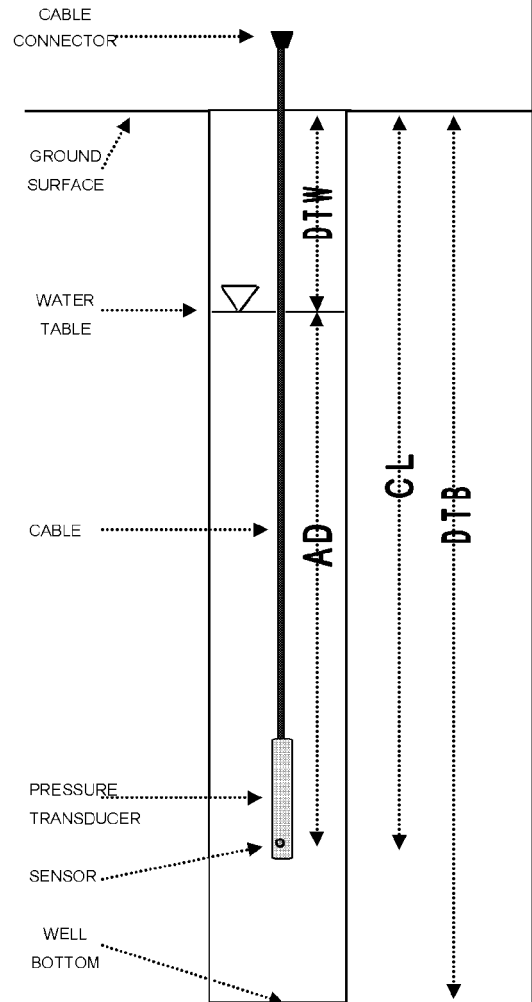
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>64.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>54.87</u>	DATE	<u>7/21/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>54.13</u>		
SERIAL NUMBER	<u>6321</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u> <u>M. Britos</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>29.82</u>
--------------	---	---	--------------

**ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)**

**DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)**

DEPTH TO BOTTOM:	<u>40.00</u>		FT	
GROUND ELEVATION:	<u>54.87</u>		FT M.S.L.	
CASING ELEVATION:	<u>54.13</u>		FT M.S.L.	
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>			
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.74</u>		FT	
MEASURED CABLE LENGTH:	<u>--</u>		FT	
TIME OF MEASUREMENT:	<u>09:11</u>		HRS	
MEASUREMENT TAKEN FROM:	<u>TOC</u>			
DEPTH TO WATER:	<u>24.31</u>		FT	
ACTUAL DEPTH:	<u>+</u>		FT	
THEORETICAL CABLE LENGTH:	<u>=</u>	<u>24.310</u>		FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>		check	
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>		check	
ELEVATION OF MEASURING POINT:	<u>54.13</u>		FT M.S.L.	
DEPTH TO WATER:	<u>-</u>	<u>24.31</u>		FT
REFERENCE ELEVATION:	<u>=</u>	<u>29.82</u>		FT M.S.L.
TEST NAME:	<u>MW-41-40</u>			
LOGGING INTERVAL:	<u>20</u>		MIN	
TEST START TIME:	<u>09:11</u>		HRS	



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-41-63
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

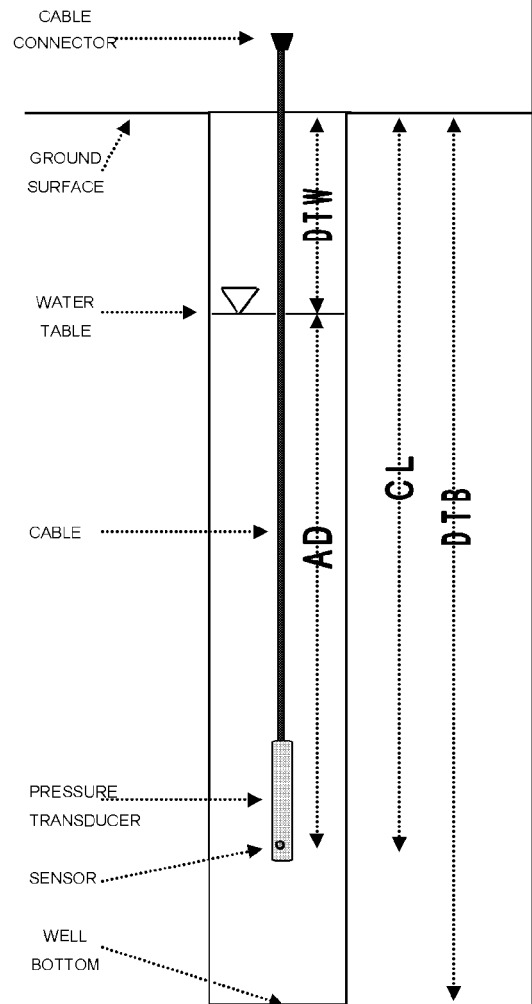
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>64.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>54.87</u>	DATE	<u>7/21/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>54.13</u>		
SERIAL NUMBER	<u>5977</u>	CASING DIAMETER (INCH)	<u>1</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>26.61</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>63.00</u>	FT
GROUND ELEVATION:	<u>54.87</u>	FT M.S.L.
CASING ELEVATION:	<u>54.13</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.74</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>08:39</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>27.52</u>	FT
ACTUAL DEPTH:	<u>+ 13.879</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 41.399</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>54.13</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 27.52</u>	FT
REFERENCE ELEVATION:	<u>= 26.61</u>	FT M.S.L.
TEST NAME:	<u>MW-41-63</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>08:39</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-43-28
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

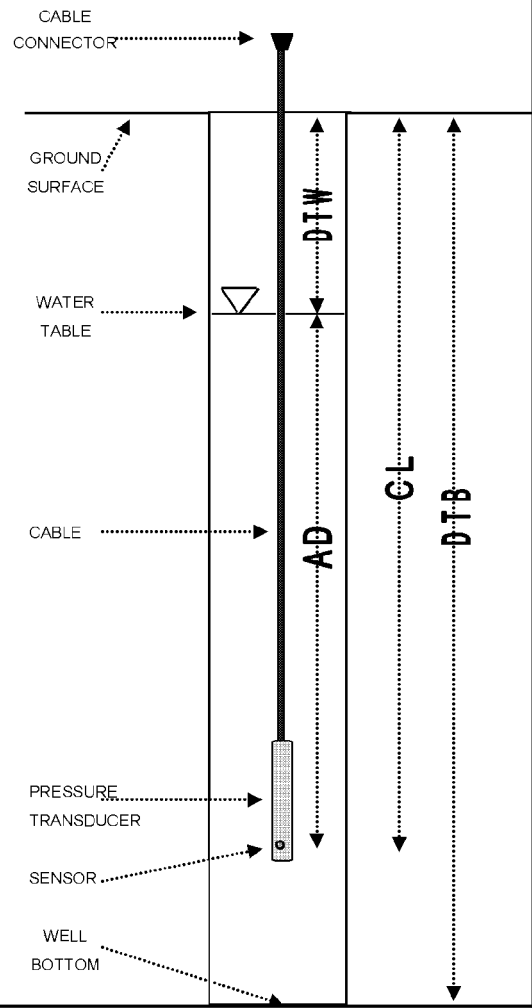
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>63.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>48.760</u>	DATE	<u>7/20/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>48.021</u>		
SERIAL NUMBER	<u>11331</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>32.28</u>
	<u>M Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>28.00</u>	FT
GROUND ELEVATION:	<u>48.760</u>	FT M.S.L.
CASING ELEVATION:	<u>48.021</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.739</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>10:01</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>15.74</u>	FT
ACTUAL DEPTH:	<u>+ 22.965</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 38.705</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>48.021</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 15.74</u>	FT
REFERENCE ELEVATION:	<u>= 32.281</u>	FT M.S.L.
TEST NAME:	<u>MW-43-28</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>10:01</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-43-28
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

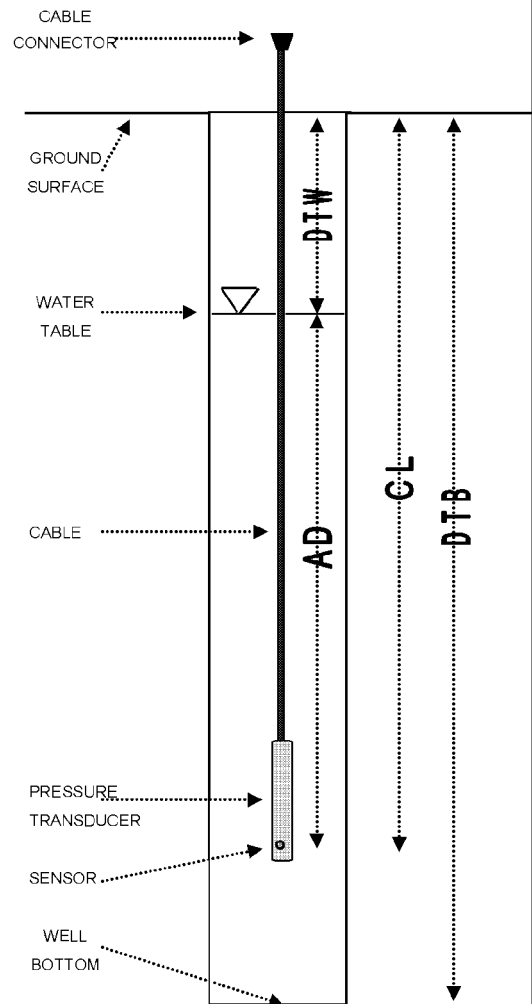
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>63.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>48.760</u>	DATE	<u>8/19/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>48.021</u>		
SERIAL NUMBER	<u>11331</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>32.13</u>
	<u>M Britos</u>		

**ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)**

**DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)**

DEPTH TO BOTTOM:	<u>28.00</u>	FT
GROUND ELEVATION:	<u>48.760</u>	FT M.S.L.
CASING ELEVATION:	<u>48.021</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.739</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>12:12</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>15.89</u>	FT
ACTUAL DEPTH:	<u>+ 22.973</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 38.863</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>48.021</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 15.89</u>	FT
REFERENCE ELEVATION:	<u>= 32.131</u>	FT M.S.L.
TEST NAME:	<u>MW-43-28</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>12:12</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:  
 Off by 2.902. Reset.  
 Test was ended at 11:57, transducer clock read 15:43:57 am  
 Reset clock.

<b>GZA</b>	WELL ID:	MW-43-28
------------	----------	----------



**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-43-62
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

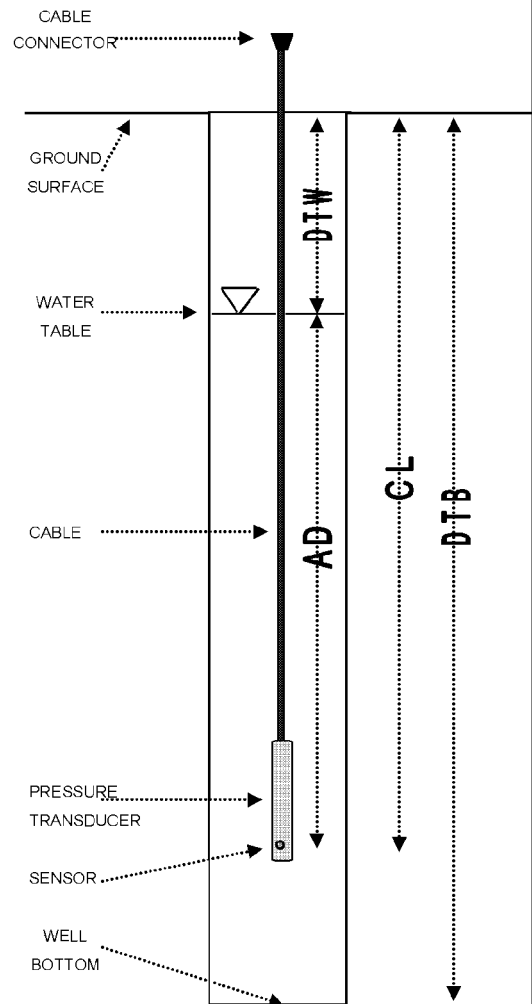
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>63.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>48.761</u>	DATE	<u>7/20/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>47.821</u>		
SERIAL NUMBER	<u>16236</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>29.83</u>
	<u>M Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>63.00</u>	FT
GROUND ELEVATION:	<u>48.761</u>	FT M.S.L.
CASING ELEVATION:	<u>47.821</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.940</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>10:21</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>17.99</u>	FT
ACTUAL DEPTH:	<u>+ 33.730</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 51.720</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>47.821</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 17.99</u>	FT
REFERENCE ELEVATION:	<u>= 29.831</u>	FT M.S.L.
TEST NAME:	<u>MW-43-62</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>10:21</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	Entergy Indian Point Energy Center	WELL ID	MW-44-67
			SHEET	1 of 1
			FILE NO.	01.0017869.92
			PROJECT LOCATION	Indian Point

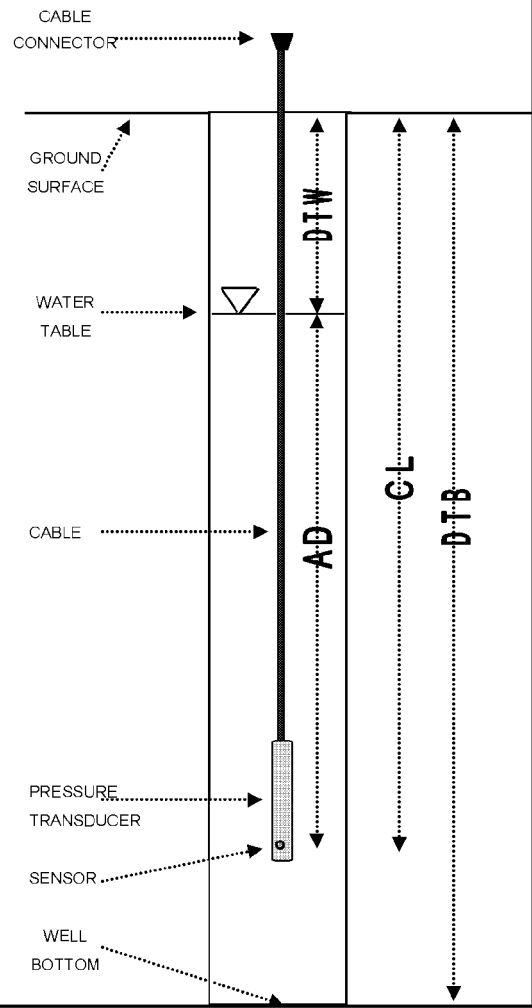
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>105.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>93.52</u>	DATE	<u>7/22/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>93.02</u>		
SERIAL NUMBER	<u></u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>33.30</u>
	<u>M Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>67.00</u>	FT
GROUND ELEVATION:	<u>93.52</u>	FT M.S.L.
CASING ELEVATION:	<u>93.02</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>0.50</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>09:54</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>59.72</u>	FT
ACTUAL DEPTH:	<u></u>	FT
THEORETICAL CABLE LENGTH:	<u>= 59.720</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>93.02</u>	FT M.S.L.
DEPTH TO WATER:	<u>= 59.72</u>	FT
REFERENCE ELEVATION:	<u>= 33.30</u>	FT M.S.L.
TEST NAME:	<u>MW-44-67</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>09:54</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-50-42
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

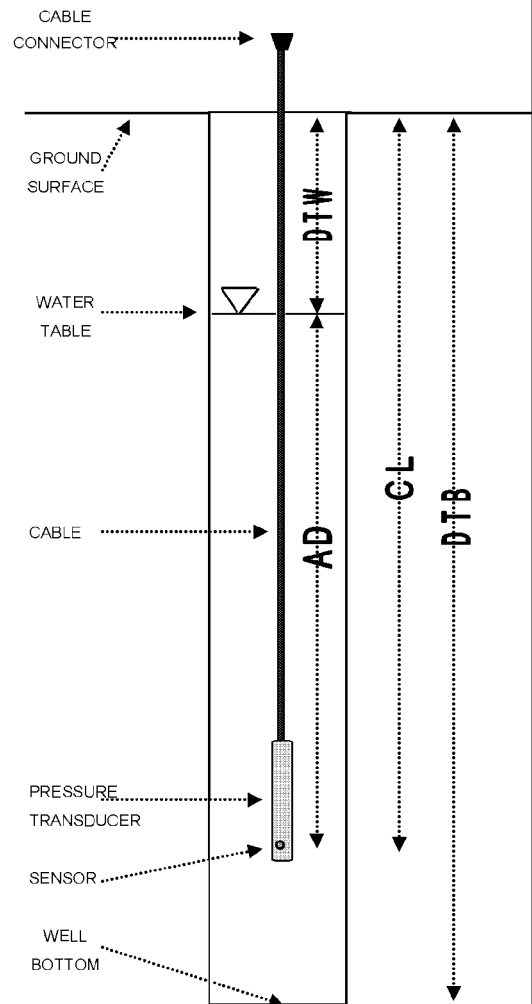
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>67.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.92</u>	DATE	<u>8/4/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>14.45</u>		
SERIAL NUMBER	<u></u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>6.05</u>
	<u>M. Britos</u>		

**ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)**

**DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)**

DEPTH TO BOTTOM:	<u>42.00</u>	FT
GROUND ELEVATION:	<u>14.92</u>	FT M.S.L.
CASING ELEVATION:	<u>14.45</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.47</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>13:42</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>8.40</u>	FT
ACTUAL DEPTH:	<u>+ 32.575</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 40.975</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>14.45</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 8.40</u>	FT
REFERENCE ELEVATION:	<u>= 6.05</u>	FT M.S.L.
TEST NAME:	<u>MW-50-42</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>13:42</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:  
 no connection. Replaced batteries. New test started.

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW65-80
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

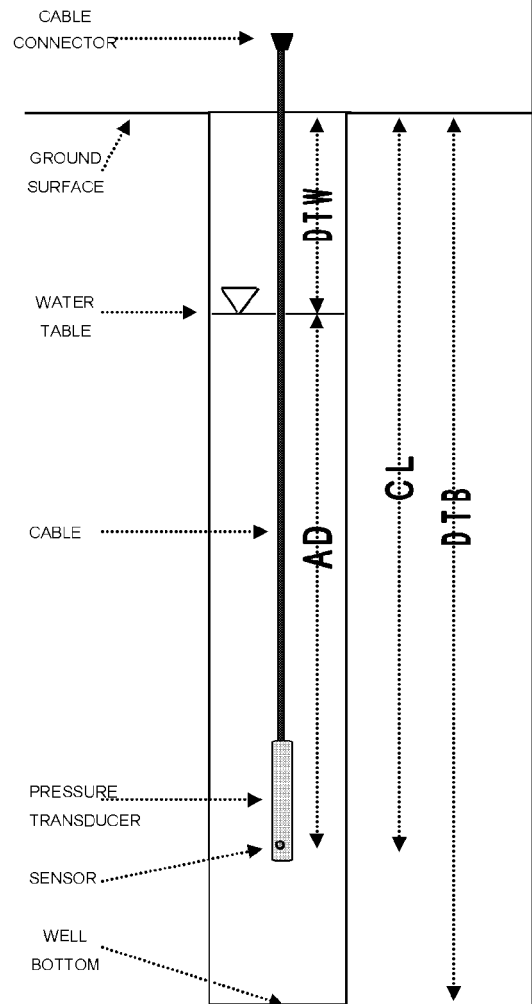
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>80.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>69.723</u>	DATE	<u>8/18/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>68.841</u>		
SERIAL NUMBER	<u>8264</u>	CASING DIAMETER (INCH)	<u>1</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>32.54</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>80.00</u>	FT
GROUND ELEVATION:	<u>69.723</u>	FT M.S.L.
CASING ELEVATION:	<u>68.841</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.882</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>13:59</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>36.30</u>	FT
ACTUAL DEPTH:	<u>+ 19.375</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 55.675</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>68.841</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 36.30</u>	FT
REFERENCE ELEVATION:	<u>= 32.541</u>	FT M.S.L.
TEST NAME:	<u>MW65-80</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>13:59</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:  
 Off by 16.249. reset.

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	MW-66-21
	Entergy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

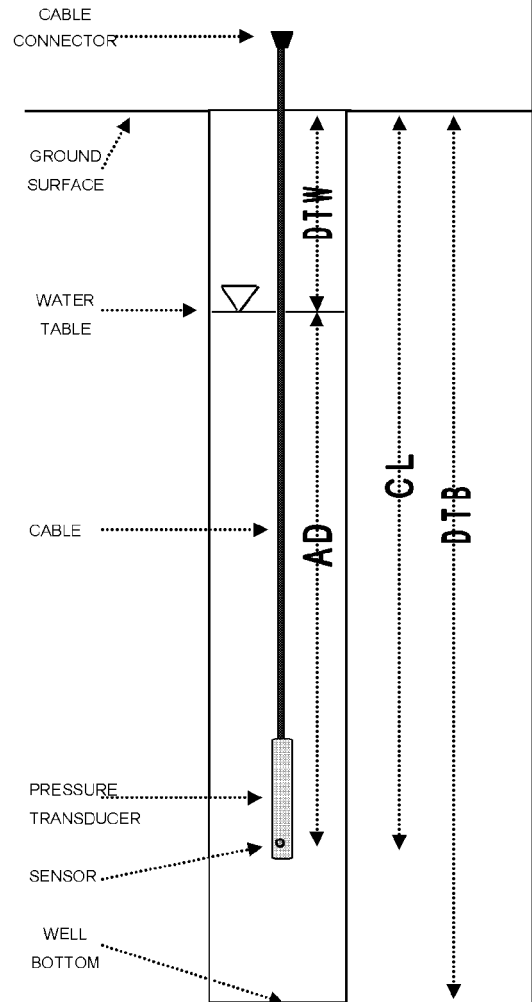
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>37.00</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>14.122</u>	DATE	<u>8/19/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>13.407</u>		
SERIAL NUMBER	<u>15849</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>1.44</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>21.00</u>	FT
GROUND ELEVATION:	<u>14.122</u>	FT M.S.L.
CASING ELEVATION:	<u>13.407</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>below</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>-0.72</u>	FT
MEASURED CABLE LENGTH	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>13:21</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>11.97</u>	FT
ACTUAL DEPTH:	<u>+ 8.05</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 20.02</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>13.407</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 11.97</u>	FT
REFERENCE ELEVATION:	<u>= 1.437</u>	FT M.S.L.
TEST NAME:	<u>MW-66-21</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>13:21</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES: Off by 0.571.

### TRANSDUCER INSTALLATION LOG

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client <b>Entergy</b> Indian Point Energy Center	WELL ID SHEET FILE NO. PROJECT LOCATION	OUT-1 1 of 1 01.0017869.92 Indian Point
---	--	--	--

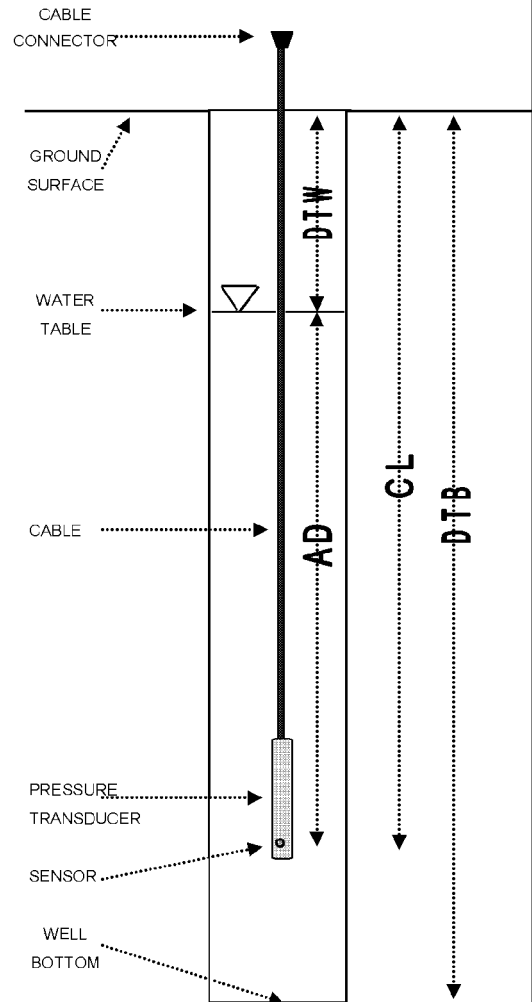
MANUFACTURER MAKE PSI CAPACITY SERIAL NUMBER	In-Situ MiniTroll 30 _____	FINAL BORING DEPTH (FT) GROUND ELEVATION (FT) CASING ELEVATION (FT) CASING DIAMETER (INCH)	-- 8.20 11.89 2	DATUM DATE	NGVD 29 8/11/10
---	-------------------------------------	---	--------------------------	---------------	--------------------

GZA ENGINEER C. Benmergui M. Britos	STATIC GROUNDWATER TABLE ELEVATION (FT)	2.95
---	---	------

**ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)**

**DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)**

<b>DEPTH TO BOTTOM:</b> <b>GROUND ELEVATION:</b> <b>CASING ELEVATION:</b> <b>CASING ABOVE (+) OR BELOW (-) GROUND:</b> <b>DISTANCE FROM CASING TO GROUND (+ OR -):</b> <b>MEASURED CABLE LENGTH:</b>	-- 8.20 11.89 above 3.69 --	FT FT M.S.L. FT M.S.L. FT FT	
<b>TIME OF MEASUREMENT:</b> <b>MEASUREMENT TAKEN FROM:</b>	15:54 TOC	HRS	
<b>DEPTH TO WATER:</b> <b>ACTUAL DEPTH:</b> <b>THEORETICAL CABLE LENGTH:</b>	8.94 + 8.735 = 17.675	FT FT FT	
<b>HAVE CLOCKS BEEN SYNCHRONIZED?</b> <b>IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?</b>	<input checked="" type="checkbox"/> <input checked="" type="checkbox"/>	check check	
<b>ELEVATION OF MEASURING POINT:</b> <b>DEPTH TO WATER:</b> <b>REFERENCE ELEVATION:</b>	11.891 - 8.940 = 2.951	FT M.S.L. FT FT M.S.L.	
<b>TEST NAME:</b> <b>LOGGING INTERVAL:</b> <b>TEST START TIME:</b>	OUT-1-n 20 15:54	MIN HRS	



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:

**GZA**

WELL ID: OUT-1

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	U3-C1
	Energy	SHEET	1 of 1
	Indian Point Energy Center	FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

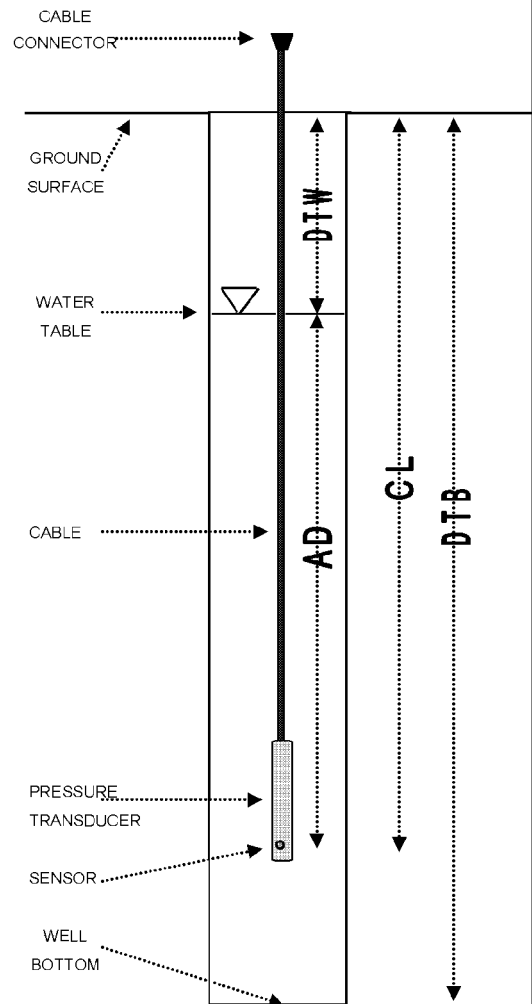
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>NA</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>15.003</u>	DATE	<u>8/19/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.060</u>		
SERIAL NUMBER	<u>5548</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>2.76</u>
	<u>M. Britos</u>		

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>NA</u>	FT
GROUND ELEVATION:	<u>15.003</u>	FT M.S.L.
CASING ELEVATION:	<u>18.060</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.057</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>14:47</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>15.30</u>	FT
ACTUAL DEPTH:	<u>+ 11.314</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 26.614</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.060</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 15.30</u>	FT
REFERENCE ELEVATION:	<u>= 2.760</u>	FT M.S.L.
TEST NAME:	<u>U3-C1</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>14:47</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:  
 Off by -2.359. Reset.

**TRANSDUCER INSTALLATION LOG**

<b>GZA GEOENVIRONMENTAL OF NEW YORK</b> 440 NINTH AVENUE, 18th FLOOR NEW YORK, NEW YORK 10001 SCIENTISTS AND ENGINEERS	Client	WELL ID	U3-C1-2
	Entergy Indian Point Energy Center	SHEET	1 of 1
		FILE NO.	01.0017869.92
		PROJECT LOCATION	Indian Point

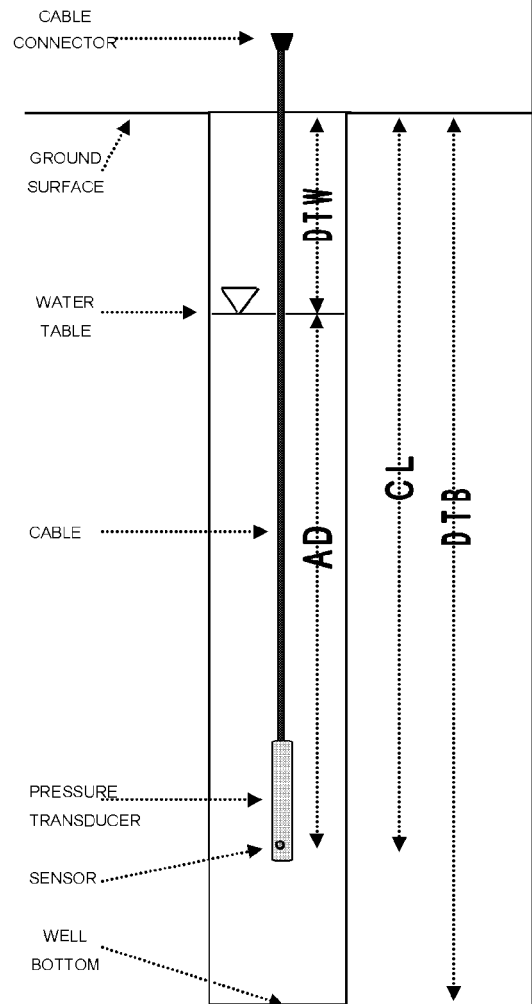
MANUFACTURER	<u>In-Situ</u>	FINAL BORING DEPTH (FT)	<u>NA</u>	DATUM	<u>NGVD 29</u>
MAKE	<u>MiniTroll</u>	GROUND ELEVATION (FT)	<u>15.003</u>	DATE	<u>8/19/10</u>
PSI CAPACITY	<u>30</u>	CASING ELEVATION (FT)	<u>18.060</u>		
SERIAL NUMBER	<u>11949</u>	CASING DIAMETER (INCH)	<u>2</u>		

GZA ENGINEER	<u>C. Benmergui</u> <u>M. Britos</u>	STATIC GROUNDWATER TABLE ELEVATION (FT)	<u>2.76</u>
--------------	---	---	-------------

ELEVATION OF MEASURING POINT - DEPTH TO WATER = REFERENCE ELEVATION (WATER TABLE ELEVATION)

DEPTH TO WATER + ACTUAL DEPTH = CABLE LENGTH (if transducer is functioning properly)

DEPTH TO BOTTOM:	<u>NA</u>	FT
GROUND ELEVATION:	<u>15.003</u>	FT M.S.L.
CASING ELEVATION:	<u>18.060</u>	FT M.S.L.
CASING ABOVE (+) OR BELOW (-) GROUND:	<u>above</u>	
DISTANCE FROM CASING TO GROUND (+ OR -):	<u>3.057</u>	FT
MEASURED CABLE LENGTH:	<u>--</u>	FT
TIME OF MEASUREMENT:	<u>14:47</u>	HRS
MEASUREMENT TAKEN FROM:	<u>TOC</u>	
DEPTH TO WATER:	<u>15.30</u>	FT
ACTUAL DEPTH:	<u>+ 17.210</u>	FT
THEORETICAL CABLE LENGTH:	<u>= 32.510</u>	FT
HAVE CLOCKS BEEN SYNCHRONIZED?	<input checked="" type="checkbox"/>	check
IS TRANSDUCER SET TO TAKE "SURFACE" READINGS?	<input checked="" type="checkbox"/>	check
ELEVATION OF MEASURING POINT:	<u>18.060</u>	FT M.S.L.
DEPTH TO WATER:	<u>- 15.30</u>	FT
REFERENCE ELEVATION:	<u>= 2.760</u>	FT M.S.L.
TEST NAME:	<u>U3-C1-2</u>	
LOGGING INTERVAL:	<u>20</u>	MIN
TEST START TIME:	<u>14:47</u>	HRS



LEGEND: **DTW** - DEPTH TO WATER  
**DTB** - DEPTH TO BOTTOM OF WELL  
**AD** - ACTUAL DEPTH OF TRANSDUCER UNDER WATER  
**CL** - CABLE LENGTH FROM SENSOR TO GROUND SURFACE/ TOP OF CASING

NOTES:





## APPENDIX C CHAINS OF CUSTODY

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number: 50013510

Client Name: Entergy

Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: M. Britos

Send Results To: Patrick Donahue

## Sample ID

\* For composites - indicate start and stop date/time

MW-45-42-(021)

MW-45-61-(021)

Date Collected (mm-dd-yyyy)

07/19/10 1538

07/19/10 1328

QC Code

N

N

Field Filtered

N

N

Sample Matrix

GW

GW

Should this sample be preserved?

Y

Y

Radioactive

N

N

TSCA Regulated

N

N

Total number of containers

1

1

1

Gamma Spec (GS)

1

1

1

Strontium 90 (Sr90)

1

1

1

2 Liter Poly

2

2

2 Liter Poly

2

Sample Analysis Requested (5) (Fill in the number of containers for each test)

← Preservative Type (6)

Comments  
Note: extra sample is required for sample specific QC

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

## Chain of Custody Signatures

Requested By (Signed) Date Time

*Erin Trent* 7/21/10 1530

Received by (Signed) Date Time

*Erin Trent* 7/21/10 1530

## Sample Shipping and Delivery Details

GEL PM: ERIN TRENT

Method of Shipment: FEDEX

Date Shipped:

Airbill #:

Airbill #:

1 Chain of Custody Number = Client Determined

2 QC Codes: N = Normal Sample; EB = Trip Blank; ED = Field Duplicate; EE = Equipment Blank; MS = Matrix Spike Sample; MSD = Matrix Spike Duplicate Sample; G = Grab; C = Composite

3 Field Filtered: For liquid matrices, indicate with a 'Y' - for yes the sample was field filtered or a 'N' - for no the sample was not field filtered.

4 Matrix Codes: DW = Drinking Water; GW = Groundwater; SW = Surface Water; WW = Waste Water; W = Water; ML = Miscellaneous; SO = Soil; SF = Sediment; SL = Sludge; ES = Solid Waste; O = Oil; F = Filter; P = Pipe; I = Inlet; F = Final; N = Normal

5 Sample Analysis Requested: Analytical method requested (ie: 8260B, 6010B, 7470A) and number of containers provided for each (ie: 8260B - 3, 6010B/7470A - 1).

6 Preservative Type: HA = Hydrochloric Acid; NI = Nitric Acid; SH = Sulfuric Acid; SA = Sodium Hydroxide; SA = Sodium Acetate; AA = Acetic Acid; BK = Bicarbonate; ST = Sodium Thiosulfate; P = preservative added = leave field blank

WHITE = LABORATORY

YELLOW = FILE

PINK = CLIENT

For Lab Receiving Use Only

Custody Seal Intact?

YES NO

Cooler Temp:

C

Page 1 of 1  
 Project #: Entergy GW Mon Prog  
 GEL Quote #: \_\_\_\_\_  
 COC Number <sup>1</sup>: \_\_\_\_\_  
 PO Number: 50019510

## GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

### GEL Work Order Number:

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 FAX: (843) 786-1778

Client Name: Entergy Phone #: (914) 736-8405  
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB/MB Send Results To: Patrick Donahue

Sample ID <small>* For comp sites - indicate start and stop date/time</small>	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code	Field Filtered <sup>2</sup>	Sample Matrix <sup>3</sup>	Should this sample be considered:		Sample Analysis Requested <sup>5</sup> (Fill in the number of containers for each test)						Preservative Type (6)	Comments
						Hazardous	TSC A Regulated	Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)				
MW-43-28-(016)	07/20/10	1348	N	N	GW	Y	N	1	1	1	1				2 Liter Poly
MW-43-62-(016)	07/20/10	1507	N	N	GW	Y	N	1	1	1	1				2 Liter Poly

TEST Requested: Normal:  Rush \_\_\_\_\_ Specialty \_\_\_\_\_ Subject to Surcharge \_\_\_\_\_ Fax Results: Yes /  No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Central Mountain

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Relinquished By (Signed) Erin Trent Date 7/21/10 Time 1530  
 Received by (Signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_

Method of Shipment: FEDEX Date Shipped: \_\_\_\_\_

Airbill #: \_\_\_\_\_

Chain of Custody Signatures

Relinquished By (Signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_  
 Received by (Signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_

Chain of Custody Number = Client Order Number

QC Codes: N = None of Sample; FB = Trip Blank; EB = Field Duplicate; E9 = Equipment Blank; MS = Matrix Spike Sample; MSD = Matrix Spike Duplicate; Sample; G = Grab; C = Composite; Field Filtered. For field matrices, indicate with a Y - BYVES the sample was field filtered or N - for sample was not field filtered.

Matrix Codes: BW = Drinking Water; GW = Groundwater; SW = Surface Water; WW = Waste Water; ML = Mobile Liquid; SL = Solid; SW = Solid Waste; O = Oil; F = Fuel; P = Fuel; N = Fuel; N = Fuel

Sample Analysis Requested: Analytical method requested is: R2648 = 60100-7470(A) and number of containers provided for each test: R2648 = 3, 60100-7470 (B)

Preservative Type: BA = Hydrochloric Acid; NH = Nitric Acid; SH = Sulfuric Acid; AA = Ascorbic Acid; HX = Hydroxide; SF = Sodium Thiosulfate. If no preservative is added = Leave field blank

WHITE = LABORATORY      YELLOW = FILE      PINK = CLIENT

For Lab Recovery Use Only

Container Seal Intact? YES / NO

Container Temp: \_\_\_\_\_ C

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

50013510

Sample Analysis Requested (5) (Fill in the number of containers for each test)

Phone #: (914) 736-8405  
 Fax #: (914) 734-6247

Client Name: Entergy  
 Project/Site Name: Indian Point Energy Center  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Send Results To: Patrick Donahue  
 Collected by: CB, MB

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military (hh:mm))	QC Code	Field Filtered?	Sample Matrix (4)
MW-41-40-(017)	07/21/10	1341	N	N	GW
MW-41-63-(016)	07/21/10	0923	N	N	GW

Should this sample be considered:	TSCA Regulated	Y	N
Metastable		Y	N
		Y	N

Tritium (H3)	Gamma Spec (GS)	Strontium 90 (SR90)
1	1	1
1	1	1

Test number of containers

Comments  
 Note: extra sample is required for sample specific QC

Preservative Type (6)

2 Liter Poly

2 Liter Poly

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone  
 Eastern  
 Central  
 Mountain  
 Pacific  
 Other

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

LAB Requested: Normal  Rush  SPECIALLY  Box Results: Yes  No

## Chain of Custody Signatures

Relinquished By (Signed)	Date	Time	Received by (Signed)	Date	Time
<i>Erin Trent</i>	7/21/10	1530	<i>Erin Trent</i>	7/21/10	1530

GEL PM: ERIN TRENT

Method of Shipment: FEDEX

Airbill #: 2

Date Shipped:

Airbill #: 3

For Lab Receiving Use Only

Custody Seal Intact?  
 YES  
 NO

Cooler Temp:  
 C

Chain of Custody Number = Client Determined

QC Codes: N = Normal Sample, FB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Mix of Spike Sample, MSB = Matrix Spike Duplicate Sample, C = Can, C = Composite

For Liquid matrices, indicate with a V for yes the sample was field filtered or N for no. For solid waste, O=Oil, F=Filter, P=Wipe, U=Line, F=Facet, N=Soil

Matrix Codes: DW=Drinking Water, GW=Ground Water, SW=Surface Water, WW=Wastewater, ML=Mineral, LQ=Liquid, SD=Soil, SP=Soil, SL=Sludge, SS=Soil waste, O=Oil, F=Filter, P=Wipe, U=Line, F=Facet, N=Soil

Sample Analysis Requested: Analytical method requested (i.e. 3250H, 6016R7470A) and number of containers provided for each (i.e. R260B = 3, 6016R7470A = 1)

Preservative Type: HA = Hydrochloric Acid, ME = Nitric Acid, SF = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, BX = Hexane, ST = Sodium Thiosulfate. If no preservative is added, leave field blank

WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT



**GEL Chain of Custody and Analytical Request**  
 \*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*  
**GEL Work Order Number:** 50013510  
 Client Name: Entergy  
 Phone #: (914) 736-8405  
 Project/Site Name: Indian Point Energy Center  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
 Collected by: **C6, M6** Send Results To: Patrick Donahue  
 Project/Site Name: Indian Point Energy Center  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
 Collected by: **C6, M6** Send Results To: Patrick Donahue

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

Sample ID <i>*For comparison - indicate start and stop time</i>	Date Collected (mm-dd-yy)	Time Collected (Military)	QC Code (2)	Field F Result <sup>3)</sup>	Sample Matrix <sup>4)</sup>	Should this sample be analyzed:		Total number of containers	Sample Analysis Requested <sup>5)</sup> (Fill in the number of containers for each test)					Preservative Type (6)	Comments Note: extra sample is required for sample specific QC	
						Radioactive	TSCA Regulated		Tridium (H3)	Gama Spec (G5)	Strontium 90 (Sr90)					
MW-39-67-(009)	07/22/10	1426	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-84-(009)	07/22/10	1442	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-102-(009)	07/22/10	1452	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-124-(009)	07/22/10	1139	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-183-(009)	07/22/10	1138	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-39-195-(009)	07/22/10	1210	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	

TAT Requested: Normal  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ Fax Results: Yes  No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern  Pacific  Central  Mountain  Other \_\_\_\_\_

**Chain of Custody Signatures**

Received by (signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_

1. *Erin Trent* 7/22/10 1645

2. \_\_\_\_\_

3. \_\_\_\_\_

GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX  
 Date Shipped: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_

For Lab Receiving Use Only  
 Custody Seal Intact? YES  NO   
 Cooler Temp: C

1) Chain of Custody Seal (3) - Chain of Custody Seal  
 2) QC Codes: A = Normal Sample, TB = Trip B, FE = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSP = Matrix Spike Duplicate Sample, G = Grab, C = Composite  
 3) Field Filtered: For liquid matrices, indicate with a 'V' for yes the sample was field filtered or 'N' for no. For sample was not field filtered.  
 4) Seal Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Milk, L = Liquid, SO = Soil, SS = Sludge, SS = Solid waste, O = Oil, F = Fuel, P = Paper, U = Urine, F = Fecal, N = Navel  
 5) Sample Analysis Requested: Analyze for metals of concern (1) = 82009, 401007, 47001 and number of containers provided for each (1) = 82609, 3, 6/20/07, 7/20, 1)  
 6) Preservative Type: BA = Hydrochloric Acid, M = Nitric Acid, SH = Sodium Hydroxide, SA = Salicylic Acid, AA = Ascorbic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added in the field bank  
**WHITE = LABORATORY**  
**PINK = CLIENT**  
**YELLOW = FILE**



# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

Phone #: (914) 736-8405

Client Name: Entergy

Fax #: (914) 734-6247

Project/Site Name: Indian Point Energy Center

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: **CB, MB** Send Results To: Patrick Donahue

Sample ID

*Please complete - this info starts and stops laboratory*

U3-4S-(001)

Date Collected (mm-dd-yy)

Time Collected (Military)

QC Code

Field Filtered

sample Matrix

Y N

Y N

I I I

I I I

I I I

I I I

I I I

I I I

I I I

I I I

I I I

I I I

2 Liter Poly

Comments  
 Note: extra sample is required for sample specific QC

Sample Analysis Requested (5) (Fill in the number of containers for each test)

Should this sample be considered?

TSCA Regulated

Kidnappings

Total number of containers

Tritium (H3)

Gamma Spec (G8)

Strontium 90 (Sr90)

← Preservative Type (6)

TAI Results: Normal:  Result: \_\_\_\_\_ Specify: \_\_\_\_\_ Subject to Sanctions: \_\_\_\_\_ Fax Results: Yes / No  Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

## Chain of Custody Signatures

Received by (signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_

**SECURED**

**STORAGE 7/23/10 1505**

Received by (signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_

Method of Shipment: **FEDEX**

Date Shipped: \_\_\_\_\_

Airbill #: \_\_\_\_\_

Airbill #: \_\_\_\_\_

## Sample Shipping and Delivery Details

GEL PM: **ERIN TRENT**

Method of Shipment: **FEDEX**

Date Shipped: \_\_\_\_\_

Airbill #: \_\_\_\_\_

Airbill #: \_\_\_\_\_

For Lab Receiving Use Only

Custody Seal Intact?

YES NO

Custody Seal Temp: \_\_\_\_\_ C

Sample Collection Time/Date

Eastern Pacific Other

Central

MEDIAN

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix

Sample Matrix







# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone (843) 536-8171  
Fax (843) 766-1178

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

50013510

Client Name: Entergy Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: **CB, MB** Send Results To: Patrick Donahue

Sample ID <small>* For composites - mix etc. start and stop date time</small>	* Date Collected (mm-dd-yy)	* Time Collected (Military)	QC Code (b)	Field Filtered (b)	Sample Matrix (c)	Should this sample be considered:		Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)				Comments  Note: extra sample is required for sample specific QC
						Radioactive	TSCA Required	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	Preservative Type (6)	
MW-32-48-(007)	07/26/10	12:52	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-32-59-(019)	07/26/10	13:00	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-32-85-(017)	07/26/10	14:51	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-32-149-(019)	07/26/10	15:34	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-32-173-(017)	07/26/10	15:17	N	N	GW	Y	N	1	1	1	2 Liter Poly	
MW-32-190-(022)	07/26/10	15:41	N	N	GW	Y	N	1	1	1	2 Liter Poly	

TAT Requested: Normal  Rush  Specific  (Subject to Surcharge) Fax Results: Yes  No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

### Chain of Custody Signatures

Received by (signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_  
**SECURED STORAGE 08/05/10 1300**

### Sample Shipping and Delivery Details

GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX  
 Date Shipped: \_\_\_\_\_  
 Airbill # \_\_\_\_\_  
 Airbill # \_\_\_\_\_

1) Chain of Custody Number - Chain Determined  
 2) QC Codes N = Normal Sample TB = Trip Blank FB = Field Duplicate, ER = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite  
 3) Field Filtered For liquid methods, indicate with a - Y - for yes the sample was field filtered or - N - for sample was not field filtered  
 4) Matrix Codes DW - Drinking Water, GW - Groundwater, SW - Surface Water, WW - Waste Water, W-Water, ME - Misc Liquid, SD - Soil, SP - Sludge, SS - Solid Waste, O - Oil, F - Filter, P - Wipe, U - Urine, F - Fecal, N - Nona  
 5) Sample Analysis Requested Analytical method requested (i.e. 8200B, 6010B, 7470A) and number of containers, provided for each (i.e. 4760B - A, 6010B 7470A - 1)  
 6) Preservative Type BA - Hydrochloric Acid, NI - Nitric Acid, SA - Sulfuric Acid, AA - Ascorbic Acid, HN = Heptane, ST = Sodium Thiosulfate If no preservative is added = leave field blank

**WHITE - LABORATORY      YELLOW - FILE      PINK - CLIENT**

*For Lab Receiving Use Only*  
 Custody Seal Intact? YES  NO   
 Cooler Temp: \_\_\_\_\_ C



Gel Laboratories, LLC  
2040 Savages Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

Client Name: **Energy** Phone #: (914) 736-8405  
 Project Site Name: **Indian Point Energy Center** Fax #: (914) 734-6247  
 Address: **450 Broadway, Suite 3, Buchanan, NY 10511**  
 Collected by: **CB, MB** Send Results To: **Patrick Donahue**

Sample ID: **MW-30-69-1033** Date Collected: **07/28/10** Time Collected: **12:33** \*Time Collected (military tabular)  
 \*Use ampoule - label, etc. start and stop date time  
 Matrix: **GW** Field Filtered: **N** QC Code: **N** Sample Matrix: **GW**  
 MW-30-84-1024 Date Collected: **07/28/10** Time Collected: **13:07** Matrix: **GW** Field Filtered: **N** QC Code: **N** Sample Matrix: **GW**

Sample Analysis Requested (5) (Fill in the number of containers for each test)	Preservative Type (6)	Comments	Should this sample be considered:		Total number of containers
			Radioactive	HA Regulated	
Gamma Spec (GS)	Strontium 90 (Sr90)	Note: extra sample is required for sample specific QC	Y	N	1
Tritium (H3)			Y	N	1
2 Liter Poly			Y	N	1
2 Liter Poly			Y	N	1

Circle Deliverable: C of A, OK Summary, Level 1, Level 2, Level 3, Level 4  
 Sample Collection Zone: Eastern, Pacific, Other, Mountain

FAI Requested: Normal  Rush  Specify  Subject to Surcharge  Fax Results  Yes  No

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Received by: **Erin Trent** Date: **07/28/10** Time: **15:00**  
 SECURED STORAGE  
 Airbill #: **2**

Chain of Custody Signatures

Received by	Date	Time
<b>Erin Trent</b>	<b>07/28/10</b>	<b>15:00</b>

Method of Shipment: **FEDEX** Date Shipped:

Sample Shipping and Delivery Details

GEL PM: **ERIN TRENT**  
 Airbill #: **2**

For Lab Receiving Use Only

Container Seal Intact? **YES**  
 Container Temp: **NO**

1. Chain of Custody Number - A four digit number  
 2. OK Codes - Normal Sample, TB - Trip Blank, FD - Field Duplicate, EB - Equipment Blank, MS - Matrix Spike Sample, MSD - Matrix Spills, Duplicate Sample, G - Grab, C - Composite  
 3. Field Filtered - For liquid samples, indicate with F - 1 - for yes the sample was field filtered or - N - for sample was not field filtered  
 4. Matrix Codes - DW - Drinking Water, GW - Groundwater, SW - Surface Water, WW - Waste Water, W - Water, HL - Hot Liquid, SO - Soil, SD - Sediment, SL - Sludge, SS - Solid Waste, O - Oil, F - Filter, P - Pipe, U - Urine, F - Feces, N - Nails  
 5. Sample Analysis Requested - Analytical method requested for each test: 3260B - 6010B/7878 and number of containers provided for each test: 3260B - 3 - 6010B/7878 - 1  
 6. Preservative Type: HA - Hydrochloric Acid, NI - Nitric Acid, SF - Sodium Fluoride, SA - Sulfuric Acid, AA - Ascorbic Acid, HY - Hydroxy, PE - Peracetic Acid, F - Field Blank

WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

Page: 1 of 1  
 Project #: Enterway GW Mon Prog  
 GEL Quote #: \_\_\_\_\_  
 COC Number: 50013510  
 PO Number: \_\_\_\_\_

GEL Laboratory, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

**GEL Chain of Custody and Analytical Request**  
 \*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*  
**GEL Work Order Number:** \_\_\_\_\_

Client Name: Enterway Phone #: (914) 736-8405  
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: CB, MB Send Results To: Patrick Donahue  
 Sample ID: \_\_\_\_\_  
 \*For composites, indicate start and stop date/time

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	OC Code (a)	Field Filtered (b)	Sample Matrix (c)	Should this sample be considered:	Total number of containers	Sample Analysis Requested (5)	Preservative Type (6)	Comments
MW-36-24-(019)	07/29/10	1204	N	N	GW	Y	1	Trilium (H3) Gamma Spec (GS) Strontium 90 (S90)		Note: extra sample is required for sample specific QC
MW-36-52-(018)	07/29/10	1224	N	N	GW	Y	1	Trilium (H3) Gamma Spec (GS) Strontium 90 (S90)		2 Liter Poly
										2 Liter Poly

LAB Requested:  Normal  Rust: \_\_\_\_\_ Specify: \_\_\_\_\_ (Subject to Surcharge) Fax Results:  Yes  No  
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4  
 Sample Collection Time Zone: Pacific  
 Eastern / Central / Other / Mountain

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**  
 Chain of Custody Signatures  
 Received by (signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_  
 SECURED STORAGE 08/05/10 1310  
 Method of Shipment: FEDEX Date Shipped: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_

For Lab Receiving Use Only  
 Custody Seal Intact? YES / NO  
 Cooler Temp \_\_\_\_\_

1) Chain of Custody Number (if not Determined)  
 2) OC Codes: N = Normal sample; EB = Equipment Blank; MS = Matrix Spike; Duplicate Sample; G = Grab; C = Composite  
 3) Field Filtered: For liquid samples, indicate with a Y for yes the sample was field filtered or N for sample was not field filtered  
 4) Matrix Codes: DW = Drinking Water; GW = Groundwater; SW = Surface Water; WW = Waste Water; W = Water; ML = Misc Liquid; SO = Soil; SD = Sediment; SL = Sludge; AS = Solid Waste; O = Oil; F = Filter; P = Pipe; L = Urin; F = Fecal; N = Nails  
 5) Sample Analysis Requested: Analytical method requested (i.e. 8200B, 0910B, 770A) and number of containers provided for each (i.e. 8200B = 3, 0910B, 770A = 1)  
 6) Preservative Type: BA = Boric Acid; M = Nitric Acid; SH = Sodium Hydroxide; SA = Sulfuric Acid; AA = Acetic Acid; W = Hresaw; ST = Sodium Thiosulfate. If no preservative is added, leave field blank  
 WHITE = LABORATORY YELLOW = FILE PINK = CLIENT





GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number: 50013510

Client Name: Entergy

Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: **CG, MB** Send Results To: Patrick Donahue

Sample ID

\* For composites - indicate start and stop date/time

MW-42-49-(022)

07/30/10 1138

N N

Y N

Tritium (H3)

Gamma Spec (GS)

Strontium 90 (Sr90)

Nickel 63 (Ni63)

Preservative Type (6)

MW-42-78-(017)

07/30/10 1223

N N

Y N

Tritium (H3)

Gamma Spec (GS)

Strontium 90 (Sr90)

Nickel 63 (Ni63)

Preservative Type (6)

Comments

Note: extra sample is required for sample specific QC

2 Liter Poly

2 Liter Poly

TAT Requested: Normal  Rush  Specify: (Subject to Surcharge) Yes  No

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

## Chain of Custody Signatures

Requested By (Signed) Date Time

*Patrick Donahue* 08/05/10 1225 SECURED

2 STORAGE 08/05/10 1225

3

## Sample Shipping and Delivery Details

GEL PM: ERIN TRENT

Method of Shipment: FEDEX

Date Shipped:

Airbill #:

Airbill #:

1. Chain of Custody Number - Chain Examined

2. QC Codes: N - Normal Sample, TB - Trip Blank, FB - Field Duplicate, EB - Field Duplicate, MS - Matrix Spike Sample, MSD - Matrix Spike Duplicate Sample, G - Grab, C - Composite

3. Field Filtered: For liquid matrices, indicate with 1-Y - for yes the sample was field filtered or -N - for sample was not field filtered

4. Matrix Codes: DW - Drinking Water, GW - Groundwater, SW - Surface Water, WW - Waste Water, W - Water, ML - Milk, LIQ - Lique, SO - Soil, L - LD - Solution, SI - Solid, W - Waste, O - Oil, F - Filter, P - Waste, U - Urine, F - Fecal, N - Nasal

5. Sample Analysis Requested: Analytical method requested (i.e. 8260E, 8210E, 7470A) and number of containers provided for each (i.e. 2/1668 + 3 40/05/10/94 + 1)

6. Preservative Type: HA - Hydrochloric Acid, M - Nitric Acid, SH - Sodium Hydroxide, SA - Sulfuric Acid, AA - Acetic Acid, BA - Boric Acid, ST - Sodium Thiosulfate. (no preservative is added - leave field blank)

WHITE = LABORATORY YELLOW = FILE PINK = CLIENT

For Lab Receipting Use Only

Cleaned Seal Intact?

YES NO

Cleaner Temp

C





Page: 1 of 1  
 Project #: Entergy GW Mon Prog  
 GEL Quote #: \_\_\_\_\_  
 COC Number: \_\_\_\_\_  
 PO Number: 50013510  
**GEL Chain of Custody and Analytical Request**  
**\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\***  
**GEL Work Order Number:**  
 GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

Client Name: Entergy Phone #: (914) 736-8405  
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Send Results To: Patrick Donahue

Sample ID <i>* For comparative - include start and stop date/time</i>	Date Collected (mm-dd-yy)	Time Collected (Military Time)	QC Code (if applicable)	Field Filtered <sup>(1)</sup>	Sample Matrix <sup>(4)</sup>	Should this sample be considered:		Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)				Preservative Type (6)	Comments Note: extra sample is required for sample specific QC	
						Radioactive	TSCA Regulated	Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr-90)			Other
MW-62-18-(014)	08/03/10	1300	N	N	GW	Y	N	1	1	1			2 Liter Poly	
MW-62-37-(014)	08/03/10	1252	N	N	GW	Y	N	1	1	1			2 Liter Poly	
MW-62-53-(013)	08/03/10	1220	N	N	GW	Y	N	1	1	1			2 Liter Poly	
MW-62-71-(014)	08/03/10	1130	N	N	GW	Y	N	1	1	1			2 Liter Poly	
MW-62-92-(014)	08/03/10	1132	N	N	GW	Y	N	1	1	1			2 Liter Poly	
MW-62-138-(014)	08/03/10	1409	N	N	GW	Y	N	1	1	1			2 Liter Poly	
MW-62-182-(014)	08/03/10	1402	N	N	GW	Y	N	1	1	1			2 Liter Poly	

TAJ Requested: Normal:  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ Subject to Sampling: Yes:  No:  Fax Results: \_\_\_\_\_  
 Circle Deliverable: C of A: \_\_\_\_\_ QC Summary: \_\_\_\_\_ Level 1: \_\_\_\_\_ Level 2: \_\_\_\_\_ Level 3: \_\_\_\_\_ Level 4: \_\_\_\_\_  
 Sample Collection Time Zone: \_\_\_\_\_  
 Location: \_\_\_\_\_ Pacific \_\_\_\_\_ Other \_\_\_\_\_  
 Maintain: \_\_\_\_\_

**Chain of Custody Signatures**  
 Received by (signed): \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_  
 SECURED STORAGE 08/05/10 1215  
 Method of Shipment: FEDEX  
 Date Shipped: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_

**Sample Shipping and Delivery Details**  
 GEL PM: ERIN TRENT  
 For Lab Receiving Use Only  
 Custody Seal Intact? YES NO  
 Cooler Temp: \_\_\_\_\_  
 Chain of Custody Number: \_\_\_\_\_ (then Determined)  
 1) OK Codes: N - Normal Sample, TB - Trip Blank, FD - Field Duplicate, EB - Equipment Blank, MS - Matrix Spike Sample, MSD - Matrix Spike Duplicate Sample, C - Grab, C - Composite  
 2) Field Filtered: For liquid matrices, indicate with a 'Y' - for vessels the sample was field filtered or 'N' - for sample was not field filtered  
 3) Matrix Codes: EW - Drinking Water, GW - Groundwater, SW - Surface Water, WW - Waste Water, W - Water, ML - Mils, Lapid, SO - Soil, SD - Sediment, SL - Sludge, SS - Solid Waste, O - Oil, F - Fuel, U - Urine, F - Food, N - Nuisal  
 4) Sample Analysis Requested: Analytical method requested (i.e. 8560B, 808017270A, 3 - of number of containers prepared for analysis - 8560B - A 60/100 - 270A - U)  
 5) Preservative Type: RA - Hydrochloric Acid, M - Nitric Acid, SH - Sodium Hydroxide, SA - Sulfuric Acid, AA - Ascorbic Acid, BX - Urea, ST - Sodium Thiosulfate. If no preservative is added - leave field blank  
**WHITE = LABORATORY YELLOW = FILE PINK = CLIENT**



# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
2940 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-4171  
Fax: (843) 766-1178

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number: 50013510

Client Name: Entergy  
Project/Site Name: Indian Point Energy Center  
Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
Phone #: (914) 736-8405  
Fax #: (914) 734-6247

Collected by: **CB, MB**  
Send Results To: Patrick Donahue

Sample ID

\*For composite, indicate start and stop date/time

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code	Field Filtered	Sample Matrix	Should this sample be considered:		Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)					
						Radioactive	TSCA Regulated	Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	Nickel 63 (Ni63)	Comments
MW-54-37-(014)	08/04/10	1432	N	N	GW	Y	N	1	1	1	1	1	2 Liter Poly
MW-54-58-(014)	08/04/10	1435	N	N	GW	Y	N	1	1	1	1	1	2 Liter Poly
MW-54-123-(014)	08/04/10	1449	N	N	GW	Y	N	1	1	1	1	1	2 Liter Poly
MW-54-144-(014)	08/04/10	1144	N	N	GW	Y	N	1	1	1	1	1	2 Liter Poly
MW-54-173-(014)	08/04/10	1209	N	N	GW	Y	N	1	1	1	1	1	2 Liter Poly
MW-54-190-(014)	08/04/10	1234	N	N	GW	Y	N	1	1	1	1	1	2 Liter Poly

IAT Requested: Normal  Rush  Specify: (Subject to Surcharge) Yes / No  /

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection:  Matrix  Pack 1  Other

Sample Shipping and Delivery Details

Received by (Signature): *[Signature]* Date: 08/05/10 1200  
 Received by (Typed): SECURED STORAGE 08/05/10 1200  
 GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX  
 Date Shipped:   
 Airbill #:   
 Airbill #:

Chain of Custody Signatures

1) Chain of Custody Number & Client Agreement  
 2) QC Codes: N - Normal Sample, IB - In-Process Blank, FD - Field Duplicate, EB - Equipment Blank, MS - Matrix Spike Sample, MSD - Matrix Spike Duplicate Sample, G - Grab, C - Composite  
 3) Field Filtered: For liquid matrices, attach with a 'V' bar yes the sample was field filtered or 'N' - No for sample was not field filtered  
 4) Matrix Codes: BW - Drink or Water, GW - Groundwater, SW - Surface Water, WW - Waste Water, W - Water, ML - Misc. Liquid, SO - Soil, SD - Sediment, SI - Sludge, SS - Solid Waste, O - Oil, F - Fiber, P - Pipes, U - Urine, F - Fecal, N - Nasal  
 5) Sample Analysis Requested: Analytical method requested (i.e. 8200B, 6010B, 7470A) and number of containers provided for each (i.e. 8200B - 3, 6010B 7470A - 1)  
 6) Preservation Type: HA - Hydrofluoric Acid, N - Nitric Acid, SH - Sulfuric Acid, AA - Ascorbic Acid, HX - Hexamine, ST - Sodium Thiosulfate. The preservation is added - send field blank  
 WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT  
 For Lab Recovery Use Only  
 Correct Seal intact? YES NO  
 Cooler Temp. C

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

**GEL Work Order Number:**

Client Name: **Entropy**

Phone #: **(914) 736-8405**

Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)

Project/Site Name: **Indian Point Energy Center**

Fax #: **(914) 734-6247**

Address: **450 Broadway, Suite 3, Buchanan, NY 10511**

Collected by: **CB, MB** Send Results To: **Patrick Donahue**

Sample ID

*For composite, indicate start and stop date/time*

B 6 (009)

Date Collected: **08/05/10 1343**

\*Time Collected (Military (hh:mm))

QC Code

N N

Field Filtered <sup>(3)</sup>

N N

Sample Matrix <sup>(4)</sup>

GW

Should this sample be considered:

TSCA Regulated

Radioactive

Y

N

N

I

I

I

I

I

I

I

I

I

I

I

I

I

I

I

I

I

I

I

I

Total number of containers

Gamma Spec (GS)

Tritium (H3)

Strontium 90 (Sr90)

← Preservative Type (6)

**Comments**  
Note: extra sample is required for sample specific QC

2 Liter Poly

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone

Eastern Pacific Other

Central Mountain

### Chain of Custody Signatures

Received by (Signed) Date Time

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

*[Signature]* 08/11/10 1300

GEL PM: **ERIN TRENT**

Method of Shipment: **FEDEX**

Date Shipped:

Airbill #:

Airbill #:

### Sample Shipping and Delivery Details

1. Chain of Custody Number = Client Determined

2. QC Codes: N = Normal Sample, TB = Trip Blank, ED = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite

3. Field Filtered: For liquid matrices, indicate with a 'Y'. For yes, no sample was field filtered or 'N' for no sample was not field filtered

4. Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, WWSW = WWSW, WWSL = WWSL, WWSM = WWSM, WWSO = WWSO, WWSL = WWSL, WWSM = WWSM, WWSO = WWSO, WWSL = WWSL, WWSM = WWSM, WWSO = WWSO

5. Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B, 7470A) and number of containers provided for each (i.e. 8260B - 3, 6010B/7470A - 1)

6. Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, AA = Acetic Acid, HX = Hexanic Acid, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

**WHITE = LABORATORY**

**YELLOW = FILE**

**PINK = CLIENT**

For Lab Receiving Use Only

Contract Seal Intact?

YES / NO

Cooler Temp:

C



Page 1 of 1  
 Project = Energy GW Mon Prog  
 GEL Quote #:  
 GEL Number: 50013510  
 PO Number: 50013510

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

**GEL Chain of Custody and Analytical Request**  
 \*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*  
**GEL Work Order Number:**  
 Phone #: (914) 736-8405  
 Fax #: (914) 734-6247

Client Name: Energy  
 Project/Site Name: Indian Point Energy Center  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
 Collected by: **CE, MB**  
 Send Results To: Patrick Donahue

Sample ID <small>* For Composites, include start and stop date/time</small>	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code (N)	Field Filtered (N)	Sample Matrix (GW)	Should this sample be considered		Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)		Preservative Type (6)	Comments  Note: extra sample is required for sample specific QC
						Radioactive	TSCA Required	Total number of containers			
MW-37-22-(019)	08/05/10	1406	N	N	GW	Y	N	1	1		2 Liter Poly
MW-37-32-(019)	08/05/10	1400	N	N	GW	Y	N	1	1		2 Liter Poly
MW-37-40-(019)	08/05/10	1425	N	N	GW	Y	N	1	1		2 Liter Poly
MW-37-57-(019)	08/05/10	1359	N	N	GW	Y	N	1	1		2 Liter Poly

Circle Deliverable: C=CA / QC Summary: Level 1 / Level 2 / Level 3 / Level 4  
 Sample Collection Limit: Zang  
 Eastern Pacific  
 Central Other  
 Mountain

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards  
 (A) Requested: Normal  Rush  Specific   
 Received by (signed): *Erin Trent* Date: 08/05/10 Time: 1600  
 Method of Shipment: FEDEX  
 Date Shipped:  
 Airbill #:  
 Airbill #:

Chain of Custody Signatures  
 Received by (signed): *Erin Trent* Date: 08/05/10 Time: 1600  
 Method of Shipment: FEDEX  
 Date Shipped:  
 Airbill #:  
 Airbill #:

For Lab Receiving Use Only:  
 Custody Seal Intact?  
 YES NO  
 Cooler Temp.  
 C

WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT

1) Chain of Custody Number - Client Designation  
 2) QC Codes: N - Normal Sample, TB - Top Blank, FD - Field Duplicate, LB - Laboratory Blank, MS - Matrix Spike Sample, MSP - Matrix Spike Duplicate Sample, G - Grab, C - Composite  
 3) Field Filtered - for liquid matrices, and care with a Y - for yes, the sample was field filtered or N - for no, the sample was not field filtered  
 4) Matrix Codes: DW - Drinking Water, CW - Groundwater, SW - Surface Water, WW - Waste Water, W - Water, ML - Misc. Liquid, SD - Sediment, SL - Sludge, SS - Soil Waste, G-O, F - Filter, P - Wipe, U - Urine, F - Food, N - Nasal  
 5) Sample Matrix Requested - add Y cell method requested to C, 8200B - 6100B/7470A, and our list of containers provided for each (i.e. 8200B - 3, 6100B/7470A - 1)  
 6) Preservative Type: BA - Boric Acid, SA - Sodium Dichromate, SA - Sulfuric Acid, AA - Ascorbic Acid, HA - Hydrochloric Acid, NI - Nitric Acid, SH - Sodium Hydroxide, FTS - Fluoride, FTS - Fluoride, FTS - Fluoride, FTS - Fluoride



Page 1 of 1  
 Project #: **Entropy GW Mon Prog**  
 GEL Quote #:  
 COC Number: **50013510**  
 PO Number:

**GEL Chain of Custody and Analytical Request**  
 \*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*  
**GEL Work Order Number:**  
 GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

Client Name: **Entropy**  
 Phone #: (914) 736-8405  
 Project Site Name: **Indian Point Energy Center**  
 Fax #: (914) 734-6247  
 Address: **450 Broadway, Suite 3, Buchanan, NY 10511**

Collected by: **CB, MB**  
 Sample ID: **CB, MB**  
 \*For compliance - indicate start and stop date times.  
 \*Date Collected (mm-dd-yy) \*Time Collected (Military) (HH:MM)  
**08/06/10 1311**  
**08/06/10 1315**  
**08/06/10 1250**  
 Send Results To: **Patrick Donahue**

Sample Analysis Requested (5) (Fill in the number of containers for each test)  
 Strontium 90 (Sr90) Nickel 63 (Ni63)  
 Tritium (H3) Gamma Spec (GS)  
 Total number of containers

Sample ID	Should this sample be considered:	Radioactive	TSCA Regulated	Preservative Type (6)	Comments
MW-55-24-(015)	Y	Y	N	GW	2 Liter Poly
MW-55-35-(014)	Y	Y	N	GW	2 Liter Poly
MW-55-54-(015)	Y	Y	N	GW	2 Liter Poly

Sample Collection Time Zone  
 Eastern Pacific Mountain Other

TAI Requested	Normal	Risk	Specify	Subject to surcharge	Fax Results	Yes	No	Circle Deliverable: C of A	QC Summary	Level 1	Level 2	Level 3	Level 4
	<input checked="" type="checkbox"/>						<input type="checkbox"/>						

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures			Sample Shipping and Delivery Details		
Received by (Signed)	Date	Time	GEL PM:	Method of Shipment:	Date Shipped
	08/06/10	1600	ERIN TRENT	FEDEX	

For Lab Receiving Use Only  
 Custody Seal Intact?  
 YES  NO   
 Cooler Temp.  C



# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 769-1178

**GEL Work Order Number:**

Client Name: **Entropy**

Phone #: (914) 736-8405

Sample Analysis Requested (5) (Fill in the number of containers for each test)

Project/Site Name: **Indian Point Energy Center**

Fax #: (914) 734-6247

Address: **450 Broadway, Suite 3, Buchanan, NY 10511**

Collected by: **Send Results To: Patrick Donahue**

**Sample ID**

\* For containers, indicate start and stop date/time

MW-66-21-(014)

Date Collected (mm-dd-yy)

Time Collected (hh:mm)

QC Cook (Military)

Field Filtered (Y/N)

Sample Matrix (A)

Radioactive

TSCA Regulated

Should this sample be considered:

Total number of containers

Tritium (H3)

Gamma Spec (GS)

Strontium 90 (S-90)

Nickel 63 (Ni63)

Preservative Type (6)

MW-66-36-(013)

08/09/10 1230

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1147

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1230-06

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1230-06

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1230-06

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1230-06

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1230-06

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1230-06

N

N

GW

Y

1

1

1

1

1

1

1

1

1

MW-66-36-(013)

08/09/10 1230-06

N

N

GW

Y

1

1

1

1

1

1

1

1

1

TAT Requested: Normal  Rush:  Spec. by: \_\_\_\_\_ Fax Results: Yes / No   Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

**Chain of Custody Signatures**

Received by (Signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_

1. *Erin Trent* 8/9/10 1500 SECURE STORAGE 8/9/10 1500

2. \_\_\_\_\_

3. \_\_\_\_\_

**Sample Shipping and Delivery Details**

GEL PM: ERIN TRENT

Method of Shipment: FEDEX

Date Shipped: \_\_\_\_\_

Airbill #: \_\_\_\_\_

Airbill #: \_\_\_\_\_

For Lab Receiving Use Only

Cooling Seal Intact?

YES NO

Cooler Temp.

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

Page: 1 of 1  
 Project #: Energy GW Mon Prog  
 GEL Quote #: \_\_\_\_\_  
 COC Number <sup>1)</sup>: \_\_\_\_\_  
 PO Number: 50013510  
 Chem Name: Energy  
 Phone #: (914) 736-8405  
 Fax #: (914) 734-6247  
 Project/Site Name: Indian Point Energy Center  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
 Collected by: CB, MB  
 Send Results To: Patrick Donahue

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 536-8171  
 Fax: (843) 766-1178

**GEL Chain of Custody and Analytical Request**  
 \*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*  
**GEL Work Order Number:**

Sample ID <small>*For composite - indicate start and stop date/time</small>	Date Collected (mm-dd-yy)	Time Collected (Military (hhmm))	QC Code <small>1)</small>	Field Filtered <small>2)</small>	Sample Matrix <small>4)</small>	Should this sample be considered:		Total number of containers	Sample Analysis Requested <sup>5)</sup> (Fill in the number of containers for each test)						Comments
						Radionuclide	TSCA Regulated		Gamma Spec (GS)	Strontium 90 (Sr90)	Nickel 63 (Ni63)	Preservative Type (6)			
MW-67-39-(014)	08/09/10	1043	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-67-105-(013)	08/09/10	1037	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-67-173-(014)	08/09/10	1107	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-67-219-(013)	08/09/10	1333	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-67-276-(013)	08/09/10	1336	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-67-323-(013)	08/09/10	1323	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	
MW-67-340-(013)	08/09/10	1320	N	N	GW	Y	N	1	1	1	1	1	1	2 Liter Poly	

TAT Requested: Normal:  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ Fax Results: Yes  No   
 Circle Deliverable: C of A / QC Summary Level 1 / Level 2 / Level 3 / Level 4  
 Sample Collection Time Zone: Eastern Pacific Other Mountain

**Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures  
 Received by (signed) Date Time  
Kenf Bryan 8/9/10 1520  
ERIN TRENT 8/9/10 1500  
 ?  
 3

Method of Shipment: FEDEX  
 Date Shipped:  
 Airbill #:  
 Airbill #:

For Lab Receiving Use Only  
 Custody Seal Intact? YES NO  
 Cooler Temp C

1) Chain of Custody Number = Client Determined  
 2) QC Codes: N = Normal Sample, TR = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike, Sample, MSD = Matrix Spike Duplicate, Sample, C = Grab, C = Composite  
 3) Field Filtered: 1 for equal volumes, matrix with a Y = for yes the sample was field filtered or N = for sample was not field filtered.  
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Wastewater, W = Water, MT = Metal, S = Soil, SS = Solid Waste, O = Oil, F = Filter, P = Wipe, U = Urine, F = Fecal, N = Nosal  
 5) Sample Analysis Requested: Analytical method requested (see 81008, 60108, 7476A) and number of containers provided for each (see 81008 - 3, 60108/7476A - 1)  
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, BX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank.  
**WHITE = LABORATORY**  
**YELLOW = FILE**  
**PINK = CLIENT**

# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number: 50013510

Client Name: Entergy Phone #: (914) 736-8405  
Project Site Name: Indian Point Energy Center Fax #: (914) 734-6247  
Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: **CB, MB** Send Results To: Patrick Donahue

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military (hh:mm))	QC Code (4)	Field Filtered (4)	Sample Matrix (4)	Should this sample be considered:		Total number of containers	Sample Analysis Requested (6)				Comments	
						Radioactive	TSC A Regulated		Preserve	Arrow	Type	(6)		
MW-63-18-(014)	08/10/10	1202	N	N	GW	Y	N	1					2 Liter Poly	Note: extra sample is required for sample specific QC
MW-63-34-(014)	08/10/10	1144	N	N	GW	Y	N	1					2 Liter Poly	
MW-63-50-(014)	08/10/10	1432	N	N	GW	Y	N	1					2 Liter Poly	
MW-63-93-(015)	08/10/10	1510	N	N	GW	Y	N	1					2 Liter Poly	
MW-63-112-(014)	08/10/10	1452	N	N	GW	Y	N	1					2 Liter Poly	
MW-63-121-(014)	08/10/10	1128	N	N	GW	Y	N	1					2 Liter Poly	
MW-63-163-(014)	08/10/10	1121	N	N	GW	Y	N	1					2 Liter Poly	
MW-63-174-(014)	08/10/10	1140	N	N	GW	Y	N	1					2 Liter Poly	

TAI Requested: Normal  Rush:  Specify: (Subject to surcharge) Fax Results: Yes  No

Circle Deliverable: C of A / QA Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Timing Zone: Eastern Pacific Other

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures

Received by (Signed)	Date	Time
<i>Erin Trent</i>	08/10/10	1645

Method of Shipment: FEDEX Date Shipped:

Airbill #:

Airbill #:

For Lab Receiving Use Only:  
Customer Seal Intact? YES / NO  
Cooler Temp. /

WHITE - LABORATORY  
YELLOW - FILE  
PINK - CLIENT

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

Client Name: Entergy  
Project Site Name: Indian Point Energy Center  
Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
Phone #: (914) 736-8405  
Fax #: (914) 734-6247  
Sample Analysis Requested (5) (Fill in the number of containers for each test)

Sample ID <small>* For duplicates - indicate start and stop date/time</small>	*Date Collected (mm-dd-yy)	*Time Collected (Military) (HH:MM)	OC Code <small>4</small>	Field Filtered <small>5</small>	Sample Matrix <small>6</small>	Total number of containers				Preservative Type (6)	Comments
						Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	Nickel 63 (Ni63)		
MW-49-26-(021)	08/11/10	1127	N	N	GW	1	1	1	1		2 Liter Poly
MW-49-42-(021)	08/11/10	1100	N	N	GW	1	1	1	1		2 Liter Poly
MW-49-65-(021)	08/11/10	1119	N	N	GW	1	1	1	1		2 Liter Poly

Should this sample be considered:	Radiation		TSCA Regulated	Sample Collection Time Zone
	Yes	No		
				Eastern Central Other

TAT Requested: Normal  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ Subject to Surcharge: \_\_\_\_\_ Fax Results: Yes / No  Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures		Sample Shipping and Delivery Details	
Relinquished By (Signed)	Date	Time	Date
<i>Erin Trent</i>	8/11/10	1310	

GEL PM: ERIN TRENT  
Method of Shipment: FEDEX  
Date Shipped:  
Airbill #: \_\_\_\_\_  
Airbill #: \_\_\_\_\_

For Lab Receiving Use Only  
Current Seal Intact? YES / NO  
Cooler Temp? \_\_\_\_\_

1) Chain of Custody Number - Client Determined  
2) QC Codes: N - Normal sample; TB - Trip Blank; FE - Field Duplicate; EB - Equipment Blank; MS - Matrix Spike Sample; MSD - Matrix Spike Duplicate Sample; G - Grab; C - Composite  
3) Field Filtered: For liquid matrices, indicate with a - V - for yes the sample was field filtered or - N - for sample was not field filtered  
4) Matrix Codes: DW - Drinking Water; GW - Groundwater; SW - Surface Water; WW - Waste Water; W - Water; ML - Misc. Liquid; SD - Soil; SS - Sludge; SS-Solid Waste; O - Oil; F - Filter; P - Waste; U - Urine; F - Fecal; N - Nasal  
5) Sample Analysis Requested: Analytical method requested (i.e. 02600, 06100, 7470A) and number of containers provided for each (i.e. 2/5/0/0 - 3, 06/10/0/7/7/2A - 1)  
6) Preservative Type: BA - Hydrochloric Acid; NI - Nitric Acid; SH - Sulfuric Acid; SA - Sulfuric Acid; AA - Acetic Acid; RX - Hexane; ST - Sodium Thiosulfate; If no preservative is added = leave field blank  
WHITE = LABORATORY  
YELLOW = FILE  
PINK = CLIENT

Page: 1 of 1  
 Project #: Entergy GW Mon Prog  
 GEL Quote #:  
 COC Number: 50013510  
 PO Number:

# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
 7040 Savage Road  
 Charleston, SC 29417  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405  
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: M. Britos Send Results To: Patrick Donahue

Sample ID

\* For composites - indicate start and stop date/time

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military (hh:mm))	QC Code (Military)	Field Filtered (N)	Sample Matrix (GW)	Total number of containers		Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)		Preservative Type (6)	Comments
						Gamma Spec (GS)	Tritium (H3)	Strontium 90 (S90)	Nickel 63 (Ni63)		
MW-60-35-(014)	08/16/10	1443	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)	08/16/10	1534	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)-B	08/16/10	1535	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)-D	08/16/10	1536	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)-S	08/16/10	1537	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-72-(014)	08/17/10	1159	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-135-(014)	08/17/10	1209	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-154-(014)	08/17/10	1218	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-176-(014)	08/17/10	1251	N	N	GW	Y	N	1	1		2 Liter Poly

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military (hh:mm))	QC Code (Military)	Field Filtered (N)	Sample Matrix (GW)	Total number of containers		Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)		Preservative Type (6)	Comments
						Gamma Spec (GS)	Tritium (H3)	Strontium 90 (S90)	Nickel 63 (Ni63)		
MW-60-35-(014)	08/16/10	1443	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)	08/16/10	1534	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)-B	08/16/10	1535	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)-D	08/16/10	1536	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-53-(014)-S	08/16/10	1537	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-72-(014)	08/17/10	1159	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-135-(014)	08/17/10	1209	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-154-(014)	08/17/10	1218	N	N	GW	Y	N	1	1		2 Liter Poly
MW-60-176-(014)	08/17/10	1251	N	N	GW	Y	N	1	1		2 Liter Poly

TAT Requested: Normal  Rush  Specify: \_\_\_\_\_ Subject to Surcharges: \_\_\_\_\_ Fax Results: Yes / No / \_\_\_\_\_

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures		Sample Shipping and Delivery Details	
Received by (Typed)	Date	GEL PM:	Date Shipped:
<u>SECURED STORAGE</u>	<u>08/17/10 1600</u>	<u>ERIN TRENT</u>	<u>FEDEX</u>
<u>Erin Trent</u>	<u>08/17/10 1600</u>	Airbill #:	
		Airbill #:	

For Lot Retention Use Only

Custody Seal Intact? YES NO

Container Temp. C

1) Chain of Custody Number = Chain Determined  
 2) QC Codes: A = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Dup (retest), Sample, G = Gels, C = Composite  
 3) Field Filters: For liquid matrices, indicate with a - L - for the sample was field filtered or - N - for sample was not field filtered  
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, WWS = WWS, LQ = LQ, SO = Soil, SD = Sediment, SL = Sludge, SS = Solid Waste, U = Oil, F = Filter, P = Pipe, A = Air, E = Ecol, N = Nal  
 5) Sample Analysis Requested: Analytical method requested (i.e., WQAR, 4010B, 7070A) and number of containers provided for analysis (e.g., 8266.B - J, 60/10/07/70A - 1)  
 6) Preservative Type: HA = Hydrochloric Acid, ME = Nitric Acid, SH = Sodium Hydroxide, AA = Ascorbic Acid, HX = Hexamine, ST = Sodium Thiosulfate. If no preservative is added, leave field blank  
 WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT



# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

Project #: Entergy GW Mon Prog  
 GEL Quote #:  
 COC Number <sup>(1)</sup>:  
 PO Number: 50013510

GEL Work Order Number:  
 Client Name: Entergy  
 Phone #: (914) 736-8405  
 Fax #: (914) 734-6247

Project/Site Name: Indian Point Energy Center  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: M. Britos  
 Sample ID  
 \* For composites - indicate start and stop date/time  
MW-36-41-(013)  
 Date Collected: 07/29/2010  
 Time Collected (Military) (hh:mm): 1223  
 QC Code: N  
 Field Filtered <sup>(5)</sup>: N  
 Sample Matrix <sup>(6)</sup>: GW

Send Results To: Patrick Donahue  
 Total number of containers considered:  
 TSCA Regulated:  
 Radiactive:  
 Y N

Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)  
 Tritium (H3): 1  
 Gamma Spec (GS): 1  
 Strontium 90 (Sr90): 1

Comments  
 Note: extra sample is required for sample specific QC  
 Preservative Type (6):  
2 Liter Poly

TAT Requested:	Normal	Rush	Specify:	(Subject to Surcharges)	Fax Results:	Yes	No
Circle Deliverable:	C of A	QC Summary	Level 1	Level 2	Level 3	Level 4	Level 4

Sample Collection Time Zone  
 Eastern  
 Central  
 Mountain  
 Pacific  
 Other

Sample Shipping and Delivery Details  
 GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX  
 Date Shipped:  
 Airbill #:  
 Airbill #:

Chain of Custody Signatures  
 Received by (signed):  
SECURED STORAGE  
 Date: 08/18/10  
 Time: 1030

Chain of Custody Number = Client Determined  
 1) QC Codes: N = Normal Sample, EB = Equipment Blank, MB = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite  
 2) Field Filtered: For liquid matrices, indicate with a Y - for yes the sample was field filtered or a N - for no sample was not field filtered  
 3) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W-Water, ML = Milk Liquid, SD = Solid, O = Oil, P = Filter, Pe = Filter, Pe = Filter, Pe = Filter  
 4) Sample Analysis Requested: Analytical method requested (i.e. R260B, 60166/7470A) and number of containers provided for each (i.e. R260B - 3, 60166/7470A - 1)  
 5) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, SA = Acetic Acid, HW = Hydroxide, ST = Sodium Thioacetate. If no preservative is added = leave field blank  
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, SA = Acetic Acid, HW = Hydroxide, ST = Sodium Thioacetate. If no preservative is added = leave field blank

Remarks: *Are there any known hazards applicable to these samples? If so, please list the hazards*

For Lab Receiving Use Only  
 Custody Seal Intact?  
 YES NO  
 Cooler Temp:  
 C

WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT



Page: 1 of 1  
 Project #: Entergy GW Mon Prog  
 GEL Quote #: \_\_\_\_\_  
 COC Number (1): \_\_\_\_\_  
 PO Number: 50013510

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

**GEL Work Order Number:**

Client Name: Entergy

Phone #: (914) 736-8405

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: M. Britos      Send Results To: Patrick Donahue

Sample Analysis Requested (5) (Fill in the number of containers for each test)

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code (5)	Filter Filtered (Y/N)	Sample Matrix (6)	Should this sample be considered:		Total number of containers	Sample Analysis Requested (5)		Preservative Type (6)	Comments
						Radioactive	TSCA Regulated		1	2		
MW-30-69-(034)	08/20/10	1508	N	N	GW	Y	N	1	1	1		Note: extra sample is required for sample specific QC  2 Liter Poly
MW-30-84-(025)	08/20/10	1651	N	N	GW	Y	N	1	1	1		

TAT Requested: Normal:  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ (Subject to Surcharges)      Fax Results: Yes / No  Yes  No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Central Mountain

### Chain of Custody Signatures

Received By (Signed)	Date	Time	Received by (Signed)	Date	Time
	08/20/10	1730	ERIN TRENT	08/20/10	1730

**Sample Shipping and Delivery Details**

GEL PM: ERIN TRENT      Method of Shipment: FEDEX      Date Shipped: \_\_\_\_\_

Airbill #: \_\_\_\_\_      Airbill #: \_\_\_\_\_

---

**For Lab Receiving Use Only:**

Custody Seal Intact? YES / NO

Cooler Temp. C

**Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards**

WHITE = LABORATORY      YELLOW = FILE      PINK = CLIENT

1) Chain of Custody Number = Client Determined  
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite  
 3) Field Filtered - for liquid matrices, associate with a - Y - for yes the sample was field filtered or - N - for sample was not field filtered  
 4) Matrix Codes: BW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, W = Water, ML = Misc. Liquid, SL = Solid, SS = Solid Waste, O = Oil, F = Filter, P = Wipe, U = Urine, F = Fecal, N = Nasal  
 5) Sample Analysis Requested - Analytical method requested (ie #2500, 60100/7470A) and number of containers provided for each (ie 42500 - 3, 60100/7470A - 1)  
 6) Preservative Type: BA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Acetate, SA = Sodium Fluoride, SA = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate, if no preservative is added = leave field blank



## GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

GEL Work Order Number:

Client Name: Entergy Phone #: (914) 736-8405 Fax #: (914) 734-6247  
 Project/Site Name: Indian Point Energy Center  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: Miguel Britos Send Results To: Patrick Donahue  
 Sample ID  
 \*For composites: indicate start and stop date/time

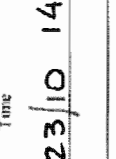
Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code	Field Filtered (Y/N)	Sample Matrix (1)	Should this sample be considered:		Total number of containers	Gamma Spec (C/S)	Strontium 90 (S/90)	Preservative Type (6)	Comments
						Radioactive	TSCA Regulated					
MW-31-49-(026)	08/23/10	1211	N	N	GW	Y	N	1	1	1		Note: extra sample is required for sample specific QC
MW-31-63-(026)	08/23/10	1311	N	N	GW	Y	N	1	1	1		2 Liter Poly
MW-31-85-(026)	08/23/10	1210	N	N	GW	Y	N	1	1	1		2 Liter Poly

TAT Requested: Normal:  Rash: \_\_\_\_\_ Specify: \_\_\_\_\_ (Subject to Surcharge: Yes / No) Fax Results: Yes / No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Mountain

### Chain of Custody Signatures

Requested By (Signed)	Date	Time	Received By (Signed)	Date	Time
	08/23/10	1450	ERIN TRENT	08/23/10	1450

Method of Shipment: FEDEX Date Shipped: \_\_\_\_\_

Airbill #: \_\_\_\_\_

Airbill #: \_\_\_\_\_

For Lab Receiving Use Only  
 Custody Seal Intact? YES / NO  
 Cooler Temp: \_\_\_\_\_

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

1) Chain of Custody Number = Client Determined  
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite  
 3) Field Filtered: For liquid matrices, indicate with a - V - for yes the sample was field filtered or - N - for sample was not field filtered  
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SO=Soil, SD=Soil, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Pipe, U=Urine, F=Food, N=Nutrient  
 5) Sample Analysis Requested: Analytical method requested (i.e. R2600, 60106/7470A) and number of containers provided for each (i.e. 426UB - 3, 60106/7470A - 1)  
 6) Preservative Type: BA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank  
 WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT

Page: 1 of 1  
 Project #: **Energy GW Mon Prog**  
 GEL Quote #:   
 COC Number:   
 PO Number: 50013510

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

**GEL Work Order Number:**

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

**Client Name:** Energy      **Phone #:** (914) 736-8405      **Sample Analysis Requested (5):** (Fill in the number of containers for each test)

**Project/Site Name:** Indian Point Energy Center      **Fax #:** (914) 734-6247

**Address:** 450 Broadway, Suite 3, Buchanan, NY 10511

**Collected by:** Miguel Britos      **Send Results To:** Patrick Donahue

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hhmm)	QC Code (2)	Field Filtered (3)	Sample Matrix (4)	Should this sample be considered:		Total number of containers	Sample Analysis Requested (5)					Preservative Type (6)	Comments	
						Radioactive	TSCA Regulated		1	2	3	4	5			6
MW-32-48-(008)	08/24/10	1403	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	Note: extra sample is required for sample specific QC
MW-32-59-(020)	08/24/10	1422	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-32-85-(023)	08/24/10	1103	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-32-149-(020)	08/24/10	1127	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-32-173-(018)	08/24/10	1123	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	
MW-32-190-(022)	08/24/10	1137	N	N	GW	Y	N	1	1	1	1	1	1	1	2 Liter Poly	

**TAT Requested:** Normal:  Rush:  Specify: \_\_\_\_\_ **Specify:** \_\_\_\_\_ **Yes / No** **Circle Deliverable:** C=of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

**Remarks:** Are there any known hazards applicable to these samples? If so, please list the hazards

**Chain of Custody Signatures**

Received By (Signed)	Date	Time	Received by (Signed)	Date	Time
<i>[Signature]</i>	08/24/10	1535	SECURED	08/24/10	1535
<i>[Signature]</i>	08/24/10	1535	STORAGE	08/24/10	1535

**Sample Shipping and Delivery Details**

**GEL PM:** ERIN TRENT      **Method of Shipment:** FEDEX      **Date Shipped:**

**Airbill #:**      **Airbill #:**

**For Lab Receiving Use Only**

**Custody Seal Broken?** YES / NO

**Cooler Temp:** C

1. Chain of Custody Number = Client Determined  
 2. QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate, Sample, G = Grab, C = Composite  
 3. Field Filtered: For liquid matrices, indicate with a 'F' for yes the sample was field filtered or 'N' for no. For solid matrices, indicate with a 'F' for yes the sample was field filtered or 'N' for no.  
 4. Matrix Codes: DW=Drinking Water, CW=Cooling Water, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SQ=Soil, SD=Soil, SS=Sludge, SL=Sludge, P=Particulate, F=Fuel, N=Nasal  
 5. Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B, 7470A) and number of containers provided for each (i.e. 8260B - 3, 6010B/7470A - 4)  
 6. Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, BV = Boric Acid, ST = Sodium Thiosulfate. If no preservative is added a box for a blank

**WHITE = LABORATORY      YELLOW = FILE      PINK = CLIENT**

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

Client Name: Entergy  
Project/Site Name: Indian Point Energy Center  
Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
Phone #: (914) 736-8405  
Fax #: (914) 734-6247  
Sample Analysis Requested (5) (Fill in the number of containers for each test)

Sample ID <i>* For composites - indicate start and stop date/time</i>	*Date Collected (mm-dd-yy)	*Time Collected (Military/Abbrev)	QC Cook #	Field Filtered #	Sample Matrix (Matrix #)	Should this sample be considered:		Total number of containers	Tritium (H3) Gamma Spec (GS) Strontium 90 (Sr90)	Preservative Type (6)	Comments Note: extra sample is required for sample specific QC
						Radioactive	TSC A Regulated				
MW-51-40-(016)	08/25/10	1629	N	N	GW	Y	N	1	1		2 Liter Poly
MW-51-79-(016)	08/25/10	1647	N	N	GW	Y	N	1	1		2 Liter Poly
MW-51-104-(014)	08/25/10	1318	N	N	GW	Y	N	1	1		2 Liter Poly
MW-51-135-(014)	08/25/10	1321	N	N	GW	Y	N	1	1		2 Liter Poly
MW-51-163-(014)	08/25/10	1351	N	N	GW	Y	N	1	1		2 Liter Poly
MW-51-189-(014)	08/25/10	1313	N	N	GW	Y	N	1	1		2 Liter Poly

TAT Requested: Normal:  Rush:  Specify: (Subject to Schedule)  Yes /  No  
Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards  
 Sample Collection Time Zone:  Eastern  Pacific  Other: \_\_\_\_\_  
 Maintenance: \_\_\_\_\_

Chain of Custody Signatures:  
 Received by (signature) Date Time  
 ERIN TRENT 08/27/10 0930  
 Method of Shipment: FEDEX  
 Airbill #: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_

For Lab Receipt Log Use Only  
 Custom Seal Initialed? YES  
 Custom Temp \_\_\_\_\_

1) Chain of Custody Number - Client Determined  
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite  
 3) Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or - N - for no sample was not field filtered.  
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, W=Water, ML=Misc Liquid, SO=Soil, SD=Soil/Sediment, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Paper, U=Urine, F=Food, S=Soil  
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B, 7470A) and number of containers provided for each (i.e. 4250B - 3, 6010B 7470A - 1)  
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexane, ST = Sodium Thiosulfate. If no preservative is added = leave field blank  
 WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT

# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number: 50013510

Project #: <u>Entergy GW Mon Prog</u>	Phone #: (914) 736-8405									
GEL Quote #: _____	Fax #: (914) 734-6247									
PO Number: 50013510	Client Name: Entergy									
Project/Site Name: Indian Point Energy Center	Address: 450 Broadway, Suite 3, Buchanan, NY 10511									
Collected by: <u>Miguel Britos</u>	Send Results To: Patrick Donahue									
Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military)	QC Code	Field Filtered	Sample Matrix	Should this sample be considered:	Total number of containers	Sample Analysis Requested (6)	Preservative Type (6)	Comments
MW-40-27-(012)	08/26/10	1442	N	N	GW	Radioactive	1	Tritium (H3)	Strontium 90 (Sr90)	Note: extra sample is required for sample specific QC
MW-40-46-(013)	08/26/10	1456	N	N	GW	TSCA Regulated	1			
MW-40-81-(013)	08/26/10	1105	N	N	GW		1			
MW-40-100-(015)	08/26/10	1109	N	N	GW		1			
MW-40-127-(015)	08/26/10	1116	N	N	GW		1			
MW-40-162-(013)	08/26/10	1229	N	N	GW		1			

TAT Requested: Normal  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ (Subject to: Surcharge) Yes / No / No  
 Fax Results: \_\_\_\_\_

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

### Chain of Custody Signatures

Received By (Signature)	Date	Time
	08/27/10	0931
	08/27/10	0931

### Sample Shipping and Delivery Details

GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX  
 Date Shipped:  
 Airbill #:  
 Airbill #:

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

1) Chain of Custody Number: Client Determined  
 2) QC Codes: N - Normal Sample, EB - Equipment Blank, MS - Matrix Spike Sample, MSD - Matrix Spike Duplicate Sample, G - Grab, C - Composite  
 3) Field Filtered: For liquid matrices, indicate with a Y - for yes the sample was field filtered or a N - for no sample was field filtered.  
 4) Matrix Codes: DW - Drinking Water, GW - Groundwater, SW - Surface Water, WW - Waste Water, WAW - Water, M - Misc - Liquid, SD - Soil, SD-Sol - Solid, SS - Solid Waste, O-GH - Filter, P - Wipe U - Urine, F - Fecal, N-Nasal  
 5) Sample Analysis Requested: Analytical method requested (i.e. 8160B, 6010B, 7470A) and number of containers provided for each (i.e. 4250B - 3, 6010B - 2, 7470A - 1)  
 6) Preservative Type: HA - Hydrochloric Acid, NI - Nitric Acid, SH - Sulfuric Acid, AA - Acetic Acid, HX - Hexane, ST - Sodium Thiosulfate. If no preservative is added - leave field blank  
 WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT  
 For Lab Receiving Use Only:  
 Custody Seal Intact? YES / NO  
 Cooler Temp: \_\_\_\_\_

Page: 1 of 1  
 Project #: **Entergy GW Mon Prog**  
 GEL Quote #:  
 COC Number (1):  
 PO Number: 50013510

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

**GEL Work Order Number:**

GEL Laboratories, LLC  
 3040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 356-8171  
 Fax: (843) 766-1178

Client Name: **Entergy** Phone #: **(914) 736-8405**

Project/Site Name: **Indian Point Energy Center** Fax #: **(914) 734-6247**

Address: **450 Broadway, Suite 3, Buchanan, NY 10511**

Collected by: **M. Britos** Send Results To: **Patrick Donahue**

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code (2)	Field Filtered (3)	Sample Matrix (4)	Should this sample be considered: (5)	Total number of containers	Gamma Spec (GS)	Tritium (H3)	Strontium 90 (Sr90)	Preservative Type (6)	Comments
MW-111-(033)	08/27/10	1521	N	N	GW	Radioactive	1	1	1	1		Note: extra sample is required for sample specific QC
												2 Liter Poly

TAT Requested: Normal  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ Fax Results: Yes / No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Other \_\_\_\_\_

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

### Chain of Custody Signatures

Received by (Signed)	Date	Time
<i>[Signature]</i>	08/27/10	1530

GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX  
 Date Shipped:

Airbill #: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_

For Lab Receiving Use Only:  
 Custody Seal Intact? YES/NO  
 Cooler Temp. \_\_\_\_\_

1) Chain of Custody Number at Client Determined  
 2) QC Codes: N=Normal Sample, FB= Trip Blank, FD= Field Duplicate, EB= Equipment Blank, MS= Matrix Spike Sample, MSD= Matrix Spike Duplicate Sample, G= Grab, C=Composite  
 3) Field Filtered: For liquid matrices, indicate with a 'Y' - for yes, the sample was field filtered or - 'N' - for sample was not field filtered  
 4) Matrix Codes: BW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc Liquid, SO=Soil, SD=Soil, SL=Sludge, SB=Soil, SW=Soil, F=Fecal, N=Nasa  
 5) Sample Analysis Requested: Analytical method requested (ie: 8360B, 6010B7PMA) and number of containers provided for each (ie: 8360B - 3 6010B7PMA)  
 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sulfuric Acid, AA = Acetic Acid, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

**WHITE = LABORATORY      YELLOW = FILE      PINK = CLIENT**

Page: 1 of 1  
 Project #: Entergy GW Mon Prog  
 GEL Quote #:   
 COC Number: 50013510  
 PO Number:   
**GEL Chain of Custody and Analytical Request**  
 \*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*  
 GEL Work Order Number:  
 GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

Client Name: Entergy Phone #: (914) 736-8405  
 Project/Site Name: Indian Point Energy Center Fax #: (914) 734-6247  
 Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
 Collected by: M. Britos Send Results To: Patrick Donahue

Sample ID <small>* For composites - indicate start and stop date/time</small>	Date Collected (mm-dd-yy)	Time Collected (Military Time)	QC Code (N/A)	Field Filtered (Y/N)	Sample Matrix (MSD)	Should this sample be considered:		Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)						Preservative Type (6)		
						Radioactive	TSCA Regulated	Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)				Comments	
MW-33-(027)	08/30/10	1429	N	N	GW	Y	N	1	1	1						2 Liter Poly Note: extra sample is required for sample specific QC

TAT Requested: Normal  Rush  Specify: \_\_\_\_\_ Fax Results: Yes  No   
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4  
 Sample Collection Time Zone: Eastern  Pacific  Central  Other   
 Mountain

Chain of Custody Signatures  
 Received by (signed) Date Time  
 SECURED 08/30/10 1531  
 STORAGE 08/30/10 1531  
 Date Shipped: FEDEX  
 Airbill #:   
 Airbill #:

For Lab Receiving Use Only  
 Custody Seal Intact? YES  NO   
 Cooler Temp: \_\_\_\_\_ C

1) Chain of Custody Name = Client Determined  
 2) QC Codes: N = Normal Sample, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate Sample, G = Grab, C = Composite  
 3) Field Filtered: For liquid matrices, indicate with a Y - for yes the sample was field filtered or a N - for sample was not field filtered  
 4) Matrix Codes: DW = Drinking Water, GW = Groundwater, SW = Surface Water, WW = Waste Water, ML = Milk, LQ = Liquid, SO = Soil, SD = Sediment, SL = Sludge, SS = Solid Waste, O = Oil, F = Filter, P = Filter, U = Urine, F = Fecal, N = Nail  
 5) Sample Analysis Requested: Analytical methods requested (i.e. 8266B, 8010B, 7770A) and number of containers provided for each (i.e. 8266P: 3, 6010P/7770A: 1)  
 6) Preservative Type: HA = Hydrochloric Acid, M = Nitric Acid, SB = Sodium Borate, SA = Sulfuric Acid, AA = Ascorbic Acid, BK = Benzene, ST = Sodium Thiosulfate. For preservative included = form field blank  
 WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT





# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

Project #: Entergy GW Mon Prog  
 GEL Quote #: \_\_\_\_\_  
 COC Number<sup>1)</sup>: \_\_\_\_\_  
 PO Number: 50013510

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

Client Name: Entergy

Phone #: (914) 736-8405

Sample Analysis Requested<sup>3)</sup> (Fill in the number of containers for each test)

Project/Site Name: Indian Point Energy Center

Fax #: (914) 734-6247

Address: 450 Broadway, Suite 3, Buchanan, NY 10511

Collected by: M. Britos Send Results To: Patrick Donahue

Sample ID  
 \* For composites - indicate start and stop date/time

Sample ID	*Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code	Field Filtered <sup>4)</sup>	Sample Matrix <sup>5)</sup>	Kathylene	Should this sample be considered:		Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	Preservative Type (6)	Comments
							TSCA Required	Radionuclide						
MW-31-49-(027)	09/07/10	1349	N	N	GW	Y	N	Y	1	1	1			2 Liter Poly
MW-31-63-(027)	09/07/10	1528	N	N	GW	Y	N	Y	1	1	1			2 Liter Poly
MW-31-85-(027)	09/07/10	1414	N	N	GW	Y	N	Y	1	1	1			2 Liter Poly

TAT Requested: Normal:  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ Fax Results: Yes /  No  
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Chain of Custody Signatures			Sample Shipping and Delivery Details		
Relinquished By (Signed)	Date	Time	Received by (Signed)	Date	Time
<i>[Signature]</i>	09/09/10	0850	<i>[Signature]</i>	09/09/10	0850

GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX Date Shipped: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_  
 Airbill #: \_\_\_\_\_

1) Chain of Custody Number - Client Determined  
 2) QC Codes: N = Normal Sample; FB = Field Duplicate; FB = Equipment Blank; MS = Matrix Spike Sample; MSD = Matrix Spike Duplicate Sample; C = Comb; C = Composite  
 3) Field Filtered: For liquid matrices, indicate with 1 - Y - (Y for yes the sample was field filtered or - N - for sample was not field filtered  
 4) Matrix Codes: DW - Drinking Water; GW - Groundwater; SW - Surface Water; WW - Wastewater; ML - Mill; LQ - Leachate; SD - Sediment; SL - Sludge; SS - Solid Waste; O - Oil; F - Filter; P - Pipe; U - Urtic; F - Fecal; N - Nasal  
 5) Sample Analysis Requested - Analytical method requested (i.e. 8260B, 6010B/7470A) and number of containers provided for each (i.e. 9/6B - 3, 6010B/7470A - 1)  
 6) Preservative Type: HA = Hydrofluoric Acid; N = Nitric Acid; SH = Sulfuric Acid; SA = Sulfuric Acid; AA = Acetic Acid; HX = Hexanoic Acid; leave field blank

For Lab Receiving Use Only  
 Custody Seal Intact? YES  
 Cooler Temp: MO  
C

WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT



Page: 1 of 1  
 Project #: **Energy GW Mon Prog**  
 GEL Quote #:  
 COC Number #:  
 PO Number: 50013510

**GEL Chain of Custody and Analytical Request**

GEL Laboratories, LLC  
 2040 Savage Road  
 Charleston, SC 29407  
 Phone: (843) 556-8171  
 Fax: (843) 766-1178

GEL Work Order Number:  
 \*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

Client Name: **Energy** Phone #: **(914) 736-8405**  
 Project/Site Name: **Indian Point Energy Center** Fax #: **(914) 734-6247**  
 Address: **450 Broadway, Suite 3, Buchanan, NY 10511**  
 Collected by: **M. Batos** Send Results To: **Patrick Donahue**

Sample ID <i>* For composites, indicate start and stop date/time</i>	Date Collected (mm-dd-yy)	Time Collected (Military (hhmm))	QC Code	Field Filtered	Sample Matrix	Should this sample be considered:		Sample Analysis Requested <sup>15</sup> (Fill in the number of containers for each test)		Preservative Type (6)	Comments
						Radioactive	TSCA Regulated	Total number of containers			
MW 30 69-(035)	09/08/10	1235	N	N	GW	Y	N	1	1	1	Note: extra sample is required for sample specific QC
MW 30-84-(026)	09/08/10	1314	N	N	GW	Y	N	1	1	1	

TAT Requested: Normal:  Rush:  Specify:  Fax Results: Yes / No  No   
 Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4  
 Sample Collection Time Zone: Eastern Central Mountain Pacific Other

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**  
 Chain of Custody Signatures  
 Received by (Signed) Date Time  
 1. *[Signature]* 09/08/10 1445  
 2. *[Signature]* 09/08/10 1445  
 3. *[Signature]* 09/08/10 1445  
 GEL PM: ERIN TRENT  
 Method of Shipment: FEDEX  
 Date Shipped:  
 Airbill #:  
 Airbill #:

1. Chain of Custody Number a Client Determined  
 2. QC Code: N = Normal Sample, FB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Sample, MSD = Matrix Spike Duplicate, Sample G, G, C = Composite  
 3. Field Filtered: For liquid matrices, indicate with Y or N. For solids the sample was field filtered or N - for sample was not field filtered  
 4. Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Mix-Liquid, SD=Soil, SP=Soil, SL=Sludge, SS=Solid Waste, Q=Oil, F=Fuel, P=Pipe, U=Line, F=Feed, N=Neut  
 5. Sample Analysis Requested: Analytical method requested (i.e. 8240B, 8010B, 7470A) and number of containers provided for each (i.e. 8250.B - 3, 6910B/7470A - 1).  
 6. Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, HX = Hexanic Acid, ST = Sodium Thiosulfate. If no preservative is added = leave field blank  
 WHITE = LABORATORY  
 YELLOW = FILE  
 PINK = CLIENT  
 For Lab Receiving Use Only  
 Custody Seal intact?  
 YES NO  
 Cooler Temp:  
 C

# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1173

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Work Order Number:

Page: 1 of 1  
Project #: **Entergy GW Mon Prog**  
GEL Quote #:  
COC Number: **50013510**  
PO Number:

Client Name: **Entergy** Phone #: **(914) 736-8405**  
Project/Site Name: **Indian Point Energy Center** Fax #: **(914) 734-6247**  
Address: **450 Broadway, Suite 3, Buchanan, NY 10511**

Sample Analysis Requested <sup>(5)</sup> (Fill in the number of containers for each test)

Collected by: **M. Britos** Send Results To: **Patrick Donahue**

\* For composites - indicate start and stop date/time

Sample ID	Date Collected (mm-dd-yy)	Time Collected (Military) (hh:mm)	QC Code (a)	Field Filtered (b)	Sample Matrix (c)	Radioactive	Should this sample be considered:	Total number of containers	Tritium (H3)	Gamma Spec (GS)	Strontium 90 (Sr90)	Preservative Type (6)	Comments
MW-32-59-(021)	09/09/10	1357	N	N	GW	Y	N	1	1	1	1	2 Liter Poly	Note: extra sample is required for sample specific QC
MW-32-85-(024)	09/09/10	1529	N	N	GW	Y	N	1	1	1	1	2 Liter Poly	
MW-32-149-(021)	09/09/10	1136	N	N	GW	Y	N	1	1	1	1	2 Liter Poly	
MW-32-173-(019)	09/09/10	1129	N	N	GW	Y	N	1	1	1	1	2 Liter Poly	
MW-32-190-(023)	09/09/10	1134	N	N	GW	Y	N	1	1	1	1	2 Liter Poly	

TAT Requested, Normal:  Rush:  Specify: (Subject to Surcharges) Fax Results: Yes / No  No  Yes

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern Pacific Other Mountain

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Chain of Custody Signatures

Requested By (Signed)	Date	Time	Received by (Signed)	Date	Time
<i>[Signature]</i>	09/09/10	1600	<i>[Signature]</i>	09/09/10	1600

GEL PM: **ERIN TRENT** Method of Shipment: **FEDEX** Date Shipped:

Airbill #: **2** Airbill #:

For Lab Receiving Use Only

Checked Serial Number? **YES** **NO**

Check Trip: **C**

1) Chain of Custody Number = Client Determined  
 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike, Sample, MSD = Matrix Spike Duplicate, Sample, G = Grab, C = Composite  
 3) Field Filtered: For liquid matrices, indicate with a - Y - for yes the sample was field filtered or a - N - for sample was not field filtered  
 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Misc. Liquid, SO=Soil, SD=Soil, SS=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Wipe, U=Urine, F=Excal, N=Nasal  
 5) Sample Analysis Requested: Analytical method requested (i.e. 8260B, 6010B, 4790A) and number of containers requested for each (i.e. 8260B - 3, 6010B/4790A - 1)  
 6) Preservative Type: HA = Hydrochloric Acid, M = Nitric Acid, SH = Sulfamic Acid, AA = Acetic Acid, BX = Boric Acid, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

**WHITE = LABORATORY**  
**YELLOW = FILE**  
**PINK = CLIENT**

# GEL Chain of Custody and Analytical Request

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

Project #: 1 of 1 Entry GW Mon Prog  
GEL Quote #: \_\_\_\_\_  
COC Number <sup>(1)</sup>: \_\_\_\_\_  
PO Number: 50013510

Client Name: Entergy  
Phone #: (914) 736-8405  
Fax #: (914) 734-6247

Project/Site Name: Indian Point Energy Center  
Address: 450 Broadway, Suite 3, Buchanan, NY 10511  
Collected by: M. Britos Send Results To: Patrick Donahue

GEL Work Order Number: \_\_\_\_\_  
Sample Analysis Requested <sup>(6)</sup> (Fill in the number of containers for each test)

Sample ID	Date Collected (mm-dd-yy)	*Time Collected (Military) (hh:mm)	QC Code	Field Filtered <sup>(3)</sup>	Sample Matrix <sup>(4)</sup>	Total number of containers	TSCA Regulated	Radioactive	Sample this considered:	Sample Analysis Requested <sup>(6)</sup>				Preservative Type (6)	Comments
										Gamma Spec (GS)	Tritium (H3)	Strontium 90 (Sr90)	Level 1		
MI-5-(012)	09/10/10	1530	N	N	GW	1	N	Y		1	1	1		2 Liter Poly	Note: extra sample is required for sample specific QC

TAT Requested: Normal:  Rush: \_\_\_\_\_ Specify: \_\_\_\_\_ (Subject to Surcharges) Fax Results: Yes /  No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Sample Collection Time Zone: Eastern / Pacific / Other / Mountain

Remarks: Are there any known hazards applicable to these samples? If so, please list the hazards

Received By (Signature)	Date	Time
	09/10/10	1559

Method of Shipment: FEDEX Date Shipped: \_\_\_\_\_  
Airbill #: \_\_\_\_\_  
Airbill #: \_\_\_\_\_

For Lab Receiving Use Only  
Capacity Seal Intact? YES  
Cooler Temp: NO  
C

- 1) Chain of Custody Number = Client Determined  
2) QC Codes: N = Normal, Sample; TB = Trip Blank; FD = Field Duplicate; EB = Equipment Blank; MS = Matrix Spike Sample; MSD = Matrix Spike Duplicate Sample; G = Grab; C = Composite  
3) Field Filtered: For liquid matrices, indicate with a Y - for yes the sample was field filtered or a N - for sample was not field filtered  
4) Matrix Codes: DW = Drinking Water; GW = Groundwater; SW = Surface Water; WW = Waste Water; ML = Micro Liquid; SO = Soil; SD = Sediment; SL = Sludge; SS = Solid Waste; O = Oil; F = Filter; P = Wipe; U = Urine; F = Fecal; N = Nsal  
5) Sample Analysis Requested: Analytical method requested (ie 8260B, 6010B/7470A) and number of containers provided for each (ie 8260B - 3, 6010B/7470A - 1)  
6) Preservative Type: HA = Hydrochloric Acid; NI = Nitric Acid; SH = Sulfuric Acid; SA = Acetic Acid; BA = Boric Acid; HX = Hexane; ST = Sodium Thiosulfate. If no preservative is added, leave field blank

WHITE = LABORATORY  
YELLOW = FILE  
PINK = CLIENT

Sample Shipping and Delivery Details

# GEL Chain of Custody and Analytical Request

\*\*See www.gel.com for GEL's Sample Acceptance SOP\*\*

GEL Laboratories, LLC  
2040 Savage Road  
Charleston, SC 29407  
Phone: (843) 556-8171  
Fax: (843) 766-1178

**GEL Work Order Number:**

Client Name: **Entergy**

Phone #: (914) 736-8405

Sample Analysis Requested <sup>15</sup>: (Fill in the number of containers for each test)

Project/Site Name: **Indian Point Energy Center**

Fax #: (914) 734-6247

Address: **450 Broadway, Suite 3, Buchanan, NY 10511**

Collected by: **M. Britos** Send Results To: **Patrick Donahue**

Sample ID

\* For composites - indicate start and stop date/time

MW-111-(034)

\*Due Collected (mm-dd-yy) **09/10/10 14:09**

QC Code <sup>2</sup>

Field Filtered <sup>3a</sup>

Sample Matrix <sup>4</sup>

Should this sample be considered:

Yes  A Regulated

Radionuclide

Total number of containers

Gamma Spec (GS)

Tritium (H3)

Strontium 90 (Sr90)

Preservative Type (6)

Comments

Note: extra sample is required for sample specific QC

2 Liter Poly

TAT Requested: Normal:  Rush:  Specify: \_\_\_\_\_ Subject to: (Surcharge)  Yes  No

Circle Deliverable: C of A / QC Summary / Level 1 / Level 2 / Level 3 / Level 4

Remarks: **Are there any known hazards applicable to these samples? If so, please list the hazards**

Sample Collection Timing Zone

Eastern  Pacific  Central  Mountain

### Chain of Custody Signatures

Received by (signed) \_\_\_\_\_ Date \_\_\_\_\_ Time \_\_\_\_\_

SECURED

09/10/10 1600

STORAGE

09/10/10 1600

### Sample Shipping and Delivery Details

GEL PM: **ERIN TRENT**

Method of Shipment: **FEDEX**

Date Shipped:

Airbill #:

Airbill #:

- 1) Chain of Custody Number = Client Determined
- 2) QC Codes: N = Normal Sample, TB = Trip Blank, FD = Field Duplicate, EB = Equipment Blank, MS = Matrix Spike Duplicate Sample, G = Grab, C = Composite
- 3) Field Filtered: For liquid matrices, indicate with a 'Y' - for yes the sample was field filtered or a 'N' - for sample was not field filtered
- 4) Matrix Codes: DW=Drinking Water, GW=Groundwater, SW=Surface Water, WW=Waste Water, W=Water, ML=Mineral Liquid, SOL=Sol: SD=Soil, SL=Sludge, SS=Solid Waste, O=Oil, F=Filter, P=Pipe, U=Line, F=Facet, N=Isol
- 5) Sample Analysis Requested: Analytical method requested (i.e. #266B, 6418B/7476A) and number of containers provided for each (i.e. #266B - 3, 6418B/7476A - 1)
- 6) Preservative Type: HA = Hydrochloric Acid, NI = Nitric Acid, SH = Sodium Hydroxide, SA = Sulfuric Acid, AA = Acetic Acid, DX = Deionized Water, ST = Sodium Thiosulfate. If no preservative is added = leave field blank

**WHITE = LABORATORY**

**YELLOW = FILE**

**PINK = CLIENT**

For Lab Receiving Use Only

Chain of Custody Intact?

YES  NO

Cooler Temp: \_\_\_\_\_ C





## **APPENDIX D 3<sup>RD</sup> QUARTER 2010 SAMPLING DATA SHEETS**

WELL ID: MW-33  
 SAMPLE ID: 027

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny 93°F

PROJECT NO: 01.0017869.92  
 DATE: 8/30/10  
 SAMPLER(S): M. BRITTS  
 PUMP DEPTH: 16 ft

MID QUARTER

WATER QUALITY: DTW = 8.04 Transducer Actual Depth : 17.427 Transd. reading = 10.683

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Purged Notes H <sub>2</sub> O (gal)	
1047	17.422									
1100	17.333	NOT ENOUGH WATER IN FLOW CELL							0.20	
1105	17.323	27.88	0.368	5.73	7.35	266.1	—		0.10	
1110	17.319	27.62	0.691	2.79	7.31	240.6	—		0.14	
1115	17.319	27.51	0.653	2.15	7.29	210.5	12.06		0.15	
1125	17.327	27.72	0.632	1.31	7.29	192.2	12.63		0.16	
1130	17.325	27.92	0.625	1.88	7.27	197.0	12.46		0.17	
1138	17.333	28.11	0.621	1.33	7.27	170.1	12.39		0.18	
1148	17.335	28.34	0.612	1.44	7.29	151.7	12.58		0.20	
1156	17.336	28.58	0.612	1.44	7.28	145.1	12.61		0.22	
1201	17.336	28.63	0.611	1.39	7.27	143.6	12.53		0.25	
1206	17.338	28.67	0.609	1.37	7.27	141.0	12.59	↓	0.28	
1207		START SAMPLE COLLECTION								
1429		SAMPLE COMPLETED : 2 L IPEC								
		PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
flow meter	3
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged \_\_\_\_\_ gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-111  
 SAMPLE ID: 033

**GZA GeoEnvironmental of New York  
 Low-Flow Sampling Data Sheet**

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny 80°F

PROJECT NO: 01.001786992  
 DATE: 8/27/10  
 SAMPLER(S): M. BRITOS  
 PUMP DEPTH: 16.5 ft

**MID QUARTER**

WATER QUALITY: DTW = 8.10 Transducer Actual Depth 7.546 Transd. reading = 10.454

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Purged Notes H <sub>2</sub> O (gal)
1257	7.549		PUMP	ON					
1312	7.399		WATER	DID NOT REACH FLOW CELL YET					
1315	7.410	26.78	0.697	7.21	7.15	199.0	—		
1321	7.408	25.59	0.795	3.11	7.30	121.3			
1329	7.426	25.44	0.823	1.88	7.35	105.8	5.37		0.18
1338	7.421	25.61	0.824	1.44	7.30	105.5	5.76		0.23
1347	7.423	25.84	0.825	1.32	7.27	103.1	5.44		0.26
1356	7.411	25.86	0.828	1.30	7.27	103.6	5.50		0.31
1401	7.413	25.89	0.829	1.29	7.29	104.1	5.47		0.36
1402		START SAMPLE COLLECTION							
1521		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	
flow meter	1
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 0.36 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.



WELL ID: MW 40.162

SAMPLE ID: 013

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/26/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
158.7 to 190.3

TOTAL VOLUME PURGED: 0.60 gal

SAMPLING PORT  
162

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
0910	0	PUMP ON						6/9	42
0920	0.01	21.34	1.310	2.29	6.26	-116.4	—	6/9	42
0930	0.02	21.54	1.305	0.73	6.28	-120.9	—	6/9	45
0940	0.05	21.58	1.303	0.49	6.30	-140.3	5.83		
0950	0.10	21.42	1.304	0.40	6.38	-150.7	7.60		
0957	0.15	21.29	1.302	0.35	6.45	-153.4	7.62		
1003	0.20	21.16	1.301	0.35	6.53	-156.3	6.62		
1013	0.25	21.15	1.299	0.30	6.67	-156.8	7.67		
1019	0.30	21.14	1.298	0.30	6.73	-154.6	6.50		
1028	0.35	21.11	1.299	0.27	6.83	-154.7	6.21		
1035	0.40	21.15	1.298	0.27	6.90	-155.6	6.14		
1042	0.45	21.07	1.303	0.27	6.91	-153.7	6.12	↓	↓
1043		PUMP OFF							
1045		START SAMPLE COLLECTION							
1229		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 40.127

SAMPLE ID: 015

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/26/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
125.2 to 136.7

TOTAL VOLUME PURGED: 1.20 gal

SAMPLING PORT  
127

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

2

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
0910	0	PUMP ON						6/9	42
0920	0.01	21.13	2.041	2.87	6.34	-110.1	—	6/9	42
0930	0.05	21.10	2.050	0.60	6.41	-125.1	—	6/9	45
0940	0.15	20.83	2.058	0.43	6.54	-131.7	4.71		
0950	0.25	20.25	2.065	0.29	6.78	-137.6	5.85		
0957	0.40	19.88	2.064	0.24	6.88	-142.9	6.15		
1003	0.55	19.72	2.065	0.21	6.92	-140.1	6.67		
1013	0.75	19.42	2.062	0.19	6.93	-143.5	6.36		
1019	0.85	19.34	2.061	0.18	6.94	-145.6	6.07		
1028	0.95	19.39	2.059	0.18	6.95	-146.7	6.10		
1035	1.05	19.36	2.057	0.17	6.95	-145.3	6.02	↓	↓
1037		PUMP OFF							
1039		START SAMPLE COLLECTION							
1116		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 40-100

SAMPLE ID: 015

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/26/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
93.2 to 106.7

TOTAL VOLUME PURGED: 2.50 gal

SAMPLING PORT  
100

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

3

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
0910	0	PUMP ON						6/9	42
0920	0.05	19.90	2.797	1.10	6.55	-104.5	—	6/9	42
0930	0.10	19.19	2.800	0.53	6.72	-101.3	—	6/9	45
0940	0.30	18.46	2.788	0.34	6.92	-76.2	14.16	↓	↓
0950	0.50	18.05	2.781	0.30	6.98	-52.9	11.21		
0957	0.70	17.88	2.772	0.35	7.01	-41.7	14.02		
1003	0.95	17.73	2.766	0.35	7.02	-35.2	12.32		
1013	1.20	17.55	2.755	0.38	7.04	-24.1	11.70		
1019	1.45	17.51	2.753	0.40	7.05	-18.2	8.69		
1028	1.75	17.53	2.756	0.42	7.06	-9.3	10.99		
1035	2.00	17.25	2.745	0.47	7.06	+4.2	11.78		
1042	2.20	17.30	2.738	0.48	7.06	+5.9	11.69		
1047	2.35	17.34	2.734	0.50	7.07	+6.4	11.74		
1048		PUMP OFF							
1049		START SAMPLE COLLECTION							
1109		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 40.81

SAMPLE ID: 013

**GZA GeoEnvironmental of New York  
Waterloo Sampling Data Sheet**

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/26/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
64.7 to 84.2

TOTAL VOLUME PURGED: 4.15 gal

SAMPLING PORT  
81

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

4

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
0910	0	PUMP ON						6/9	42
0920	0.10	18.71	5.903	2.01	6.62	-14.7	—	6/9	42
0930	0.30	18.36	5.958	1.66	6.57	-10.0	—	6/9	45
0940	0.50	17.75	5.989	1.50	6.56	-0.6	7.07		
0950	0.80	17.36	5.984	1.47	6.56	+7.4	4.44		
0957	1.10	17.23	5.973	1.46	6.56	12.7	6.89		
1003	1.40	17.11	5.966	1.46	6.57	17.1	6.22		
1013	1.80	17.00	5.957	1.43	6.62	23.7	5.91		
1019	2.05	16.97	5.959	1.43	6.64	26.5	5.80		
1028	2.50	16.99	5.959	1.42	6.65	27.6	5.77		
1035	2.80	16.78	5.957	1.43	6.66	34.4	6.61		
1042	3.20	16.80	5.963	1.41	6.68	35.9	6.54		
1047	4.00	16.84	5.960	1.41	6.68	36.7	6.51	↓	↓
1048		PUMP OFF							
1049		START SAMPLE COLLECTION							
1105		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>5</u> 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 40-46

SAMPLE ID: 013

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/26/10  
 SAMPLER(S): M. BRITUS

SAMPLING INTERVAL (depth in ft below top of casing)  
44.2 to 53.7

TOTAL VOLUME PURGED: 0.85 gal

SAMPLING PORT  
46 5

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)		
1327	0	PUMP ON						6/6	25		
1333	0.01	21.39	5.379	1.01	6.73	38.1	—	5/9	20		
1340	0.05	22.07	5.370	0.50	6.74	39.8	6.37	↓	↓		
1348	0.10	22.78	5.358	0.35	6.78	44.4	5.95				
1355	0.20	22.67	5.377	0.27	6.84	49.1	5.83				
1400	0.30	21.99	5.387	0.22	6.88	51.9	4.83				
1405	0.40	20.86	5.388	0.18	6.89	53.2	5.32				
1415	0.55	22.10	5.412	0.18	6.90	55.2	5.19				
1420	0.60	22.07	5.425	0.18	6.90	56.4	5.27				
1425	0.70	22.00	5.430	0.18	6.90	57.4	5.18				
1426		PUMP OFF									
1427		START SAMPLE COLLECTION									
		SAMPLE COMPLETED : 2 L IPEC									
		PUMP OFF									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 40.27

SAMPLE ID: 012

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/26/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
18.2 to 35.2

TOTAL VOLUME PURGED: 1.35 gal

SAMPLING PORT  
27

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

6

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1327	0	PUMP ON						6/6	25
1333	0.01	21.48	2.310	6.41	7.22	2.2	—	5/9	20
1340	0.05	21.23	4.585	6.20	7.09	33.9	7.07		
1348	0.15	21.00	4.620	5.80	7.03	58.3	6.56		
1355	0.30	20.74	4.664	5.48	7.01	69.5	6.41		
1400	0.50	20.15	4.705	5.46	6.99	75.3	5.14		
1405	0.60	20.19	4.721	5.00	6.99	79.0	6.29		
1415	0.90	20.17	4.761	4.80	6.99	81.5	5.88		
1420	1.05	20.10	4.768	4.78	6.99	81.8	5.79		
1425	1.20	20.09	4.778	4.72	6.99	81.5	5.76	↓	↓
1426		PUMP OFF							
1427		START SAMPLE COLLECTION							
1442		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF.							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 51-189

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/25/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
184.2 to 197.8

TOTAL VOLUME PURGED: 0.85 gal

SAMPLING PORT  
189

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1130	0	PUMP ON						5.6/5.6	48
1140	0.01	17.94	0.798	2.37	6.36	-71.3	—		
1150	0.05	16.69	1.421	0.98	6.77	-129.5	8.48		
1200	0.15	16.34	1.524	0.46	6.93	-168.3	7.98		
1207	0.25	16.29	1.528	0.36	6.95	-230.9	6.92		
1213	0.35	16.14	1.538	0.29	6.98	-280.1	5.27		
1222	0.45	15.87	1.540	0.25	6.99	-283.5	4.36		
1227	0.50	15.85	1.539	0.21	7.00	-283.7	4.20		
1234	0.60	15.89	1.544	0.20	7.03	-282.3	4.17		
1239	0.70	15.91	1.547	0.19	7.03	-283.2	4.13	↓	↓
1240		PUMP OFF							
1241		START SAMPLE COLLECTION							
1313		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 51-163

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/25/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
154.7 to 166.2

TOTAL VOLUME PURGED: 0.75 gal

SAMPLING PORT  
163 2

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1130	0	PUMP ON						5.6   5.6	48
1140	0.01	18.39	1.093	2.98	6.66	-69.6	—		
1150	0.02	17.68	2.104	1.12	6.57	-63.5	9.16		
1200	0.05	17.46	2.088	0.51	6.85	-71.7	7.18		
1207	0.10	17.34	2.074	0.46	6.94	-61.8	6.48		
1213	0.15	17.19	2.078	0.39	6.98	-51.6	6.51		
1222	0.25	16.80	2.084	0.26	7.00	-36.6	6.40		
1227	0.30	16.98	2.081	0.25	7.01	-30.0	6.27		
1234	0.40	16.97	2.087	0.25	7.03	-21.6	6.06		
1239	0.45	16.95	2.088	0.25	7.03	-21.7	6.00		
1247	0.50	16.99	2.088	0.26	7.04	-18.4	5.86		
1252	0.55	17.04	2.087	0.25	7.05	-17.7	5.90		
1257	0.60	17.08	2.087	0.24	7.05	-16.9	5.96	↓	↓
1258		PUMP OFF							
1259		START SAMPLE COLLECTION							
1351		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
turbidity meter	200701254

NOTES AND OBSERVATIONS:



WELL ID: MW 51-135

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/25/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
130.2 to 143.7

TOTAL VOLUME PURGED: 1.65 gal

SAMPLING PORT  
135 3

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1130	0	PUMP ON						5.6 / 5.6	48
1140	0.01	16.63	2.371	1.36	6.47	-85.5	-		
1150	0.10	15.92	2.446	0.59	6.86	-106.0	6.71		
1200	0.20	15.77	2.466	0.29	6.94	-67.6	5.67		
1207	0.40	15.70	2.470	0.26	6.97	-38.9	5.21		
1213	0.50	15.58	2.474	0.20	6.98	-20.9	5.06		
1222	0.65	15.35	2.472	0.15	6.99	-7.3	5.29		
1227	0.85	15.4	2.470	0.14	6.99	-2.2	4.87		
1234	1.00	15.4	2.475	0.10	7.00	+8.7	4.79		
1239	1.15	15.46	2.474	0.12	7.00	+8.9	5.10		
1247	1.30	15.51	2.467	0.10	7.00	13.2	4.90		
1252	1.40	15.59	2.471	0.10	7.01	14.7	4.82		
1257	1.50	15.61	2.472	0.09	7.01	15.2	4.89	↓	↓
1258		PUMP OFF							
1259		START SAMPLE COLLECTION							
1321		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 5L-104

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/25/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
130.2 to 143.7

TOTAL VOLUME PURGED: 3.25 gal

SAMPLING PORT  
104 4

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1130	0	PUMP ON						5.6/5.6	48
1140	0.05	15.29	2.582	2.00	6.52	-40.5	—		
1150	0.35	14.76	2.615	1.50	6.49	-24.0	7.08		
1200	0.60	14.62	2.624	1.48	6.53	-16.2	6.20		
1207	0.95	14.60	2.622	1.34	6.57	-11.3	5.38		
1213	1.30	14.43	2.625	1.24	6.65	-7.3	5.16		
1222	1.65	14.38	2.625	1.26	6.63	-2.0	5.07		
1227	1.90	14.44	2.628	1.29	6.65	-1.6	4.51		
1234	2.20	14.39	2.628	1.26	6.68	+2.	5.29		
1239	2.40	14.36	2.627	1.23	6.68	+3.4	5.17		
1247	2.60	14.4	2.623	1.23	6.69	6.6	5.00		
1252	2.80	14.50	2.632	1.26	6.72	8.6	4.71		
1257	2.95	14.49	2.630	1.23	6.74	9.0	4.66		
1302	3.10	14.53	2.630	1.21	6.74	9.9	4.73	↓	↓
1303		PUMP OFF							
1305		START SAMPLE COLLECTION							
1318		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 51-79

SAMPLE ID: 016

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/25/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
63.2 to 81.2

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
79 6

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1455	0	PUMP	ON					6.5/8.4	25
1505	0.05	16.27	2.709	1.60	6.59	-214.0	---	6.5/8.4	24
1511	0.15	16.37	2.712	1.37	6.78	-199.6	13.99		
1520	0.30	16.61	2.718	1.21	6.93	-183.5	9.50		
1528	0.42	16.50	2.725	1.21	6.98	-176.8	6.15		
1533	0.50	16.48	2.720	1.21	7.00	-165.0	5.69		
1538	0.60	16.57	2.718	1.21	7.01	-161.4	4.81		
1545	0.70	16.62	2.719	1.19	7.02	-156.5	6.71		
1553	0.85	16.64	2.717	1.21	7.02	-153.1	4.33		
1600	0.95	16.60	2.718	1.22	7.02	-153.9	6.88		
1612	1.05	16.67	2.714	1.21	7.02	-150.1	6.93		
1617	1.15	16.69	2.712	1.21	7.03	-148.9	6.85		
1618		PUMP	OFF						
1619		START SAMPLE COLLECTION							
1647		SAMPLE COMPLETED : 2 L IPEC							
		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u>6</u>
turbidity meter	<u>200701254</u>

NOTES AND OBSERVATIONS:

WELL ID: MW 51-40

SAMPLE ID: 016

**GZA GeoEnvironmental of New York  
Waterloo Sampling Data Sheet**

CLIENT: Energy - IPEC  
SITE: Buchanan, NY  
WEATHER: Cloudy 70's

PROJECT NO: 01.0017869.92  
DATE: 8/25/10  
SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
29.7 to 44.2

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
40 7

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1455	0	PUMP ON						6.5/8.4	25
1505	0.05	15.83	2.733	4.86	6.96	-11.1	—	6.5/8.4	24
1511	0.15	15.28	2.764	5.07	6.98	+10.2	0.24		
1520	0.45	15.28	2.779	5.27	6.98	32.1	0.59		
1528	0.70	15.17	2.784	5.13	6.98	36.5	1.69		
1533	0.80	15.12	2.783	5.15	6.98	40.1	0.95		
1538	0.95	15.21	2.781	5.26	6.98	42.1	3.94		
1545	1.10	15.21	2.781	5.20	6.98	45.0	3.00		
1553	1.30	15.22	2.779	5.10	6.98	48.2	1.48		
1600	1.50	15.19	2.782	5.08	6.98	49.7	1.41		
1607	1.65	15.26	2.773	5.05	6.98	51.0	1.47		
1608		PUMP OFF							
1609		START SAMPLE COLLECTION							
1629		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 32-190

SAMPLE ID: 022

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy, 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/24/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
180.3 to 193.9

TOTAL VOLUME PURGED: 0.85 gal

SAMPLING PORT  
190

PURGE RATE: variable (gal/min)  
 PURGE METHOD: Double Valve Pump  
MID QUARTER

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Press (psi)
929	0							10/12	49
940	0.01	21.33	1.755	0.28	6.87	-173.0	—		
950	0.05	21.47	1.746	0.28	6.88	-174.3	4.27		
1000	0.15	21.51	1.742	0.19	6.94	-172.6	4.09		
1010	0.25	21.37	1.743	0.12	7.04	-180.2	3.86		
1020	0.35	21.21	1.742	0.09	7.08	-174.8	2.23		
1027	0.45	21.03	1.742	0.08	7.10	-169.7	3.60		
1035	0.55	20.96	1.738	0.07	7.11	-146.4	4.39		
1040	0.60	20.93	1.737	0.06	7.12	-143.5	4.46		
1048	0.70	20.90	1.735	0.05	7.12	-140.2	4.50	↓	↓
1049		PUMP OFF							
1052		START SAMPLE COLLECTION							
1137		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 32 - 173

SAMPLE ID: 018

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Cloudy, 70's

PROJECT NO: 01.0017369.92  
DATE: 8/24/10  
SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
165.8 to 174.3

TOTAL VOLUME PURGED: 1.10 gal

SAMPLING PORT  
173

PURGE RATE: variable (gal / min)  
PURGE METHOD: Double Valve Pump  
MID QUARTER

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
0929								10/12	49
0940	0.01	21.07	1.999	0.65	6.84	-148.1	—		
0950	0.05	21.35	1.981	0.55	6.84	-146.7	4.07		
1000	0.20	21.25	1.972	0.38	6.96	-153.1	3.86		
1010	0.40	21.01	1.977	0.26	7.06	-155.3	4.35		
1020	0.50	20.88	1.987	0.22	7.09	-154.2	3.93		
1027	0.65	20.74	1.996	0.21	7.10	-152.1	3.74		
1035	0.75	20.68	2.002	0.19	7.11	-144.1	3.29		
1040	0.80	20.64	2.006	0.19	7.11	-141.7	3.36		
1048	0.95	20.60	2.013	0.18	7.12	-139.6	3.27	↓	↓
1049		PUMP OFF							
1052		START SAMPLE COLLECTION							
1123		SAMPLE COMPLETED			: 2	L IPEC			
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 32-149

SAMPLE ID: 020

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Cloudy, 70's

PROJECT NO: 01.0017869.92  
DATE: 8/24/10  
SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
147.3 to 156.8

TOTAL VOLUME PURGED: 0.70 gal

SAMPLING PORT 149 3

PURGE RATE: variable (gal/min)  
PURGE METHOD: Double Valve Pump  
MID QUARTER

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressu (psi)
0929								10   12	49
0940	0.01	21.41	1.549	0.86	6.80	-187.0	—		
0950	0.02	21.57	1.555	0.64	6.82	-183.6	3.02		
1000	0.10	21.44	1.734	0.43	6.84	-176.1	2.78		
1010	0.20	21.25	1.896	0.27	6.99	-145.8	2.46		
1020	0.30	21.11	1.952	0.22	7.08	-131.2	2.45		
1027	0.40	20.94	1.978	0.18	7.09	-123.3	2.39		
1035	0.50	20.87	1.991	0.18	7.11	-120.1	2.43		
1040	0.55	20.85	1.996	0.18	7.12	-117.9	2.46	↓	↓
1041		PUMP OFF							
1043		START	SAMPLE COLLECTION						
1127		SAMPLE COMPLETED:	2 L	IPEC					
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
turbidity meter	200704293

NOTES AND OBSERVATIONS:







WELL ID: MW 32 . 59

SAMPLE ID: 020

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy, 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/24/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
28.3 to 61.3

TOTAL VOLUME PURGED: 1.40 gal

SAMPLING PORT  
59

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

6  
 MID QUARTER

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
1244	0	PUMP	ON					8/8	26
1252	0.05	21.32	0.513	5.13	6.81	36.0	—		
1257	0.10	21.19	0.461	5.58	6.97	48.2	6.91		
1302	0.25	21.11	0.421	6.09	7.17	43.3	6.40		
1309	0.40	21.07	0.397	6.48	7.40	39.2	4.44		
1317	0.60	21.02	0.382	6.48	7.58	44.4	7.39		
1323	0.75	20.95	0.377	6.61	7.71	45.8	7.39		
1333	0.85	20.96	0.367	6.64	7.86	52.1	7.61		
1338	0.95	20.96	0.366	6.49	7.88	53.3	7.70		
1343	1.05	20.99	0.365	6.42	7.93	56.3	7.32		
1348	1.15	20.95	0.364	6.42	7.95	57.8	7.38		
1353	1.25	20.92	0.364	6.40	7.99	59.1	7.40	↓	↓
1354		PUMP	OFF						
1356		START	SAMPLE COLLECTION						
1422		SAMPLE	COMPLETED : 2 L IPEC						
		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200704293

NOTES AND OBSERVATIONS:



WELL ID: MW 31-85

SAMPLE ID: 025

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Showers, 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/23/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
69.8 to 85.4

TOTAL VOLUME PURGED: 0.90 gal

SAMPLING PORT  
85

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

MID QUARTER

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
1019	0	PUMP	ON					9/10	20
1029	0.01	21.79	1.789	7.14	7.16	-121.5	-		
1037	0.05	21.90	1.855	2.09	7.16	-109.4	0.81		
1044	0.10	21.82	1.918	2.27	7.16	-81.2	0.36		
1052	0.20	21.58	1.937	2.42	7.17	+9.9	0.00		
1059	0.30	21.44	1.939	2.45	7.17	31.9	0.00		
1108	0.45	21.22	1.939	2.39	7.18	45.5	0.00		
1115	0.55	21.10	1.939	2.35	7.18	50.5	0.00		
1120	0.60	21.06	1.939	2.33	7.18	52.0	0.00		
1125	0.70	21.04	1.939	2.31	7.19	52.9	0.00		
1130	0.75	20.98	1.939	2.31	7.19	52.2	0.00	↓	↓
1131		PUMP	OFF						
1132		START SAMPLE COLLECTION							
1210		SAMPLE COMPLETED : 2 L IPEC							
		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 31-63

SAMPLE ID: 026

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Showers, 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/23/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
55.8 to 63.8

TOTAL VOLUME PURGED: 0.85 gal

SAMPLING PORT  
63

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

MID QUARTER

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
1019	0	PUMP	ON					9/10	20
1029	0.01	21.53	1.432	3.91	6.94	-69.8	-		
1037	0.02	21.70	1.431	3.47	6.91	-62.7	1.01		
1044	0.05	21.83	1.421	2.50	6.88	-59.4	0.18		
1052	0.10	21.89	1.355	2.13	6.89	-51.8	0.00		
1059	0.15	21.86	1.296	2.13	6.90	-44.5	0.00		
1108	0.20	21.74	1.218	2.21	6.93	-29.8	0.00		
1115	0.25	21.65	1.186	2.30	6.96	-20.9	0.00		
1120	0.30	21.59	1.167	2.27	6.96	-13.5	0.00		
1125	0.33	21.53	1.150	2.26	6.96	-7.9	0.00		
1130	0.38	21.46	1.139	2.30	6.97	-3.7	0.00		
1135	0.42	21.43	1.126	2.28	6.98	+2.9	0.00		
1142	0.48	21.33	1.112	2.25	7.02	10.8	0.00		
1147	0.51	21.31	1.110	2.29	7.01	14.2	0.00		
1152	0.55	21.30	1.106	2.29	7.02	17.9	0.00		
1157	0.60	21.27	1.104	2.30	7.02	19.8	0.00		
1202	0.63	21.24	1.106	2.29	7.03	20.2	0.00		
1207	0.70	21.21	1.107	2.28	7.03	21.0	0.00	↓	↓
1208		PUMP	OFF						
1210		START SAMPLE COLLECTION							
1311		SAMPLE COMPLETED : 2 L IPEC							
		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 31-49

SAMPLE ID: 025

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Showers, 70's

PROJECT NO: 01.0017869.92  
 DATE: 8/23/10  
 SAMPLER(S): M. BRITTS

SAMPLING INTERVAL (depth in ft below top of casing)  
34.8 to 49.3

TOTAL VOLUME PURGED: 3.40 gal

SAMPLING PORT  
49

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

MID QUARTER

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1019	0	PUMP	ON					9/10	20
1029	0.2	21.25	2.356	2.41	6.88	208.8	—		
1037	0.4	21.09	2.382	1.56	6.87	212.2	2.01		
1044	0.6	20.79	2.391	1.21	6.86	202.0	1.24		
1052	0.8	20.63	2.272	1.90	6.91	190.4	0.43		
1059	1.1	20.50	2.190	2.24	6.92	186.1	0.93		
1108	1.4	20.34	2.139	2.41	6.93	181.8	0.00		
1115	1.7	20.25	2.107	2.63	6.95	179.2	0.00		
1120	1.9	20.21	2.068	2.87	6.96	177.2	0.00		
1125	2.05	20.19	2.004	3.96	6.99	174.9	0.00		
1130	2.25	20.17	1.550	6.08	7.13	168.4	0.00		
1135	2.50	20.11	1.221	7.24	7.25	168.1	0.00		
1142	2.70	20.04	1.073	7.81	7.32	166.5	0.00		
1147	2.90	20.02	1.047	8.17	7.33	166.1	0.00		
1152	3.10	20.00	1.031	8.20	7.34	165.7	0.00		
1157	3.25	20.01	1.023	8.23	7.34	165.2	0.00	↓	↓
1158		PUMP	OFF						
1159		START	SAMPLE COLLECTION						
1211		SAMPLE	COMPLETED : 2 L IPEC						
		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200704293

NOTES AND OBSERVATIONS:







WELL ID: MW 60-35

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Cloudy, Humid 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/16/10  
 SAMPLER(S): M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
24.9 to 39.4

TOTAL VOLUME PURGED: 1.70 gal

SAMPLING PORT  
35

PURGE RATE: variable (gal/min)

PURGE METHOD: Double Valve Pump

7

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1249	0	PUMP ON						5/7	19
1256	0.05	21.42	2.200	2.94	6.76	-40.2	—	5/7	18
1301	0.15	22.00	2.161	1.11	7.01	-66.2	2.19		
1310	0.30	22.48	2.179	0.75	7.24	-60.5	1.98		
1318	0.45	22.56	2.275	0.64	7.45	-48.2	0.54		
1329	0.60	22.45	2.489	1.19	7.51	-22.6	0.32		
1340	0.80	22.40	2.640	1.34	7.54	5.7	0.00		
1345	0.90	22.24	2.681	1.60	7.55	12.5	0.00		
1353	1.0	21.85	2.702	1.75	7.56	21.6	0.00		
1358	1.05	21.78	2.711	1.84	7.57	27.4	0.00		
1403	1.15	21.69	2.720	1.97	7.57	31.3	0.00		
1408	1.20	21.50	2.725	2.01	7.57	35.0	0.00		
1413	1.35	21.45	2.730	2.15	7.57	40.8	0.00		
1418	1.45	21.40	2.735	2.17	7.57	42.1	0.00		
1423	1.55	21.38	2.733	2.19	7.57	44.4	0.00	↓	↓
1424		PUMP OFF							
1443		START SAMPLE COLLECTION							
1443		SAMPLE COMPLETED : 2 L IPEC							
1443		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200704293

NOTES AND OBSERVATIONS:



WELL ID: MW 60-53

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Cloudy, humid 80's

PROJECT NO: 01.0017869.92  
DATE: 8/16/10  
SAMPLER(S): M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
45.4 to 59.4

TOTAL VOLUME PURGED: 2.20 gal

SAMPLING PORT  
53

PURGE RATE: variable (gal / min)  
PURGE METHOD: Double Valve Pump

#### WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1249	0	PUMP ON						5/7	19
1256	0.05	22.20	2.827	2.73	6.51	-76.5	—	5/7	18
<del>1254</del>	0.10	22.37	2.771	1.30	6.70	-83.6	2.98		
1310	0.30	22.08	2.744	0.70	7.05	-69.4	2.17		
1318	0.45	21.34	2.731	0.58	7.24	-42.6	1.08		
1329	0.60	21.49	2.728	0.56	7.39	-21.7	0.10		
1340	0.80	20.72	2.725	0.54	7.42	-8.4	0.00		
1345	1.00	20.39	2.730	0.56	7.44	-1.9	0.00		
1353	1.20	20.17	2.723	0.55	7.46	+6.5	0.00		
1358	1.30	19.90	2.726	0.57	7.47	9.0	0.00		
1403	1.50	19.78	2.727	0.59	7.48	16.8	0.00		
1408	1.65	19.75	2.729	0.65	7.49	19.9	0.00		
1413	1.80	19.64	2.727	0.63	7.49	22.9	0.00		
1418	1.95	19.69	2.726	0.64	7.49	23.9	0.00		
1423	2.05	19.70	2.727	0.63	7.49	25.6	0.00	↓	↓
1424		PUMP OFF							
1425		START SAMPLE COLLECTION							
1534		SAMPLE COMPLETED : 2 L IPEC ROUTINE							
1536		" : 2 L IPEC DUPLICATE							
1537		" : 2 L IPEC SPIKE							
		PUMP OFF.							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 60-72

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: sun + clouds 90's L

PROJECT NO: 01.0017569.92  
 DATE: 8/17/10  
 SAMPLER(S): M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
66.4 to 78.2

TOTAL VOLUME PURGED: 3.40 gal

SAMPLING PORT  
72

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

4

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1020	0	PUMP ON						5/6	31
1033	0.1	18.96	4.548	1.62	6.83	18.6	—	6/5	30
1040	0.3	18.25	4.556	0.75	7.10	10.9	2.28		
1050	0.8	17.61	4.247	0.52	7.23	14.9	1.94		
1100	1.3	17.46	4.120	0.47	7.30	18.8	1.53		
1110	1.6	17.41	4.097	0.47	7.32	21.2	1.81		
1116	2.3	17.27	4.075	0.47	7.34	23.5	1.57		
1122	2.6	17.01	4.070	0.45	7.34	24.6	1.72		
1127	2.85	16.99	4.057	0.45	7.35	20.0	1.36		
1132	3.00	17.01	4.023	0.44	7.35	28.7	1.41		
1140	3.25	17.06	4.030	0.43	7.36	29.9	1.32	↓	↓
1141		PUMP OFF							
1145		START SAMPLE COLLECTION							
1159		SAMPLE COMPLETED :				2 L IPEC			
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 60 - 135

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sum + clouds 90's

PROJECT NO: 01.0017869.92  
 DATE: 8/17/10  
 SAMPLER(S): M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
124.9 to 141.4

TOTAL VOLUME PURGED: 2.15 gal

SAMPLING PORT  
135

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

3

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1020	0	PUMP ON						5/6	31
1033	0.05	20.88	2.285	2.24	6.43	-134.0	—	6/5	30
1040	0.15	20.06	2.267	0.77	6.77	-158.8	2.41		
1050	0.35	18.76	2.270	0.42	7.21	-225.0	1.96		
1100	0.70	18.51	2.286	0.31	7.29	-236.2	1.64		
1110	0.90	18.48	2.292	0.28	7.30	-235.9	0.95		
1116	1.10	18.29	2.298	0.25	7.31	-239.6	1.25		
1122	1.35	18.12	2.300	0.23	7.31	-244.3	0.01		
1127	1.50	17.96	2.299	0.22	7.31	-246.7	0.01		
1132	1.70	17.91	2.302	0.21	7.31	-241.9	0.03		
1140	2.00	17.96	2.303	0.20	7.32	-239.6	0.02	↓	↓
1141		PUMP OFF							
1145		START SAMPLE COLLECTION							
1209		SAMPLE COMPLETED : 2 L				IPEC			
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 60-154

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 90's

PROJECT NO: 01.0017869.92  
 DATE: 8/17/10  
 SAMPLER(S): M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
147.4 to 164.9

TOTAL VOLUME PURGED: 2.15 gal

SAMPLING PORT  
154

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

2

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1020	0	PUMP ON						5/6	31
1033	0.05	21.69	2.060	2.50	6.39	16.2	—	6/5	30
1040	0.10	20.80	1.937	1.42	6.66	-61.1	3.01		
1050	0.30	19.28	1.825	0.68	7.14	-75.2	2.73		
1100	0.60	18.98	1.812	0.56	7.28	-81.6	2.53		
1110	0.75	19.11	1.809	0.50	7.32	-86.5	2.53		
1116	1.0	18.83	1.810	0.47	7.36	-89.6	1.91		
1122	1.15	18.55	1.811	0.46	7.38	-92.2	1.42		
1127	1.25	18.37	1.811	0.46	7.39	-93.3	1.29		
1132	1.50	18.30	1.811	0.44	7.40	-97.4	1.21		
1140	1.75	18.28	1.811	0.42	7.41	-99.2	1.27		
1146	2.0	18.26	1.816	0.41	7.42	-100.1	1.20	↓	↓
1147		PUMP OFF							
1150		START SAMPLE COLLECTION							
1218		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	3 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 60.176

SAMPLE ID: 014

**GZA GeoEnvironmental of New York  
Waterloo Sampling Data Sheet**

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sum + clouds 90's

PROJECT NO: 01.0017869.92  
 DATE: 8/17/10  
 SAMPLER(S): M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
170.9 to 200.4

TOTAL VOLUME PURGED: 1.10 gal

SAMPLING PORT  
176

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1020	0	PUMP ON						5/6	31
1033	0.1	23.60	0.742	0.50	6.36	-145.6	—	6/5	30
1040	0.15	24.59	0.743	0.22	6.50	-161.2	2.28		
1050	0.20	24.89	0.746	0.15	6.76	-196.2	1.84		
1100	0.30	24.96	0.747	0.12	7.02	-218.6	1.55		
1110	0.40	24.94	0.748	0.09	7.09	-224.1	1.31		
1116	0.45	24.75	0.751	0.09	7.17	-233.8	1.13		
1122	0.50	24.41	0.751	0.07	7.24	-244.0	1.04		
1127	0.60	24.23	0.751	0.06	7.26	-247.8	1.15		
1132	0.70	23.81	0.750	0.06	7.27	-251.6	1.19		
1140	0.80	23.70	0.750	0.05	7.28	-254.1	1.20		
1146	0.90	23.74	0.748	0.05	7.28	246.8	1.11		
1151	0.95	23.78	0.746	0.04	7.29	241.4	1.17	↓	↓
1152		PUMP OFF							
1155		START SAMPLE COLLECTION							
1251		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW-49-26  
 SAMPLE ID: 021

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 90'S

PROJECT NO: 01.0017869.92  
 DATE: 8/11/10  
 SAMPLER(S): 1.5 mb  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes (gal)
0934	13.73	PUMP ON							
0955	13.57	24.99	2.327	1.02	6.97	139.3	—		0.15
1005	13.49	25.03	2.319	0.74	6.99	108.4	0.00		0.35
1015	13.41	25.11	2.312	0.65	7.03	88.0	0.00		0.55
1020	13.38	25.20	2.308	0.61	7.05	79.8	0.00		0.60
1025	13.35	25.23	2.306	0.55	7.07	73.2	0.00		0.65
1030	13.29	25.18	2.296	0.47	7.10	66.3	0.00		0.70
1035	13.27	25.33	2.296	0.43	7.09	60.6	0.00		0.75
1040	13.24	25.52	2.292	0.46	7.14	56.4	0.00		0.80
1045	13.20	25.46	2.296	0.56	7.15	51.4	0.00		0.85
1050	13.10	25.25	2.286	0.36	7.15	48.2	0.00		1.00
1055	12.98	25.21	2.286	0.38	7.19	41.7	0.00		1.10
1100	12.94	25.17	2.287	0.33	7.14	39.6	0.00		1.20
1102	START SAMPLE COLLECTION								
1127	END SAMPLE COLLECTION: 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	1
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 1.55 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-49-42  
 SAMPLE ID: 021

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 90's

PROJECT NO: 01.0017869.92  
 DATE: 8/1/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

**WATER QUALITY:** DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes (gpi)
0934	13.976								
0955	14.095	25.23	2.386	1.15	7.27	215.5	—		0.15
1005	14.150	25.07	2.415	0.65	7.30	201.4	0.00		0.35
1015	14.227	25.04	2.419	0.43	7.33	198.5	0.00		0.55
1020	14.272	24.95	2.425	0.29	7.33	185.4	0.00		0.60
1025	14.249	24.92	2.425	0.38	7.33	181.3	0.00		0.70
1030	14.352	24.89	2.427	0.37	7.34	176.6	0.00		0.80
1033	START SAMPLE COLLECTION								
1100	END SAMPLE COLLECTION: 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	2
turbidity meter	200704293

**NOTES AND OBSERVATIONS:** Total volume purged 1.20 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.









WELL ID: MW-49-42

SAMPLE ID: 021

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 90°

PROJECT NO: 01.0017869.92  
 DATE: 8/1/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

**WATER QUALITY:** DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (w/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes (gal)
0934	13.976								(gal)
0955	14.095	25.23	2.386	1.15	7.27	215.5	—		0.15
1005	14.150	25.07	2.415	0.85	7.30	201.4	0.00		0.35
1015	14.227	25.04	2.419	0.43	7.33	198.5	0.00		0.55
1020	14.272	24.95	2.425	0.39	7.33	185.4	0.00		0.60
1025	14.299	24.92	2.425	0.38	7.33	181.3	0.00		0.70
1030	14.352	24.89	2.427	0.37	7.34	176.6	0.00		0.80
1033	START SAMPLE COLLECTION								
1100	END SAMPLE COLLECTION: 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
Flow ineter	2
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 120 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.





WELL ID: MW 63-34  
 SAMPLE ID: 014

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 90'S, HUMID

PROJECT NO: 01.0017869.92  
 DATE: 8/10/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

**WATER QUALITY:** DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (µl)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes (gal)
1015	13.322	PUMP ON	DN						
1032	13.494	24.07	1.441	4.7	7.43	-144.3	4.77		0.01
1042	13.587	23.90	1.392	1.36	7.46	-145.2	0.93		0.20
1050	13.662	24.11	1.383	0.89	7.46	-148.5	0.00		0.30
1056	13.712	24.28	1.384	0.81	7.46	-146.0	0.00		0.40
1100	13.763	24.07	1.389	0.76	7.48	-162.0	0.00		0.45
1105	13.803	23.91	1.388	0.65	7.48	-163.6	0.00		0.55
1110	13.845	23.89	1.387	0.61	7.48	-165.4	0.00		0.65
1115	13.887	23.86	1.384	0.59	7.48	-164.2	0.00		0.70
1117	START SAMPLE COLLECTION								
1144	END SAMPLE COLLECTION: 2 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
flow meter	1
turbidity meter	200704293

**NOTES AND OBSERVATIONS:** Total volume purged 0.45 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.





WELL ID: MW 63-121

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
SITE: Buchanan, NY  
WEATHER: Sun + clouds 90°F

PROJECT NO: 01.0017869.92  
DATE: 8/10/10  
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
118 to 127.5

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
121 3

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

#### WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1015	0							8.2/8.0	39
1020	0.2	22.02	1.415	0.25	7.24	-182.5	—		↓
1025	0.3	21.30	1.394	0.17	7.32	-177.1	7.06		
1030	0.5	20.69	1.390	0.14	7.35	-178.8	5.84		35
1037	0.6	20.18	1.384	0.12	7.37	-172.4	3.90		
1043	0.95	20.03	1.395	0.13	7.38	-169.1	2.14		
1049	1.20	19.80	1.380	0.15	7.39	-150.1	0.00		
1056	1.50	19.74	1.377	0.13	7.39	-147.6	0.00		
1101	1.70	19.59	1.373	0.14	7.40	-148.6	0.00		
1108	1.90	19.51	1.373	0.15	7.40	-145.4	0.00		
1113	2.10	19.55	1.372	0.15	7.40	-143.6	0.00		
1114		PUMP OFF							
1115		START SAMPLE COLLECTION							
1128		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200704293

NOTES AND OBSERVATIONS:



WELL ID: MW 63-159

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 90°F

PROJECT NO: 01.0017869 92  
 DATE: 8/10/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
106.5 to 152.0

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
152 4

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1300	0	PUMP ON						7.7	22
1312	0.05	24.56	1.280	0.17	7.26	-177.3	—	7.4	22
1317	0.15	25.61	1.264	0.18	7.33	-126.2	0.00	↓	20
1327	0.25	25.69	1.279	0.11	7.37	-134.8	0.00		
1333	0.35	25.13	1.290	0.10	7.37	-128.4	0.00		
1339	0.40	24.42	1.289	0.09	7.38	-117.5	0.00		
1350	0.70	23.94	1.288	0.08	7.39	-97.0	0.00		
1400	0.85	23.60	1.285	0.07	7.39	-103.7	0.00		
1406	0.90	23.47	1.282	0.06	7.39	-104.7	0.00		
1420	1.20	23.41	1.281	0.06	7.40	-103.9	0.00		
1421		PUMP OFF							
1423		START SAMPLE COLLECTION							
1452		SAMPLE COMPLETED: 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 63-93

SAMPLE ID: 015

**GZA GeoEnvironmental of New York  
Waterloo Sampling Data Sheet**

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/10/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
81.5 to 100.5

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
50 5

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1300	0	PUMP ON						7/7.4	22
1312	0.05	24.26	1.049	0.88	6.41	-70.5	—		22
1317	0.10	25.54	1.060	0.44	6.49	-86.1	0.00		20
1327	0.25	25.69	1.072	0.31	6.84	-74.2	0.00		
1333	0.35	24.90	1.071	0.24	6.95	-75.5	0.00		
1339	0.40	24.42	1.060	0.20	6.95	-69.4	0.00		
1350	0.75	23.93	0.994	0.17	6.96	-53.2	0.00		
1400	0.00	23.53	0.963	0.16	6.98	-49.8	0.00		
1406	1.05	23.11	0.954	0.16	7.00	-49.0	0.00		
1420	1.30	23.24	0.940	0.16	7.09	-42.7	0.00		
1429	1.50	23.80	0.935	0.17	7.19	-45.7	0.00		
1438	1.70	23.75	0.934	0.18	7.21	-47.1	0.00		
1444	1.80	23.70	0.933	0.18	7.23	-47.0	0.00		
1445		PUMP OFF							
1446		START SAMPLE COLLECTION							
1510		SAMPLE COMPLETED: 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u>5</u>
turbidity meter	<u>200704293</u>

NOTES AND OBSERVATIONS:

WELL ID: MW 63-50

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Sun + clouds 90°F

PROJECT NO: 01.0017869.92  
DATE: 8/10/10  
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)

40.5 to 58.0

TOTAL VOLUME PURGED:

\_\_\_\_\_ gal

SAMPLING PORT

50

7

PURGE RATE: variable (gal / min)

PURGE METHOD:

Double Valve Pump

#### WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1300	0							7/7.4	22
1303									
1310									
1312	0.01	25.10	1.361	6.26	7.24	-56.7	—	↓	↓
1317	0.15	23.23	1.292	3.65	7.48	-53.9	0.00	7/7.4	20
1327	0.30	23.02	1.292	2.62	7.57	-54.9	0.00		
1333	0.50	22.39	1.296	2.54	7.60	-55.1	0.00		
1339	0.75	21.63	1.292	2.43	7.60	-54.5	0.00		
1350	1.10	21.46	1.292	2.15	7.62	-57.5	0.00		
1400	1.50	20.95	1.294	2.11	7.62	-55.5	0.00		
1406	1.70	20.89	1.295	2.09	7.62	-54.3	0.00		
1414	1.90	20.97	1.298	2.07	7.64	-53.9	0.00		
1415			PUMP OFF						
1416			START SAMPLE COLLECTION						
1432			SAMPLE COMPLETED						
			PUMP OFF						

#### Equipment Used

YSI 556 MPS Reader and 5563 Sonde  
turbidity meter

#### Equipment Identification #

3  
200704293

#### NOTES AND OBSERVATIONS:

WELL ID: MW-66-21  
 SAMPLE ID: 014

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

**WATER QUALITY:** DTW = 12.14 Transducer Actual Depth 8.554

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
0941	8.975	Pump	ON						
0954	9.094	23.48	5.092	2.50	6.98	-194.1	—		0.01
1015	9.329	24.79	5.044	0.39	7.06	-231.3			0.20
1023	9.399	25.15	5.040	0.37	7.06	-229.3	126.8		0.25
1029	9.407	26.02	5.045	0.47	7.07	-230.4	31.87		0.30
1035	9.467	26.61	5.047	0.41	7.08	-225.8	28.09		0.35
1041	9.523	27.26	5.053	0.33	7.08	-227.7	26.11		0.40
1050	9.578	27.60	5.055	0.19	7.09	-241.2	22.12		0.45
1056	9.620	27.89	5.060	0.17	7.09	-236.1	14.91		0.48
1101	9.646	27.79	5.100	0.14	7.07	-264.6	9.57		0.50
1106	9.747	27.82	5.098	0.14	7.06	-268.9	9.59		0.60
1111	9.712	28.02	5.098	0.12	7.06	-262.2	10.83		0.65
1116	9.767	28.29	5.100	0.11	7.07	-260.1	11.20		0.68
1121	9.754	28.98	5.106	0.12	7.07	-241.4	8.15		0.69
1126	9.780	29.05	5.108	0.12	7.08	-236.7	8.05		0.70
1131	9.803	29.09	5.109	0.12	7.09	-240.2	8.12		0.72
1134	START SAMPLE COLLECTION								
1230	SAMPLE COMPLETED : 2 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
flow meter	3
turbidity meter	200704293

**NOTES AND OBSERVATIONS:** Total volume purged 0.90 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-66-36  
 SAMPLE ID: 013

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 11.50 Transducer Actual Depth 12.956

Time	DTW or <u>Actual Depth</u>	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
0941	13.134	PUMP	ON						
1015	13.323	28.02	2.481	3.08	7.23	-88.2	—		0.01
1023	13.353	26.17	2.446	1.89	7.38	-133.7	—		0.02
1029	13.373	25.78	2.424	1.21	7.37	-137.5	5.75		0.05
1035	13.381	25.15	2.429	1.01	7.40	-139.6	5.36		0.10
1041	13.405	24.60	2.416	0.71	7.41	-136.5	4.99		0.15
1050	13.489	24.55	2.402	0.52	7.40	-128.1	3.19		0.25
1056	13.499	24.67	2.404	0.49	7.40	-137.8	3.06		0.40
1101	13.519	24.60	2.409	0.46	7.41	-139.2	3.11		0.50
1106	13.538	24.63	2.405	0.45	7.42	-138.6	3.08		0.60
1111	START SAMPLE COLLECTION								
1147	END SAMPLE COLLECTION: 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
flow meter	1
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 0.90 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet incl.

WELL ID: MW 07-39

SAMPLE ID: 04

**GZA GeoEnvironmental of New York  
Waterloo Sampling Data Sheet**

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly Sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
28.8 to 54.3

TOTAL VOLUME PURGED: 2.70 gal

SAMPLING PORT  
39 7

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
931	0							8/8	20
			PUMP ON						
940	0.1	21.17	2.322	0.79	6.68	-121.9	—		
945	0.2	20.76	2.317	0.36	7.08	-153.3	—		
950	0.35	20.60	2.317	0.33	7.28	-161.8	—		
955	0.60	20.45	2.333	0.32	7.48	-162.3	—		
1001	0.90	20.44	2.366	0.32	7.63	-160.3	—		
1006	1.20	20.44	2.369	0.29	7.68	-159.2	—		
1011	1.35	20.46	2.375	0.29	7.71	-158.6	—		
1016	1.50	20.51	2.378	0.27	7.74	-157.2	—		
1021	1.65	20.42	2.389	0.26	7.76	-161.4	—		
1026	1.90	20.43	2.396	0.25	7.76	-160.3	—		
1031	2.15	20.44	2.400	0.25	7.76	-159.2	—		
1033	START SAMPLE COLLECTION								
1043	END SAMPLE COLLECTION: 7L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	—

NOTES AND OBSERVATIONS:

WELL ID: MW 67-105

SAMPLE ID: 013

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
DATE: 8/9/10  
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
90.3 to 110.8

TOTAL VOLUME PURGED: 1.40 gal

SAMPLING PORT  
105 6

PURGE RATE: variable (gal / min)  
PURGE METHOD: Double Valve Pump

#### WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
931	0		PUMP ON					8/8	20
940	0.10	21.54	1.560	1.48	6.21	-96.5	—		
945	0.20	21.51	1.544	0.75	6.32	-132.4	—		
950	0.30	21.35	1.539	0.60	6.38	-154.2	—		
955	0.45	21.25	1.534	0.51	6.43	-167.1	—		
1001	0.65	21.15	1.535	0.40	6.51	-183.6	—		
1006	0.80	21.21	1.533	0.37	6.54	-190.9	—		
1011	0.90	21.21	1.532	0.35	6.56	-196.4	—		
1016	1.05	21.19	1.534	0.32	6.57	-205.6	—		
1018	START SAMPLE COLLECTION								
1037	END SAMPLE COLLECTION: 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>3</u>

NOTES AND OBSERVATIONS:



WELL ID: MW 67-173

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
164.8 to 188.3

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
173 5

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
931	0	PUMP ON						8/8	20
940	0.1	21.19	1.116	0.85	6.70	-96.7	—		
945	0.2	21.44	1.154	0.67	6.71	-111.7	—		
950	0.35	21.40	1.188	0.50	6.83	-140.2	—		
955	0.50	21.36	1.221	0.32	6.95	-191.7	—		
1001	0.60	21.28	1.226	0.23	7.00	-223.7	—		
1006	0.70	21.37	1.226	0.19	7.03	-254.2	—		
1011	0.80	21.26	1.223	0.19	7.08	-276.8	—		
1016	0.90	21.30	1.216	0.16	7.09	-269.9	—		
1021	1.00	21.32	1.207	0.14	7.13	-276.8	—		
1026	1.10	21.26	1.204	0.13	7.15	-268.1	—		
1031	1.20	21.33	1.190	0.12	7.16	-266.5	—		
1036	1.30	21.36	1.185	0.11	7.19	-287.4	—		
1041	1.40	21.29	1.182	0.12	7.21	-280.8	—		
1042	START SAMPLE COLLECTION								
1107	END SAMPLE COLLECTION: 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	2

NOTES AND OBSERVATIONS: Turbidity meter not reading accurately.



WELL ID: MW 67-219

SAMPLE ID: 013

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
209 to 229.8

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
219 4

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1155	0	PUMP ON						6/6	45
1200	0.10	21.61	1.451	3.85	6.67	-141.3	-		
1210	0.30	21.09	1.147	0.46	6.39	-62.6	3.65		
1217	0.50	21.49	1.146	0.31	6.47	-82.3	0.80		
1225	1.15	21.71	1.159	0.28	6.88	-100.8	0.00		
1235	1.50	20.57	1.148	0.21	6.68	-49.1	0.00		
1240	1.75	20.76	1.150	0.23	6.76	-44.3	0.00		
1245	1.90	20.57	1.147	0.19	6.83	-45.6	0.00		
1250	2.05	20.91	1.144	0.18	6.85	-57.1	0.00		
1255	2.25	21.33	1.148	0.18	6.98	-71.2	0.00		
1300	2.40	20.99	1.149	0.15	7.02	-62.8	0.00		
1305	2.60	21.12	1.145	0.14	6.98	-73.3	0.00		
1310	2.80	21.15	1.149	0.15	7.00	-71.8	0.00		
1315	3.0	21.14	1.147	0.14	7.02	-72.7	0.00		
1316		PUMP OFF							
1317		START SAMPLE COLLECTION							
1333		SAMPLE COMPLETED : 2 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u>5</u>
turbidity meter	<u>200704293</u>

NOTES AND OBSERVATIONS:

WELL ID: MW 67-276

SAMPLE ID: 013

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
250.8 to 281.3

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
270 3

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1155	0	PUMP	ON					6/6	45
1200	0.10	22.07	0.951	0.77	6.95	-130.8	—		
1210	0.30	21.99	0.945	0.37	7.11	-137.5	2.14		
1217	0.40	22.43	0.945	0.31	7.16	-131.1	0.49		
1225	0.75	22.52	0.951	0.30	7.20	-125.2	0.00		
1235	1.00	21.31	0.940	0.20	7.17	-128.0	0.00		
1240	1.25	21.54	0.942	0.22	7.20	-129.0	0.00		
1245	1.50	21.36	0.937	0.19	7.21	-130.0	0.00		
1250	1.65	21.73	0.935	0.20	7.22	-132.5	0.00		
1255	1.75	22.05	0.939	0.20	7.24	-137.1	0.00		
1300	1.90	21.75	0.941	0.16	7.22	-133.4	0.00		
1305	2.00	21.84	0.938	0.19	7.24	-140.0	0.00		
1310	2.10	21.79	0.941	0.18	7.25	-138.6	0.00		
1315	2.30	21.83	0.938	0.17	7.24	-137.0	0.00		
1316		PUMP	OFF						
1317		START	SAMPLE COLLECTION						
1336		SAMPLE	COMPLETED: 2 L IPEC						
		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	6 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 67-323

SAMPLE ID: 013

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly Sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)

317.8 to 328.3

TOTAL VOLUME PURGED:

1.40 gal

SAMPLING PORT

323 2

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1155	0	PUMP ON						6/6	45
1200	0.10	23.47	0.921	0.59	7.07	-157.7	—		
1210	0.30	23.32	0.895	0.31	7.18	-195.3	7.15		
1217	0.40	23.89	0.898	0.28	7.13	-268.8	2.61		
1225	0.50	24.47	0.930	0.27	7.07	-316.3	0.00		
1235	0.75	22.67	0.921	0.14	7.02	-320.7	0.00		
1240	0.90	22.84	0.918	0.13	7.03	-308.5	0.00		
1245	1.00	22.60	0.914	0.12	7.03	-297.5	0.00		
1250	1.15	22.68	0.910	0.11	7.03	-283.4	0.00		
1255	1.25	22.72	0.911	0.11	7.04	-282.0	0.00	↓	↓
1259	START SAMPLE COLLECTION								
1323	SAMPLE COMPLETED				: 2	L IPEC			
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	3 200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 67-340

SAMPLE ID: 013

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 8/9/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
335.3 to 347.9

TOTAL VOLUME PURGED: 1.65 gal

SAMPLING PORT  
340

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1155	0	PUMP ON						6/6	45
1200	0.10	23.00	0.774	0.22	7.22	-199.0	—		
1210	0.30	23.09	0.768	0.11	7.34	-265.6	6.41		
1217	0.40	23.65	0.762	0.10	7.32	-298.8	1.47		
1225	0.50	23.52	0.770	0.10	7.30	-307.7	0.00		
1235	1.00	22.46	0.760	0.07	7.24	-305.6	0.00		
1240	1.25	22.71	0.762	0.07	7.24	-303.9	0.00		
1245	1.25	22.47	0.762	0.06	7.23	-305.8	0.00		
1250	1.35	22.51	0.763	0.06	7.23	-301.4	0.00		
1255	1.50	22.48	0.764	0.06	7.24	-307.6	0.00	↓	↓
1258	START SAMPLE COLLECTION								
1320	SAMPLE COMPLETED			: 2	L IPEC				
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW-55-24  
 SAMPLE ID: 015

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/6/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 9.95 Transducer Actual Depth = 5.875 <sup>Transd. reading</sup> = 7.805

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1035	5.862	PUMP ON							
1102	5.679	21.15	0.585	2.11	7.90	24.0	—		0.10
1116	5.675	29.63	0.564	1.59	7.99	-131.0	2.30		0.15
1126	5.682	29.64	0.556	1.09	8.00	-125.8	1.82		0.25
1136	5.711	29.75	0.556	0.98	8.00	-85.0	1.03		0.35
1145	5.671	29.69	0.558	0.93	8.01	-103.7	0.40		0.45
1150	5.674	29.37	0.564	0.91	8.01	-135.7	0.00		0.50
1156	5.657	29.41	0.566	0.93	8.02	-129.1	0.00		0.55
1200	5.666	29.47	0.566	0.88	8.02	-118.2	0.00		0.60
1205	START SAMPLE COLLECTION								
1311	END SAMPLE COLLECTION - 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	7
flow meter	3
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 1000 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-55-35  
 SAMPLE ID: 014

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly Sunny 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/6/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 10.30 Transducer Actual Depth = 21.699 Transd. reading = 7.501

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1035	21.685								
			pump on						
1102	21.1018	32.24	0.170	7.63	7.31	87.3	—		0.01
1116	21.143	32.57	0.654	7.79	7.23	29.8	—		0.05
1126	21.571	30.90	0.644	2.49	7.35	38.1	21.43		0.08
1136	21.1061	28.10	0.574	1.55	6.88	-89.9	0.00		0.10
1145	21.580	28.48	0.564	0.94	6.74	-59.2	0.00		0.15
1150	21.566	28.49	0.563	0.89	6.84	-64.4	0.00		0.18
1155	21.543	28.70	0.563	0.82	6.96	-55.2	0.00		0.20
1200	21.585	28.82	0.563	0.72	7.11	-52.5	0.00		0.25
1205	21.574	28.88	0.564	0.67	7.28	-58.3	0.00		0.30
1210	21.555	28.87	0.566	0.67	7.36	-65.1	0.00		0.35
1215	21.555	28.86	0.568	0.67	7.38	-69.7	0.00		0.40
1220	START SAMPLE COLLECTION								
1315	END SAMPLE COLLECTION - 2 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	1
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 0.70 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msf.

# GZA GeoEnvironmental of New York

## Low-Flow Sampling Data Sheet

WELL ID: MW-55-54  
 SAMPLE ID: 015

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/6/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 10.05 Transducer Actual Depth 39.304 Transd. reading = 7841

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1035	10.08	PUMP ON							
1102	10.09	27.17	2.135	3.31	7.48	170.8	—		0.15
1116	10.09	26.53	2.069	3.08	7.50	163.0	0.00		0.25
1126	10.09	26.37	2.096	2.98	7.51	156.2	0.00		0.50
1136	10.08	26.47	2.098	2.89	7.52	150.8	0.00		0.60
1145	10.07	26.30	2.094	2.95	7.52	145.3	0.00		0.65
1150	10.06	26.44	2.095	2.80	7.53	142.4	0.00		0.70
1155	10.05	26.51	2.096	2.82	7.54	139.3	0.00		0.75
1200	10.05	26.58	2.097	2.79	7.54	137.0	0.00		0.80
1203	START SAMPLE COLLECTION								
1250	END SAMPLE COLLECTION: 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
flow meter	2
turbidity meter	200704293

**NOTES AND OBSERVATIONS:** Total volume purged 1.25 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.







WELL ID: MW-37-32  
 SAMPLE ID: 019

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, HUMID, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/5/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1109	15.048	PUMP ON							
1150	15.041	31.37	4.158	2.16	7.29	197.2	—		0.01
1200	15.024	31.51	4.176	1.65	7.34	186.8	0.00		0.1
1213	15.001	31.68	4.226	1.15	7.37	173.9	0.00		0.15
1220	14.999	31.67	4.245	1.05	7.37	167.8	0.00		0.20
1225	15.016	31.73	4.243	1.03	7.38	163.8	0.00		0.25
1230	15.002	31.75	4.270	0.94	7.38	161.1	0.00		0.30
1235	15.014	31.78	4.280	0.96	7.38	156.7	0.00		0.35
1240	15.008	31.80	4.278	0.93	7.39	154.0	0.00		0.40
1242	START SAMPLE COLLECTION								
1400	END SAMPLE COLLECTION: 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	3
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 0.60 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-37-57  
 SAMPLE ID: 019

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, HUMID, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/5/10  
 SAMPLER(S): CB, MR  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1109	42.471	PUMP ON							
1150	42.355	31.34	2.295	3.57	7.50	173.4	—		0.01
1200	42.338	31.41	2.305	2.58	7.53	157.1	0.00		0.10
1213	42.235	31.52	2.309	2.58	7.53	160.8	0.00		0.15
1220	42.338	31.60	2.310	2.46	7.53	157.7	0.00		0.20
1225	42.364	31.63	2.311	2.21	7.53	155.1	0.00		0.25
1230	42.328	31.67	2.311	2.14	7.53	152.9	0.00		0.30
1235	42.332	31.70	2.310	2.07	7.53	150.6	0.00		0.35
1237	STARTS SAMPLE COLLECTION								
1359	END SAMPLE COLLECTION 2 L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	2
turbidity meter	210704293

NOTES AND OBSERVATIONS: Total volume purged 0.60 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-37-40  
SAMPLE ID: 019

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: SUNNY, HUMID, 80's

PROJECT NO: 01.0017869.92  
DATE: 8/5/16  
SAMPLER(S): LB

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{40}{\text{DTB}} - \frac{8.50}{\text{DTW}} = \frac{31.5}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 31.5 x 0.041 Multiplier = 1.29 gal Well Volume

1.29 x 1.5 = 1.94 gal Designed Purge Volume

TOTAL VOLUME PURGED: 2.20 gal

**WATER QUALITY:** DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1327	0	<del>29.254</del>	PUMP ON	DN					
1337	0.25	29.479	28.42	2.345	0.62	7.22	-243.1	—	
1347	0.50	29.556	27.75	2.283	0.38	7.25	-220.3	151.0	
1348	0.75	29.421	27.38	2.237	0.61	7.24	-228.5	82.4	
1355	1.25	29.404	27.20	2.222	0.30	7.25	-210.0	839.0	
1358	1.50	29.390	27.21	2.709	0.32	7.26	-199.2	678.3	
1402	1.75	29.775	27.33	2.197	0.37	7.26	-176.2	639.2	
1410	2.00	30.125	27.63	2.190	0.38	7.29	-229	351.1	
1411	START SAMPLE COLLECTION								
1425	END SAMPLE COLLECTION; 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200704293

**NOTES AND OBSERVATIONS:**  
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.



WELL ID: MW-50-66  
 SAMPLE ID: 027

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly cloudy 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/4/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 11.24 Transducer Actual Depth = 87.917 <sup>transd. reading = 3.361</sup>

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Purged Notes H <sub>2</sub> O (gal)
1109	87.904		PUMP	ON					
1118	87.435	27.81	1.152	8.89	7.20	213.9	—	0.00	0.01
1124	87.354	27.77	2.262	4.21	7.20	222.4	—		0.02
1130	87.735	27.73	2.263	2.15	7.21	207.9	—		0.03
1140	87.459	27.67	2.272	1.92	7.23	189.0	—		
1150	87.588	27.66	2.299	1.80	7.25	190.0	—		0.04
1200	87.555	27.71	2.342	1.68	7.25	177.9	—		0.05
1205	87.471	27.78	2.343	1.67	7.25	180.4	—		0.06
1210	87.794	27.80	2.345	1.72	7.25	179.9	—	↓	0.06
1212		START SAMPLE COLLECTION							
1638		SAMPLE COMPLETED: 2 L IPEC							
1638		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
flow meter	3
turbidity meter	—

rugged reader # 2

NOTES AND OBSERVATIONS: Total volume purged 0.20 gal

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

Turbidity meter not reading accurately. Not used.



WELL ID: MW 54-58

SAMPLE ID: 014

## GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, Humid, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/4/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
51.5 to 64.0

TOTAL VOLUME PURGED: 3.00 gal

SAMPLING PORT  
58 5

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1333	0	PUMP ON						0/4	20
1340	0.25	23.07	1.811	2.09	6.68	-63.6			
1350	1.00	22.53	1.769	0.29	7.12	-98.2	4.62		
1400	1.50	22.27	1.800	0.33	7.22	-107.4	4.94		
1405	2.00	22.19	1.819	0.30	7.25	-108.9	2.44		
1410	2.25	22.14	1.838	0.30	7.27	-108.9	2.57		
1415	2.50	22.09	1.840	0.29	7.29	-109.4	2.47		
1420	2.75	22.08	1.846	0.30	7.30	-109.7	2.49		
1424	START SAMPLE COLLECTION								
1435	END SAMPLE COLLECTION - 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	3 200701254

NOTES AND OBSERVATIONS:







WELL ID: MW 54-173

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, Humid, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/4/10  
 SAMPLER(S): CD, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
170.5 to 182.0

TOTAL VOLUME PURGED: 2.15 gal

SAMPLING PORT  
173 2

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1043	0	PUMP ON						814	35
1049	0.05	23.59	1.950	2.83	6.03	6.3	—		
1100	0.50	22.66	1.996	0.44	6.70	-29.4	8.40		
1110	1.00	22.32	1.999	0.30	7.07	-25.7	5.33		
1116	1.25	22.15	1.999	0.23	7.19	-25.6	5.54		
1122	1.50	21.96	1.999	0.25	7.24	-27.7	3.68		
1128	1.75	21.81	1.999	0.24	7.27	-32.0	3.01		
1135	2.00	21.71	1.998	0.23	7.30	-40.3	5.13		
1140	2.25	21.67	1.999	0.20	7.32	-47.6	5.17		
1145	2.50	21.63	1.998	0.22	7.32	-52.9	5.19		
1148	START SAMPLE COLLECTION								
1209	END SAMPLE COLLECTION: 2L IPEC PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	3 200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 54-190

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, Humid, 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/4/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
185.0 to 203.6

TOTAL VOLUME PURGED: 3.0 gal

SAMPLING PORT  
190 |

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1042	0	PUMP ON						814	35
1049	0.05	24.35	2.090	1.33	6.00	-47.2	—		
1100	0.45	23.48	2.074	0.29	6.40	-105.2	6.73		
1110	0.80	23.00	2.087	0.19	6.83	-81.0	7.90		
1116	1.05	22.74	2.091	0.16	6.97	-104.7	5.74		
1122	1.25	22.58	2.091	0.15	7.04	-44.9	5.98		
1128	1.50	22.38	2.092	0.15	7.09	-30.5	3.42		
1135	1.60	22.27	2.093	0.16	7.11	-17.0	5.36		
1140	1.75	22.22	2.093	0.16	7.13	-14.2	2.51		
1145	2.00	22.12	2.094	0.14	7.15	-11.7			
1150	PUMP OFF: REPLACED BATTERIES				IN YSI				
1158	PUMP ON								
1201	2.25	22.61	2.103	0.33	7.17	-8.4	4.23		
1206	2.40	22.45	2.102	0.20	7.17	-8.0	2.76		
1211	2.50	22.45	2.102	0.17	7.16	-3.8	2.51		
1216	2.60	22.45	2.099	0.18	7.16	-1.3	2.64		
1218	START SAMPLE COLLECTION								
1234	END SAMPLE COLLECTION: 2L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200701254

NOTES AND OBSERVATIONS:







WELL ID: MW 62-71

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/3/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
61.1 to 82.6

TOTAL VOLUME PURGED: 1.20 gal

SAMPLING PORT  
71 5

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1020	0	PUMP ON						5/6	25
1030	0.01	24.16	1.387	1.47	—	-219.1	—	↓	↓
1035	0.25	23.26	1.400	1.07	—	-211.1	9.72		
1042	0.40	22.10	1.382	0.71	—	-200.6	9.21		
1052	0.60	21.52	1.382	0.50	—	-170.2	8.95		
1059	0.75	21.38	1.381	0.44	—	-161.2	7.78		
1104	0.90	21.37	1.381	0.43	—	-154.7	7.71		
1109	1.05	21.31	1.380	0.41	—	-151.6	7.76		
1110		PUMP OFF							
1111		START SAMPLE COLLECTION							
1130		SAMPLE COMPLETED : 2 L IPEC							
1130		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	4 200704293

NOTES AND OBSERVATIONS: pH sensor stopped working properly.

WELL ID: MW 62-92

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/3/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
88.6 to 99.1

TOTAL VOLUME PURGED: 1.25 gal

SAMPLING PORT  
92 4

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1020	0	PUMP ON						5/6	25
1030	0.01	24.86	1.359	0.45	6.72	-116.9	—	↓	↓
1035	0.25	24.26	1.364	0.40	6.95	-132.9	9.45		
1042	0.40	23.21	1.347	0.25	6.88	-126.6	9.41		
1052	0.60	22.36	1.350	0.19	6.87	-120.5	9.38		
1059	0.80	22.30	1.349	0.16	6.87	-116.1	9.01		
1004	0.95	22.28	1.352	0.17	6.90	-111.8	9.10		
1109	1.10	22.21	1.350	0.16	6.94	-109.9	9.06		
1110		PUMP OFF							
1112		START SAMPLE COLLECTION							
1132		SAMPLE COMPLETED : 2L IPEC							
1132		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:



WELL ID: MW 62-138

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
DATE: 8/3/10  
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
126.1 to 143.6

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
138 3

PURGE RATE: variable (gal / min)  
PURGE METHOD: Double Valve Pump

#### WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1225	0							6/4	30
		PUMP ON							
1231	0.02	22.00	1.586	1.80	6.97	-108.4	—		
1236	0.20	21.58	1.626	0.40	7.18	-125.8	8.19		
1243	0.45	21.49	1.640	0.24	7.37	-125.5	8.58		
1254	0.70	21.26	1.646	0.22	7.43	-121.6	8.69		
1304	1.00	21.22	1.645	0.19	7.45	-120.6	7.87		
1314	1.25	21.25	1.645	0.21	7.46	-118.4	7.53		
1320	1.50	20.96	1.641	0.20	7.46	-117.9	6.38		
1326	1.75	20.87	1.636	0.20	7.46	-117.4	5.59		
1332	1.90	20.83	1.627	0.19	7.46	-115.8	5.27		
1337	2.00	20.90	1.620	0.20	7.47	-116.1	3.40		
1343	2.25	20.88	1.614	0.21	7.47	-115.9	3.15		
1348	2.50	20.82	1.612	0.20	7.48	-115.3	3.26		
1350	START SAMPLE COLLECTION								
1409	END SAMPLE COLLECTION								
1409	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 62-182

SAMPLE ID: 014

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
DATE: 8/3/10  
SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
177.6 to 198.7

TOTAL VOLUME PURGED: \_\_\_\_\_ gal

SAMPLING PORT  
182

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1225	0	PUMP ON						6/4	30
1231	0.01	22.82	1.269	2.20	6.95	-104.8	—		
1236	0.10	22.74	1.266	0.68	6.66	-113.7	8.86		
1243	0.25	22.56	1.265	0.24	6.69	-97.0	9.07		
1254	0.50	22.30	1.265	0.17	6.97	-85.1	10.71		
1304	0.75	22.26	1.265	0.14	6.96	-64.6	9.70		
1314	1.00	22.44	1.263	0.12	7.03	-63.9	8.65		
1320	1.25	22.03	1.265	0.11	7.06	-73.8	9.37		
1326	1.50	21.91	1.264	0.10	7.07	-72.4	6.52		
1332	1.55	21.73	1.264	0.10	7.07	-73.5	6.22		
1337	1.65	21.81	1.262	0.10	7.07	-75.7	5.97		
1342	START SAMPLE COLLECTION								
1402	END SAMPLE COLLECTION: 7 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200704293

NOTES AND OBSERVATIONS:

WELL ID: I-2  
 SAMPLE ID: \_\_\_\_\_

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
 DATE: 8/2/10  
 SAMPLER(S): MB  
 PUMP DEPTH: 38.28 ft

WATER QUALITY: DTW = Transducer Actual Depth

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1116	8.495	PUMP ON							42.390
1125	8.207	22.33	1.253	7.49	7.12	134.9	—	0.25	42.104
1130	8.147	22.77	1.221	7.07	6.62	117.9	9.07		4 0.05
1135	8.122	23.17	1.217	6.85	6.55	102.6	7.78		42.018
1140	8.096	23.92	1.215	7.19	6.67	82.5	4.57		41.983 0.10
1147	8.086	25.00	1.216	7.86	6.83	63.2	5.78		41.972
1152	8.084	25.72	1.217	7.78	6.87	55.1	4.37		41.966 0.20
1200	8.129	26.38	1.220	6.89	6.90	51.9	3.66		42.017 0.23
1208	8.173	26.67	1.222	6.30	6.90	47.5	3.01		42.052 0.24
1215	8.219	26.91	1.223	6.11	6.90	42.4	2.78		42.092
1220	8.250	27.23	1.224	6.20	6.91	38.2	2.84		42.132 0.25
1225	8.258	27.37	1.224	6.22	6.90	37.6	2.79		42.132
1232	8.246	27.98	1.225	6.00	6.92	43.7	2.71		42.132 0.28
1237	8.252	28.02	1.225	5.97	6.93	43.4	2.67		42.132
1242	8.254	28.06	1.225	5.93	6.93	42.6	2.64		42.132 0.30
1244		START SAMPLE COLLECTION							
1439		SAMPLE COMPLETED			2	L IPEC			
1439		PUMP OFF							

*Purged H<sub>2</sub>O gal*

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
flow meter	1
turbidity meter	200704293

NOTES AND OBSERVATIONS: Total volume purged 0.40 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet in sl.

*Use peristaltic pump for low flow sampling*

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

WELL ID: MW-42-49  
SAMPLE ID: 022

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: SUNNY, 80's

PROJECT NO: 01.0017869.92  
DATE: 7/30/10  
SAMPLER(S): CB, MB  
PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 35.03 Transducer Actual Depth 34.304

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes gal
1033	13.418	PUMP	DNI					5/10	27	0
1036	12.743	17.55	1.387	7.85	7.40	127.0	—		↓	0.10
1046	12.134	16.80	0.865	8.40	8.02	126.8	0.00		25	1.00
1053	12.332	17.51	0.916	8.23	8.06	125.4	0.87		20	1.25
1100	12.444	17.55	0.926	8.20	8.05	122.7	2.14		25	1.75
1105	12.343	16.96	0.921	7.85	8.09	122.5	1.67			2.00
1110	12.257	16.89	0.933	7.75	8.10	121.3	0.00			2.25
1115	12.181	16.91	0.941	7.92	8.10	119.6	0.00			2.50
1120	12.139	16.88	0.946	8.00	8.09	117.9	0.00			2.85
1125	12.141	16.82	0.950	8.02	8.08	116.4	0.00			3.25
1130	12.099	16.86	0.953	8.03	8.07	114.9	0.00	↓	↓	
1131	START	SAMP	LE COLLECTION							
1138	END	SAMPLE	COLLECTION: 2L IPEC							
	PUMP	OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200704293

**NOTES AND OBSERVATIONS:** Total volume purged 3.45 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-42-78  
SAMPLE ID: 017

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: SUNNY, 80s

PROJECT NO: 01.0017869.92  
DATE: 7/30/10  
SAMPLER(S): CB,MS

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{78}{\text{DTB}} - \frac{34.10}{\text{DTW}} = \frac{43.90}{\text{Water Column Height}}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 43.90 x 0.041 Multiplier = 1.80 gal Well Volume

1.80 x 1.5 = 2.70 gal Designed Purge Volume

**TOTAL VOLUME PURGED: 3.00 gal**

WATER QUALITY: DTW = 34.10 Transducer Actual Depth 35.361

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
1201	0	—	Pump ON	ON					N/A	N/A	
1204	0.15	—	21.76	1.983	10.80	7.28	162.8	21.54			
1207	0.50	—	17.60	2.026	5.49	7.11	151.5	137.7			
1209	1.00	—	17.34	2.042	4.92	7.09	145.2	188.4			
1212	1.75	—	17.34	2.049	4.61	7.09	138.0	212.2			
1215	2.15	—	17.24	2.051	4.52	7.10	134.4	194.10			
1217	2.50	—	17.18	2.052	4.29	7.11	131.3	192.5			
1219	2.70	—	17.08	2.052	4.30	7.12	129.3	171.5			
1220	START	SAMPLE COLLECTION									
1223	END	SAMPLE COLLECTION: 2L IPEC									
	Pump OFF										

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	<u>2</u>
turbidity meter	<u>200704293</u>

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.

# GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

WELL ID: MW-53-82  
SAMPLE ID: 016

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Sunny 80's

PROJECT NO: 01.0017869.92  
DATE: 7/30/10  
SAMPLER(S): CB, MB  
PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 59.90 Transducer Actual Depth 21.643 Trans. reading = 10.007

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Purged Notes H <sub>2</sub> O (gal)
10:33	21.643		PUMP	ON				5/9	40	
1041	21.440	21.16	2.583	5.47	7.01	140.4	7.51	5/11	40	0.01
1046	21.468	21.83	2.478	5.03	6.78	117.9	7.21	5/13	40	
1053	21.470	22.37	2.341	5.35	6.89	83.4	7.54	5/16	40	0.1
1058	21.471	22.17	2.326	5.83	7.00	67.8	7.81	5/16	40	0.15
1103	21.428	21.54	2.242	6.50	7.08	53.1	8.86			0.25
1110	21.423	21.15	2.199	6.45	7.13	44.7	8.84			0.35
1115	21.463	21.59	2.170	6.51	7.14	41.0	9.08			0.45
1120	21.478	21.99	2.167	6.55	7.27	36.1	9.79			0.50
1126	21.490	22.14	2.164	6.55	7.29	30.5	9.97			0.60
1133	21.487	22.17	2.166	6.58	7.31	28.4	10.02			0.70
1138	21.492	22.16	2.165	6.60	7.33	28.0	10.05			0.75
1143	21.484	22.13	2.171	6.62	7.35	27.6	10.09	↓	↓	0.85
1145	Start sample collection.									
1232	Sample completed: 2 L IPEC									
1232	PUMP off									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200701254

NOTES AND OBSERVATIONS: Total volume purged 1.0 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-53-120  
SAMPLE ID: 020

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Sunny 80's

PROJECT NO: 01.0017869.92  
DATE: 7/30/10  
SAMPLER(S): CG

WATER COLUMN HEIGHT (ft)  $\frac{120}{DTB} - \frac{60.57}{DTW} = \frac{59.43}{\text{Water Column Height}}$  Well Diameter: 1 in

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

GALLONS OF WATER PER WELL VOLUME:

Water Column Height 59.43 x  $\frac{0.041}{\text{Multiplier}}$  = 2.44 gal Well Volume

2.44 x 1.5 = 3.66 gal  
Designed Purge Volume

TOTAL VOLUME PURGED: 3.85 gal

WATER QUALITY: DTW = Transducer Actual Depth

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
1346	0	60.57	PUMP ON								
1349	0.1	—	22.44	1.567	5.84	7.36	44.1	18.79	—	—	
1351	0.3	—	20.54	1.571	3.47	7.02	57.5	49.44	—	—	
1355	0.7	—	19.63	1.608	1.88	6.93	63.6	92.76	—	—	
1358	1.0	—	19.60	1.638	1.48	6.85	64.1	120.1	—	—	
1402	1.3	—	20.10	1.661	1.29	7.03	50.5	138.6	—	—	
1406	1.6	—	19.77	1.678	1.53	7.05	48.2	171.5	—	—	
1410	1.9	—	19.49	1.693	1.77	6.99	49.0	172.5	—	—	
1415	2.5	—	19.54	1.704	1.17	6.96	48.1	178.4	—	—	
1420	2.8	—	19.64	1.712	1.45	6.99	46.1	161.8	—	—	
1425	3.3	—	19.50	1.720	1.56	7.05	44.6	153.0	—	—	
1430	3.7	—	19.46	1.725	1.80	7.01	45.0	140.9	—	—	
1430			START SAMPLE COLLECTION								
1436			SAMPLE COMPLETED : 2 L IPEC								
1436			PUMP OFF								

### Equipment Used

### Equipment Identification #

YSI 556 MPS Reader and 5563 Sonde  
turbidity meter

5  
200701254

### NOTES AND OBSERVATIONS:

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.



# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-36-52  
SAMPLE ID: 018

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Humid, P. Cloudy, 80's

PROJECT NO: 01.0017869.92  
DATE: 7/29/10  
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{52}{\text{DTB}} - \frac{4.94}{\text{DTW}} = \frac{47.06}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

$$\text{Water Column Height } \frac{47.06}{\text{Multipler}} \times \frac{0.041}{\text{Well Volume}} = \frac{1.93}{\text{gal}}$$

$$\frac{1.93}{\text{gal}} \times 1.5 = \frac{2.90}{\text{Designed Purge Volume}} \text{ gal}$$

**TOTAL VOLUME PURGED: 3.25 gal**

WATER QUALITY: DTW = 4.94 Transducer Actual Depth 46.610

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1013	0	46.694	Pump	ON					
1023	0.15	40.230	28.70	1.984	0.57	7.10	-118.3	—	
1040	0.50	37.917	27.65	1.819	0.29	7.10	-102.5	5.04	
1050	0.75	37.940	27.34	1.740	0.24	7.11	-87.2	2.09	
1100	1.00	37.613	27.06	1.694	0.20	7.12	-90.1	3.10	
1110	1.15	37.621	26.96	1.684	0.20	7.12	-86.0	2.50	
1115	1.25	37.729	26.92	1.682	0.20	7.12	-80.8	4.80	
1125	1.55	37.805	26.75	1.678	0.20	7.13	-79.0	3.57	
1144	2.15	37.610	26.76	1.683	0.18	7.15	-73.1	4.02	
1150	2.25	37.316	26.71	1.686	0.18	7.15	-73.3	3.39	
1156	2.50	37.114	26.49	1.690	0.18	7.14	-76.6	3.02	
1202	2.60	37.952	26.52	1.689	0.17	7.14	-77.3	3.72	
1209	2.90	34.186	24.88	1.721	0.18	7.14	-77.0	4.27	
1211	START SAMPLE COLLECTION								
1224	END SAMPLE COLLECTION: 2L IPEC								
	Pump	OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200704293

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.



# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-36-41  
SAMPLE ID: 013

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Humid, P. Cloudy, 80's

PROJECT NO: 01.0017869.92  
DATE: 7/29/10  
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{41}{\text{DTB}} \cdot \frac{4.36}{\text{DTW}} = \frac{36.64}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 36.64 x 0.041 Multiplier = 1.5 gal Well Volume

1.5 x 1.5 = 2.25 gal Designed Purge Volume

TOTAL VOLUME PURGED: 2.60 gal

WATER QUALITY: DTW = 4.36 Transducer Actual Depth N/A

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1013	0	4.36	Pump ON	DN					
1023	0.15	14.67	29.09	8.092	0.53	8.09	-192.1	—	
1040	0.50	19.74	28.46	3.102	0.30	7.82	-189.2	4.83	
1050	0.75	25.27	27.82	2.776	0.44	7.77	-176.5	4.27	
1100	1.00	24.55	27.25	2.982	0.43	7.72	-170.1	3.99	
1110	1.25	25.20	27.06	3.297	0.60	7.71	-161.8	3.78	
1115	1.40	24.67	27.03	3.540	0.80	7.70	-153.0	3.29	
1125	1.75	24.82	27.03	3.747	1.14	7.69	-138.3	2.71	
1144	2.00	25.07	27.28	3.779	1.45	7.67	-127.0	3.37	
1150	2.25	27.00	27.22	3.811	1.52	7.67	-124.8	3.74	
1155	START SAMPLE COLLECTION								
1204-1223	END SAMPLE COLLECTION IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200704293

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-36-24  
 SAMPLE ID: 019

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Humid, P. Cloudy, 80's

PROJECT NO: 01.0017869.92  
 DATE: 7/29/10  
 SAMPLER(S): CB, MB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 4.15 Transducer Actual Depth 56.719

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
1013	56.719	PUMP	DN						0
1023	56.720	30.64	7.235	0.98	7.39	49.5	—		0.05
1040	56.723	30.66	7.342	0.53	7.64	3.6	8.92		0.35
1050	56.726	30.69	7.266	1.10	7.66	21.7	2.07		0.55
1100	56.726	30.71	7.184	0.87	7.67	27.2	1.78		0.70
1110	56.730	30.72	7.134	0.60	7.67	28.9	1.85		0.80
1115	56.724	30.72	7.133	0.46	7.67	30.2	2.56		0.90
1120	56.727	30.74	7.088	0.56	7.67	29.6	2.34		1.00
1125	56.720	30.73	7.078	0.52	7.67	29.8	2.18		1.05
1130	56.720	30.75	7.063	0.51	7.67	32.2	2.25		1.15
1134	START	SAMPLE COLLECTION							
1204	END SAMPLE	COLLECTION 1.2L IPEC							
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
flow meter	1
turbidity meter	200704293

**NOTES AND OBSERVATIONS:** Total volume purged 1.65 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.



WELL ID: MW 30-84

SAMPLE ID: 024

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 80'S

PROJECT NO: 01 0017869.92  
 DATE: 7/28/10  
 SAMPLER(S): CB/MR

SAMPLING INTERVAL (depth in ft below top of casing)  
77.3 to 85.4

TOTAL VOLUME PURGED: 0.50 gal

SAMPLING PORT  
84

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1115	0	PUMP	ON					6/12	33
1125	0.001	27.71	0.004	5.83	7.01	175.7	---	↓	↓
1135	0.002	27.90	0.004	6.12	7.01	171.6	---	↓	↓
1145	0.003	28.00	0.004	6.23	7.00	166.8	---	↓	↓
1155	0.004	28.19	0.004	6.28	7.00	160.7	---	7/10	33
1205	0.005	28.29	0.004	6.14	7.00	143.4	---	8/9	33
1220	0.007	28.49	0.008	5.95	7.01	78.8	---	10/7.5	40
1227	0.015	28.76	1.825	4.65	7.23	60.4	---	↓	↓
1235	0.05	28.84	1.837	4.42	7.31	38.4	---	↓	↓
1240	0.10	28.88	1.840	4.38	7.33	36.3	---	↓	↓
1245	0.15	28.89	1.842	4.30	7.34	37.0	---	↓	↓
1250	0.20	28.90	1.844	4.29	7.36	38.1	---	↓	↓
1251	START SAMPLE COLLECTION								
1307	END SAMPLE COLLECTION: 2 L IPEC								
			0.52	IPEC					
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	N/A

NOTES AND OBSERVATIONS:

WELL ID: MW 31-63

SAMPLE ID: 025

**GZA GeoEnvironmental of New York  
Waterloo Sampling Data Sheet**

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 80's

PROJECT NO: 01.0017869.92  
 DATE: 7/27/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
55.8 to 63.8

TOTAL VOLUME PURGED: 0.75 gal

SAMPLING PORT  
63

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1238	0	PUMP	ON					7/10	30
1258	0.01	31.17	1.675	1.18	6.72	-42.8	—	9/10	20
1310	0.05	33.18	1.640	0.42	6.80	-46.1	10.22		
1320	0.075	34.22	1.597	0.45	7.00	-46.3	7.78		
1330	0.10	35.28	1.548	0.48	7.07	-37.0	5.70		
1328	0.12	35.81	1.529	0.52	7.10	-32.8	8.57		
1344	0.14	36.34	1.505	0.54	7.11	-28.5	4.79		
1355	0.15	36.87	1.472	0.55	7.11	-22.6	5.11		
1402	0.20	36.87	1.480	0.57	7.12	-20.9	4.48		
1415	0.25	36.86	1.485	0.58	7.13	-19.5	3.70		
1423	0.28	36.84	1.481	0.56	7.14	-19.3	3.41		
1430	0.30	36.86	1.482	0.52	7.13	-14.8	3.52		
1433	START SAMPLE COLLECTION								
1554	END SAMPLE COLLECTION: 2L IPEC 0.5 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 31-85

SAMPLE ID: 025

## GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 80's

PROJECT NO: 01.0017869.92  
 DATE: 7/27/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
69.8 to 85.4

TOTAL VOLUME PURGED: 1.0 gal

SAMPLING PORT  
85

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH * (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1238	0	PUMP ON						7/10	30
1258	0.15	28.60	2.217	1.31	32.00*	-86.5	—	9/10	20
1310	0.25	30.27	2.723	1.90	31.32*	-49.7	8.90		
1320	0.25	31.13	2.182	2.00	29.91*	-70.7	6.41		
1330	0.35	31.68	2.159	2.30	29.59	-5.5	4.27		
1338	0.45	32.23	2.127	2.25	29.91	7.7	3.95		
1344	0.50	32.73	2.123	2.42	30.33	15.9	3.76		
1355	0.60	32.74	2.103	2.62	30.03	48.2	3.79		
1402	0.70	32.35	2.093	2.76	30.18	50.5	3.82		
1415	0.80	32.28	2.086	2.78	30.07	66.8	3.77		
1423	0.90	32.25	2.077	2.76	30.29.98	70.8	3.81		
1430	START SAMPLE COLLECTION								
1522	END SAMPLE COLLECTION. 2LT PEC 0.5 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200701254

NOTES AND OBSERVATIONS:  
 \*pH SENSOR NOT WORKING PROPERLY.

WELL ID: MW 31-49

SAMPLE ID: 025

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 80's

PROJECT NO: 01.0017869.92  
 DATE: 7/27/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
34.8 to 49.3

TOTAL VOLUME PURGED: 2.50 gal

SAMPLING PORT  
49

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1238	0	PUMP ON						7/10	30
1258	0.80	23.51	1.919	5.89	6.97	43.9	—	9/10	20
1310	1.15	23.31	1.819	3.65	6.88	108.7	8.29		
1320	1.25	23.63	1.766	3.63	6.89	71.2	10.71		
1330	1.50	23.67	1.733	3.67	6.84	86.8	8.65		
1338	1.75	23.75	1.712	3.71	6.83	98.2	6.58		
1344	2.00	23.69	1.683	3.80	6.82	108.5	8.39		
1355	2.35	23.42	1.653	3.98	6.79	116.2	5.23		
1402	2.5	23.31	1.644	4.03	6.79	120.1	5.47		
1415	2.75	23.29	1.639	4.07	6.78	124.9	5.80		
1423	START SAMPLE COLLECTION								
1443	END SAMPLE COLLECTION: 2 L IPEC								
	0.5 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	1 200702274

NOTES AND OBSERVATIONS:

WELL ID: MW 32 - 59

SAMPLE ID: 019

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90's

PROJECT NO: 01.0017869.92  
 DATE: 7/27/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
28.3 to 61.3

TOTAL VOLUME PURGED: 1.05 gal

SAMPLING PORT  
59

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

6

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1140	0	PUMP ON						8/8	26
1147	0.01	23.92	0.768	1.71	6.72	82.9	—		
1153	0.1	23.26	0.692	4.75	7.04	65.8	9.13		
1200	0.25	23.05	0.674	5.12	7.25	69.8	12.05		
1206	0.35	22.98	0.668	5.22	7.36	72.8	11.91		
1214	0.50	23.08	0.662	5.16	7.49	75.5	10.74		
1222	0.70	22.95	0.660	5.01	7.53	75.8	10.82		
1227	0.80	23.01	0.659	5.00	7.55	76.4	10.90		
1232	0.90	23.03	0.659	5.07	7.58	75.1	10.91		
1233		PUMP OFF							
1235		START SAMPLE COLLECTION							
1300		SAMPLE COMPLETED : 2 L IPEC 0.5 L IPEC							
1300		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200701254

NOTES AND OBSERVATIONS:



WELL ID: MW 32-48

SAMPLE ID: 008

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90's

PROJECT NO: 01.0017869.92  
 DATE: 7/27/08  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
28.3 to 61.3

TOTAL VOLUME PURGED: 1.35 gal

SAMPLING PORT  
48

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

7

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1140	0	PUMP ON						8/8	26
1147	0.1	22.83	0.330	6.18	7.00	168.3	—		
1153	0.2	22.32	0.304	6.07	7.34	162.8	14.50		
1200	0.4	22.22	0.288	6.11	7.56	156.2	10.16		
1206	0.5	22.18	0.283	6.16	7.77	148.7	12.63		
1214	0.7	22.21	0.280	6.21	8.00	142.2	11.08		
1222	0.9	22.12	0.280	6.27	8.09	132.0	11.16		
1227	1.1				8.11	129.9	11.19		
1232	1.2	22.20	0.282	6.32	8.16	128.2	11.24	↓	↓
1233		PUMP OFF							
1235		START SAMPLE COLLECTION							
1252		SAMPLE COMPLETED : 2 L IPEC 0.5 L IPEC							
1252		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	3 <u>200701254</u>

NOTES AND OBSERVATIONS:

WELL ID: MW 32-190

SAMPLE ID: 021

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
 DATE: 7/26/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
180.3 to 193.9

TOTAL VOLUME PURGED: 0.70 gal

SAMPLING PORT  
190

PURGE RATE: variable (gal/min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
1311	0	PUMP ON						8/8	49
1320	0.05	26.63	1.748	0.61	6.88	-169.5	—	10/9	47
1340	0.10	27.48	1.750	0.42	6.91	-199.7	13.21	10/12	49
1350	0.13	27.50	1.753	0.30	6.95	-195.0	12.05		
1400	0.15	27.51	1.764	0.22	7.04	-196.9	11.14		
1410	0.20	27.29	1.759	0.15	7.07	-188.1	9.01		
1420	0.25	27.40	1.755	0.13	7.08	-184.0	8.99		
1429	0.30	27.37	1.755	0.12	7.09	-181.2	8.96		
1434	0.40	27.39	1.755	0.11	7.10	-180.1	9.09		
1442	0.45	27.41	1.755	0.10	7.10	-178.6	9.11		
1450	0.55	27.34	1.754	0.10	7.09	-179.5	9.04	↓	↓
1451		PUMP OFF							
1453		START SAMPLE COLLECTION							
1541		SAMPLE COMPLETED : 2 L IPEC 0.5 L IPEC							
1541		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	2
turbidity meter	200701254

NOTES AND OBSERVATIONS:

WELL ID: MW 32 - 173

SAMPLE ID: 017

GZA GeoEnvironmental of New York  
Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
DATE: 7/26/10  
SAMPLER(S): C.B., MB

SAMPLING INTERVAL (depth in ft below top of casing)  
165.8 to 174.3

TOTAL VOLUME PURGED: 1.05 gal

SAMPLING PORT  
173 2

PURGE RATE: variable (gal / min)  
PURGE METHOD: Double Valve Pump

WATER QUALITY:

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1311	0		PUMP ON					8/8	49
1320	0.15	25.62	2.066	0.49	6.98	-199.2	—	10/9	47
1340	0.25	25.88	2.062	0.43	7.03	-206.0	15.91	10/12	49
1350	0.35	25.62	2.069	0.35	7.12	-212.8	16.20		
1400	0.45	25.18	2.083	0.32	7.15	-212.5	15.78		
1410	0.60	25.11	2.097	0.30	7.16	-212.2	11.54		
1420	0.70	25.12	2.099	0.29	7.16	-212.3	11.39		
1429	0.80	25.15	2.103	0.29	7.16	-211.9	11.45		
1434	0.90	25.17	2.107	0.29	7.16	-211.6	11.37		
1435		PUMP OFF							
1436		START SAMPLE COLLECTION							
1517		SAMPLE COMPLETED							
1517		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	3 200701254

NOTES AND OBSERVATIONS:



WELL ID: MW 32-85

SAMPLE ID: 022

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sun + clouds 80's

PROJECT NO: 01.0017869.92  
 DATE: 7/26/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
79.3 to 92.8

TOTAL VOLUME PURGED: 1.40 gal

SAMPLING PORT  
85

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

5

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1311	0	PUMP ON						8/8	49
1320	0.20	23.42	1.626	3.00	6.62	-68.5	—	10/9	47
1340	0.40	23.11	1.627	1.64	6.70	-71.4	12.21	10/12	49
1350	0.60	22.99	1.635	1.25	6.84	-67.6	11.76		
1400	0.80	22.92	1.638	1.25	6.87	-61.2	11.15		
1410	0.95	22.87	1.643	1.28	6.91	-60.0	9.21		
1420	1.05	22.89	1.645	1.28	6.93	-59.3	9.09		
1425	1.15	22.91	1.645	1.28	6.93	-58.8	9.01		
1430	1.25	22.93	1.645	1.28	6.94	-56.9	9.07	↓	↓
1430		PUMP OFF							
1431		START SAMPLE COLLECTION							
1451		SAMPLE COMPLETED:			12 L	IPEC			
1451		PUMP OFF			10.5 L	IPEC			

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 200701254

NOTES AND OBSERVATIONS:

WELL ID: U3-T1  
 SAMPLE ID: 029

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Summer, 80's

PROJECT NO: 01.0017869.92  
 DATE: 7/26/10  
 SAMPLER(S): CB10  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 4.30 Transducer Actual Depth 2.781

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes gal
095	2.781								
1030	2.834	PUMP ON							
1036	2.837	27.24	1.174	2.10	7.54	238.4	—		0.01
1045	2.845	27.42	1.162	1.13	7.73	204.2	5.68		0.15
1051	2.847	27.54	1.160	1.07	7.79	181.4	4.80		0.20
1055	2.854	27.59	1.159	0.69	7.82	169.1	1.97		0.25
1100	2.854	27.57	1.160	0.65	7.82	157.9	2.01		0.30
1105	2.856	27.59	1.158	0.63	7.83	154.4	1.78		0.35
1110	2.860	27.69	1.158	0.87	7.84	152.3	2.50		0.40
1115	2.862	27.83	1.156	0.81	7.85	148.2	2.83		0.50
1120	2.865	27.94	1.157	0.76	7.86	143.4	2.04		0.55
1125	2.867	28.01	1.158	0.65	7.86	141.9	1.96		0.70
1130	2.871	28.05	1.158	0.57	7.86	137.8	1.79		0.75
1135	2.877	28.06	1.157	0.60	7.86	129.8	1.84		0.80
1140	2.881	28.10	1.157	0.56	7.86	124.1	1.86		0.95
1143	START SAMPLE COLLECTION								
1215	END SAMPLE COLLECTION. 2 L IPEC								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
Flow meter	1
turbidity meter	200704293

BATTERY #5

NOTES AND OBSERVATIONS: Total volume purged 1.20 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

WELL ID: U3-T2  
 SAMPLE ID: 034

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: SUNNY, 80S

PROJECT NO: 01.0017869.92  
 DATE: 7/26/10  
 SAMPLER(S): CB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 4.21 Transducer Actual Depth 2.618

Time	DTW or <u>Actual Depth</u>	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Flow Rate (gal/hr)	Notes
1313	2.754	PUMP	ON						
1323	2.717	34.97	1.628	1.37	7.69	-74.7	—		0.01
1333	2.717	35.30	1.645	0.64	7.77	-101.2	6.45		0.25
1340	2.721	35.50	1.659	0.47	7.77	-136.7	3.36		0.40
1345	2.725	35.58	1.662	0.44	7.77	-144.5	3.31		0.60
1350	2.722	35.69	1.661	0.39	7.76	-144.1	2.36		0.75
1355	2.720	35.74	1.660	0.37	7.76	-155.6	2.53		1.00
1400	2.718	35.79	1.659	0.36	7.76	-157.3	2.45		1.15
1405	2.712	35.84	1.657	0.34	7.76	-158.5	2.38		1.25
1407	START SAMPLE COLLECTION								
1426	END SAMPLE COLLECTION								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
flow meter	3
turbidity meter	200704293

BATTERY #5  
 NOTES AND OBSERVATIONS: Total volume purged 1.45 gal  
 Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.







# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: 43-4D  
SAMPLE ID: 025

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Mostly cloudy, showers 80's

PROJECT NO: 01.0017869.92  
DATE: 07/23/10  
SAMPLER(S): CB, MB

WATER COLUMN HEIGHT (ft) Well Diameter: 4 in

$$\frac{27.25}{\text{DTB}} - \frac{10.15}{\text{DTW}} = \frac{17.10}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 17.10 x 0.653 Multiplier = 11.17 gal Well Volume

11.17 x 1.5 = 16.75 gal Designed Purge Volume

TOTAL VOLUME PURGED: 8.25 gal

**WATER QUALITY:** DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1008	0	→	PUMP ON						
1013	0.2+0.2		32.27	1.685	0.88	8.67	104.1	10.39	
1020	0.9+0.5		32.57	1.612	0.84	8.75	100.0	6.22	
1025	1.5+0.8		32.65	1.595	1.11	8.75	99.8	6.12	
1030	2.2+1.3		32.91	1.555	1.37	8.72	102.6	6.48	
1037	3.2+2.2		33.33	1.379	2.09	8.51	90.4	7.16	
1043	3.8+2.8		33.33	1.358	2.17	8.45	81.5	7.59	
1049	4.2+3.4 = 7.6		32.89	1.364	2.12	8.44	79.4	6.63	
1055	7.9		32.71	1.369	2.04	8.43	66.2	7.36	
1058	8.1		32.59	1.385	2.43	8.43	60.0	—	
1058			Well dry. Let recharge						
1058			PUMP OFF						
1258			START SAMPLE COLLECTION						
1321			SAMPLE COMPLETED : 2 L. IPEC						
1321			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>4</u> <u>200701254</u>

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.

# GZA GeoEnvironmental of New York

## Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-46  
SAMPLE ID: 021

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: OVERCAST, HUMID, 88°F

PROJECT NO: 01.0017869.92  
DATE: 7/23/10  
SAMPLER(S): CB

WATER COLUMN HEIGHT (ft) Well Diameter: 4 in

<u>29.7</u> DTB	-	<u>4.49</u> DTW	=	<u>25.21</u> Water Column Height	ft
--------------------	---	--------------------	---	-------------------------------------	----

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 25.21 x 0.653 = 16.46 gal  
Multiplier Well Volume

16.46 x 1.5 = 24.69 gal  
Designed Purge Volume

TOTAL VOLUME PURGED: gal

WATER QUALITY: DTW = 4.49 Transducer Actual Depth 23.400

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
0944		23.400							
1013	0	23.403	PUMP ON	DN					
1020	1.50	21.289	21.46	1.246	0.59	6.52	-101.0	13.50	
1032	2.50	20.281	21.99	1.354	0.33	6.85	-79.1	10.36	
1044	4.00	19.301	21.71	1.355	0.28	6.97	-95.9	9.53	
1100	6.00	18.723	21.65	1.353	0.24	7.05	-87.1	8.65	
1112	7.75	17.557	21.19	1.351	0.19	7.04	-93.4	7.44	
1125	9.00	18.129	21.64	1.352	0.22	7.15	-105.3	6.24	
1135	10.50	18.063	21.59	1.351	0.21	7.17	-108.3	7.18	
1145	12.00	17.371	21.45	1.350	0.17	7.18	-98.0	6.03	
1157	14.50	16.074	21.30	1.302	0.17	7.20	-102.5	5.76	
1220	16.25	17.697	21.25	1.121	1.14	7.19	-77.3	7.97	
1231	19.50	17.001	21.33	1.093	2.64	7.21	-51.0	10.73	
1243	22.00	15.799	21.20	1.000	4.95	7.23	-19.6	10.99	
1255	23.50	13.624	21.01	0.994	5.15	7.22	-15.1	13.73	
1300	24.70	13.651	21.06	0.951	5.70	7.24	-19.3	14.13	

1301 START SAMPLE COLLECTION	<b>Equipment Identification #</b>
1310 END SAMPLE COLLECTION: 2L IPEC PUMP OFF Equipment Used	
YSI 556 MPS Reader and 5563 Sonde turbidity meter	
	5 200704293

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW 39-67

SAMPLE ID: 009

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 7/22/10  
 SAMPLER(S): C.B., M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
65.0 to 70.5

TOTAL VOLUME PURGED: 2.55 gal

SAMPLING PORT  
67 7

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1224	0	PUMP	ON					6/8	40
1232	0.50	17.04	2.296	9.25	7.75	-85.0			
1240	0.75	16.81	2.456	10.12	7.81	-54.1	8.77		
1246	1.00	17.47	2.488	9.95	7.82	-37.9		6/15	34
1247		PUMP	OFF						
1300		PUMP	ON					6/18	36
1305	1.20	22.57	2.522	8.57	7.61	-6.2	8.67	6/16	36
1311	1.25	22.63	2.523	8.33	7.57	-4.3	8.87	6/14	36
1318	1.40	22.80	2.528	7.60	7.45	+0.9	5.58	↓	↓
1326	1.65	21.	2.559	7.50	7.36	1.4	7.44	↓	↓
1332	1.95	20.80	2.559	7.06	7.32	3.1	5.32	↓	↓
1340	2.10	20.78	2.541	6.65	7.30	5.4	3.77	↓	↓
1345	2.20	20.78	2.547	6.53	7.30	6.7	3.46	↓	↓
1350	2.30	20.72	2.544	6.41	7.29	8.0	3.44	↓	↓
1355	2.40	20.67	2.548	6.32	7.29	9.4	3.40	↓	↓
1400	START	SAMPLE COLLECTION							
1426	END	SAMPLE COLLECTION							
1426	PUMP	OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	3
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 39.84

SAMPLE ID: 009

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 7/22/10  
 SAMPLER(S): C.B., MB

SAMPLING INTERVAL (depth in ft below top of casing)  
76.5 to 85.0

TOTAL VOLUME PURGED: 1.30 gal

SAMPLING PORT  
84 6

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1224	0	PUMP	ON					6/8	40
1232	0.08	20.10	2.407	2.33	6.69	-192.1	—		
1240	0.25	20.17	2.344	3.44	7.03	-130.4	6.88		
1246	0.30	21.10	2.322	3.61	7.07	-135.1		6/15	34
1247		PUMP	OFF						
1300		PUMP	ON					6/18	36
1305	0.35	23.99	2.332	3.41	7.11	-112.4	7.43	6/16	36
1311	0.37	24.39	2.335	3.20	7.11	-109.7	7.51	6/14	36
1318	0.39	24.00	2.352	3.27	7.13	-102.5	5.39		
1326	0.50	22.70	2.396	3.75	7.17	-87.0	5.46		
1332	0.60	21.53	2.377	3.85	7.18	-77.7	5.04		
1340	0.70	21.33	2.377	3.84	7.18	-71.2	2.42		
1345	0.80	21.48	2.377	3.82	7.19	-67.0	3.77		
1350	0.90	21.36	2.380	3.91	7.18	-62.7	3.18		
1355	0.95	21.20	2.386	3.87	7.18	-58.9	2.73		
1400	1.05	21.22	2.384	3.84	7.19	-56.2	2.52		
1405	1.10	21.24	2.388	3.86	7.19	-53.1	2.56		
1410	1.15	21.24	2.389	3.82	7.19	-52.0	2.51	↓	↓
1413	START SAMPLE COLLECTION								
1442	SAMPLE COMPLETED: 2 L IPEC								
1442	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	4
turbidity meter	200704293

NOTES AND OBSERVATIONS:

WELL ID: MW 39-102

SAMPLE ID: 009

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 07/22/10  
 SAMPLER(S): C.B., M.B.

SAMPLING INTERVAL (depth in ft below top of casing)  
93.0 to 103.0

TOTAL VOLUME PURGED: 1.45 gal

SAMPLING PORT  
102 4

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1224	0	Pump ON						6/8	40
1232	0.05	21.32	2.624	1.49	6.60	-178.0			
1240	0.20	20.81	2.565	2.34	6.89	-132.6	6.83		
1246	0.25	21.55	2.545	2.43	6.97	-97.6		6/15	34
1247		Pump OFF							
1300		PUMP ON						6/18	36
1305	0.30	24.31	2.551	2.08	7.04	-61.2	6.43	6/16	36
1311	0.35	24.40	2.557	2.00	7.04	-64.2	8.74	6/14	36
1318	0.50	24.47	2.560	2.01	7.05	-62.8	6.22		
1326	0.70	22.41	2.580	2.32	7.07	-51.6	5.02		
1332	0.75	21.83	2.555	2.31	7.06	-46.9	4.97		
1340	0.80	21.82	2.552	2.22	7.06	-42.8	3.87		
1345	0.85	21.84	2.553	2.20	7.06	-39.7	3.55		
1350	0.95	21.88	2.553	2.24	7.07	-36.7	3.08		
1355	1.05	21.89	2.553	2.26	7.07	-37.0	2.54		
1400	1.10	21.82	2.552	2.23	7.07	-32.9	2.38		
1405	1.15	21.82	2.554	2.28	7.08	-32.2	2.68		
1410	1.20	21.86	2.551	2.27	7.08	-29.1	2.51		
1415	1.30	21.81	2.552	2.27	7.08	-27.5	2.49		
1420	START	SAMPLE COLLECTION							
1452	SAMPLE COMPLETED	: 2 L IPEC							
1452	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	<u>6</u> 200704293

NOTES AND OBSERVATIONS:



WELL ID: MW 39.183

SAMPLE ID: 009

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 7/22/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
169.5 to 186.0

TOTAL VOLUME PURGED: 1.75 gal

SAMPLING PORT  
183 2

PURGE RATE: variable (gal / min)

PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1027	0	PUMP ON						8/10	70
1040	0.1	20.80	1.166	1.05	6.88	-293.8	9.08		
1047	0.3	20.31	1.166	0.51	7.09	-288.6	8.69		
1053	0.5	19.77	1.158	0.40	7.16	-276.5	8.58		
1058	0.8	19.22	1.148	0.37	7.19	-273.1	8.56		
1106	1.1	18.76	1.130	0.34	7.17	-269.9	7.64		
1114	1.4	18.70	1.122	0.33	7.17	-272.2	7.57		
1119	1.6	18.70	1.112	0.32	7.18	-271.1	7.61	↓	↓
1120		PUMP OFF							
1121		START SAMPLE COLLECTION							
1138		SAMPLE COMPLETED : 2 L IPEC							
1138		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	3 200704293

NOTES AND OBSERVATIONS:



WELL ID: MW 39.124

SAMPLE ID: 009

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Mostly sunny 90°F

PROJECT NO: 01.0017869.92  
 DATE: 7/22/10  
 SAMPLER(S): CB, MB

SAMPLING INTERVAL (depth in ft below top of casing)  
115.0 to 126.5

TOTAL VOLUME PURGED: 3.55 gal

SAMPLING PORT  
124 3

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)
1027	0	PUMP ON						8/10	70
1040	0.3	18.45	2.763	1.24	6.61	-286.3	17.10		
1047	0.6	17.91	2.762	0.84	6.66	-280.0	15.71		
1053	1.0	17.52	2.753	0.60	6.68	-270.6	15.05		
1058	1.8	17.17	2.744	0.83	6.69	-250.0	11.66		
1106	2.3	16.89	2.671	1.42	6.80	-180.4	10.26		
1114	2.5	16.78	2.610	1.50	6.79	-146.9	9.71		
1119	3.0	16.73	2.596	1.56	6.79	-153.1	9.85		
1127	3.4	16.69	2.595	1.54	6.78	-148.8	9.66	↓	↓
1128		PUMP OFF							
1130		START SAMPLE COLLECTION							
1139		SAMPLE COMPLETED : 2 L IPEC							
1139		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	4 200704293

NOTES AND OBSERVATIONS:



# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-44-66  
SAMPLE ID: 010 017

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: SUNNY, 88°F

PROJECT NO: 01.0017869.92  
DATE: 7/22/10  
SAMPLER(S): CB

WATER COLUMN HEIGHT (ft) Well Diameter: 2 in

$$\frac{67}{\text{DTB}} - \frac{59.73}{\text{DTW}} = \frac{7.27}{\text{Water Column Height}}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 7.27 x 0.163 Multiplier = 1.185 gal Well Volume

1.185 x 1.5 = 1.78 gal Designed Purge Volume

**TOTAL VOLUME PURGED:** 1.78 gal

WATER QUALITY: DTW = 59.73 Transducer Actual Depth 4.926

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes	Drive PRES
1035	0	Pump	ON						10/9	88
1050	0.75	4.9	18.19	1.028	7.60	6.42	64.3	—	↓	
1055	1.00	1.771	19.44	1.029	6.06	6.56	57.9	—	10/15	
1100	1.05	1.771	20.61	1.036	5.41	6.76	45.4	107.5		
1105	1.15	1.776	21.79	1.042	4.81	6.94	36.3	87.40		
1110	1.25	1.764	23.24	1.040	4.36	7.03	30.7	93.18		
1115	1.30	1.761	23.81	1.050	4.83	7.04	19.7	—		
1120	1.35	WELL	DRY	LET RECHARGE		BEFORE	SAMPLING.		↓	↓
1538		START SAMPLE COLLECTION								
1547		END SAMPLE COLLECTION: 2L IPEC								
		PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200701254

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.



# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-41-63  
SAMPLE ID: 016

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: SUNNY, HUMID, 80's

PROJECT NO: 01.0017869.92  
DATE: 7/21/10  
SAMPLER(S): CA/B/B

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{63}{\text{DTB}} \cdot \frac{27.52}{\text{DTW}} = \frac{35.48}{\text{Water Column Height}} \text{ ft}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 35.48 x  $\frac{0.041}{\text{Multiplier}}$  =  $\frac{1.45}{\text{Well Volume}}$  gal

1.45 x 1.5 =  $\frac{2.175}{\text{Designed Purge Volume}}$  gal

**TOTAL VOLUME PURGED: 2.4 gal**

**WATER QUALITY:** DTW = \_\_\_\_\_ Transducer Actual Depth \_\_\_\_\_

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
0852	0	PUMP	ON						
0857	0.4	<del>18.95</del>	18.95	2.078	5.38	6.82	222.0	23.88	
0900	0.9	—	18.30	2.044	4.89	6.56	198.6	26.77	
0904	1.5	—	18.20	2.097	4.69	6.32	173.6	—	
0905	PUMP OFF								
0909	PUMP ON								
0912	2.0	—	20.63	2.432	4.36	6.47	139.2	20.8	
0916	2.2	—	19.87	2.151	4.33	6.39	130.0	20.16	
0916	START SAMPLE COLLECTION								
0923	END SAMPLE COLLECTION								
	PUMP OFF								

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	4
turbidity meter	20070

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.

# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-44-102  
SAMPLE ID: 017018

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Hot, humid

PROJECT NO: 01.0017869.92  
DATE: 7/21/10  
SAMPLER(S): MB/CB

WATER COLUMN HEIGHT (ft) Well Diameter: 1 in

$$\frac{102}{\text{DTB}} - \frac{69.17}{\text{DTW}} = \frac{32.83}{\text{Water Column Height}}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 32.83 x 0.041 Multiplier = 1.35 gal Well Volume

1.35 x 1.5 = 2.01 gal Designed Purge Volume

**TOTAL VOLUME PURGED:** \_\_\_\_\_ gal

WATER QUALITY: DTW = 69.17 Transducer Actual Depth = 29.563 Transd. read = 234.5

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1255	0		PUMP ON						
1259	0.15	—	22.31	1.261	6.78	7.28	130.7	149.0	
1304	0.80	—	20.28	1.300	7.09	7.13	129.6	224.0	
1309	1.50	—	19.02	1.285	6.76	7.11	119.0	280.0	
1312	2.0	—	19.07	1.277	6.99	7.07	115.3	460.0	
1314	2.2		19.33	1.277	6.99	7.08	111.9	621.0	
1314			PUMP OFF						
1315			START SAMPLE COLLECTION						
1320			SAMPLE COMPLETED : 2 L IPEC						
1320			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	4 200704293

**NOTES AND OBSERVATIONS:**  
Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.

WELL ID: MW-43-28  
 SAMPLE ID: 016

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: WARM, 88°F, HUMID, SUNNY

PROJECT NO: 01.0017869.92  
 DATE: 7/20/10  
 SAMPLER(S): CSMB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 15.74 Transducer Actual Depth 25.971 TRANSDUCER SURFACE: 32.280

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes gal
1003	25.971	Pump ON						5.5/22	16	
1023	25.772	28.43	4.865	4.55	7.28	207.6	—			0.01
1035	25.723	29.16	4.919	1.69	7.25	109.4	—			0.05
1045	25.662	29.77	4.933	1.35	7.24	78.6	11.98			0.10
1055	25.623	30.14	4.942	1.20	7.21	105.8	9.51			0.15
1105	25.589	30.25	4.973	1.08	7.09	63.7	10.19			0.20
1115	25.560	29.57	4.989	1.03	7.18	62.1	8.25			0.25
1125	25.515	29.45	4.973	0.73	7.16	54.1	7.65			0.30
1130	25.508	29.26	4.973	0.66	7.16	51.6	5.49			0.35
1136	25.493	29.21	4.963	0.64	7.13	49.8	6.44			0.35
1140	25.490	28.85	4.971	1.03	7.12	54.1	5.42			0.38
1145	25.481	28.83	4.958	1.00	7.15	56.5	5.55			0.42
1150	25.468	28.84	4.949	0.73	7.11	51.8	4.31			0.45
1155	25.461	28.76	4.953	0.65	7.12	49.4	5.67			0.47
1200	25.459	28.75	4.949	0.59	7.10	46.7	5.47			0.50
1205	25.447	28.73	4.946	0.55	7.08	45.0	5.26			0.52
1209	START SAMPLE COLLECTION									0.65
1348	END SAMPLE COLLECTION: 2L IPEC									
	PUMP OFF									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	6
turbidity meter	200701254

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

Total volume purged 0.85 gal

WELL ID: MW-43-62  
 SAMPLE ID: 016

## GZA GeoEnvironmental of New York Low-Flow Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Humid, 88°F

PROJECT NO: 01.0017869.92  
 DATE: 7/20/10  
 SAMPLER(S): CBMB  
 PUMP DEPTH: \_\_\_\_\_ ft

WATER QUALITY: DTW = 17.99      <sup>SURFACE</sup> Transducer Actual Depth 29.826      <sup>TRANSDUCER</sup> ACTUAL DEPTH 33.882

Time	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
1325	33.882	Pump	ON					6/6	32	
1335	33.219	19.89	2.846	10.51	6.98	72.4	—			0.10
1345	33.116	20.02	2.829	3.87	6.94	68.0	7.57			0.30
1355	33.102	20.13	2.834	3.34	6.96	66.7	9.77			0.55
1400	33.109	20.00	2.832	3.27	6.98	66.3	10.44			0.75
1405	33.024	19.94	2.834	3.24	6.98	66.1	10.55		30	0.85
1412	32.990	20.41	2.832	3.11	6.98	65.8	15.07			1.05
1420	32.992	20.01	2.834	3.12	6.98	65.5	14.33			1.25
1425	32.985	20.05	2.830	2.99	6.94	64.1	11.78			1.35
1430	32.969	19.89	2.826	2.98	6.98	63.8	11.99			1.45
1435	32.970	19.81	2.826	2.99	6.97	63.5	10.96			1.55
1440	32.972	19.83	2.825	2.98	6.97	63.2	10.63			1.65
1445	32.965	19.85	2.821	2.97	6.97	63.1	10.89			1.75
1449	START SAMPLE COLLECTION									2.15
1507	END SAMPLE COLLECTION									
	Pump OFF									

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	1
turbidity meter	200701254

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
 Groundwater Elevation measurements are given in feet msl.

Total volume purged 2.35 gal

# GZA GeoEnvironmental of New York

## Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-45-42  
SAMPLE ID: 021

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Thunder storms, 90's

PROJECT NO: 01.0017869.92  
DATE: 7/19/10  
SAMPLER(S): M. Britos

WATER COLUMN HEIGHT (ft) Well Diameter: \_\_\_\_\_ in

$$\frac{42}{\text{DTB}} - \frac{26.39}{\text{DTW}} = \frac{15.61}{\text{Water Column Height}}$$

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 15.61 x 0.163 Multiplier = 2.54 gal Well Volume

2.54 x 1.5 = 3.82 gal  
Designed Purge Volume

TOTAL VOLUME PURGED: 2.95 gal

WATER QUALITY: DTW = 26.39 Transducer Actual Depth = 14.681

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressure (psi)	Notes
1049	0	14.680	PUMP ON						5.5/7	30	
1053	0.01	13.800	20.13	1.453	3.21	7.14	150.0	—	5.5/7	26	
1056	0.10	13.652	19.83	1.497	2.70	7.40	144.4				
1100	0.30	12.863	19.45	1.517	1.71	7.52	134.3	7.78			
1104	0.50	11.758	19.34	1.524	1.35	7.55	125.3	5.69			
1110	1.0	10.456	19.18	1.517	1.05	7.58	112.0	7.11	5.5/7	28	
1116	1.5	8.757	19.03	1.422	1.54	7.65	99.8	12.96			
1121	1.8	7.488	19.05	1.436	1.39	7.64	92.3	13.68			
1127	2.2	5.777	19.05	1.479	1.00	7.63	85.2	10.41			
1131	2.5	4.441	19.10	1.496	0.83	7.62	81.1	11.26			
1136	2.8	3.541	19.50	1.514	1.59	7.59	76.4	—			
		Well dry. Let well recharge									
1530		Start sample collection									
1538		Sample completed 2 L IPEC									
1538		Pump off									

**Equipment Used**

**Equipment Identification #**

YSI 556 MPS Reader and 5563 Sonde  
turbidity meter

4  
200704293

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.

Groundwater Elevation measurements are given in feet msl.

*Excavation in MW-41/MW-45 area overflow after heavy rain earlier in the morning.*



# GZA GeoEnvironmental of New York Modified Traditional Purge Sampling Data Sheet

WELL ID: MW-45-61  
SAMPLE ID: 021

CLIENT: Entergy - IPEC  
SITE: Buchanan, NY  
WEATHER: Thunder storms 90's

PROJECT NO: 01.0017869.92  
DATE: 7/19/10  
SAMPLER(S): M. Britos

WATER COLUMN HEIGHT (ft) Well Diameter: \_\_\_\_\_ in

$\frac{61}{\text{DTB}} - \frac{26.94}{\text{DTW}} = \frac{34.06}{\text{Water Column Height}}$  ft

Diameter	Multipliers
1	0.041
2	0.163
4	0.653

**GALLONS OF WATER PER WELL VOLUME:**

Water Column Height 34.06 x  $\frac{0.041}{\text{Multiplier}}$  = 1.40 gal

1.40 x 1.5 = 2.10 gal

**TOTAL VOLUME PURGED: 2.25 gal**

WATER QUALITY: DTW = 26.94 Transducer Actual Depth - 44.724

Time	Volume Purged (gal)	DTW or Actual Depth	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Notes
1246	0	—	PUMP ON						
1250	0.1	—	21.76	0.601	7.02	5.31	112.7		
1255	0.15	—	22.00	0.969	5.51	5.25	102.5	40.40	
1300	0.50	—	21.26	1.046	4.00	5.43	96.9	40.46	
1305	0.85	—	21.15	1.150	2.67	5.65	92.3	41.47	
1310	1.40	—	21.05	1.204	1.94	5.80	87.8	78.64	
1315	1.80	—	21.09	1.238	1.66	6.02	79.6	94.42	
1320	2.10	—	21.25	1.251	1.67	6.21	76.4	87.63	
1321			PUMP OFF						
1322			START SAMPLE COLLECTION						
1328			SAMPLE COMPLETED : 2 L IPEC						
1328			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde	5
turbidity meter	200704293

**NOTES AND OBSERVATIONS:**

Depth and Depth to Water (DTW) measurements are given in feet from top of casing.  
Groundwater Elevation measurements are given in feet msl.





## **APPENDIX E POST-Q3 2010 MID-QUARTER SAMPLING DATA SHEETS**





WELL ID: MW 32-190

SAMPLE ID: 023

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny, 70's

PROJECT NO: 01.0017869.92  
 DATE: 9/9/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
180.3 to 193.9

TOTAL VOLUME PURGED: 1.25 gal

SAMPLING PORT  
190

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

WATER QUALITY: 2nd MID QUARTER

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Press (psi)
1010	0	PUMP ON						10/12	49
1017	0.05	21.62	1.761	5.01	6.70	-100.2	—	10/12	56
1027	0.20	20.87	1.752	0.29	6.91	-149.6	1.28	10/12	58
1035	0.30	20.51	1.749	0.21	7.02	-137.5	0.00		
1042	0.40	20.37	1.746	0.13	7.06	-127.9	0.00		
1047	0.50	20.29	1.744	0.14	7.08	-116.4	0.00		
1052	0.65	20.19	1.742	0.12	7.10	-114.6	0.00		
1057	0.80	20.12	1.740	0.10	7.10	-115.0	0.00		
1102	0.95	20.06	1.737	0.10	7.11	-120.0	0.00		
1107	1.10	20.09	1.735	0.09	7.11	-114.7	0.00		
1109		PUMP OFF							
1110		START SAMPLE COLLECTION							
1134		SAMPLE COMPLETED : 2 L IPEC							
		0.5 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 556J Sonde turbidity meter	2 LaMotte 2020/2530-1701

NOTES AND OBSERVATIONS:



WELL ID: MW 32-149

SAMPLE ID: 021

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Energy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny 70's

PROJECT NO: 01.0017869.92  
 DATE: 9/9/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
147.3 to 156.8

TOTAL VOLUME PURGED: 1.35 gal

SAMPLING PORT  
149 3

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

WATER QUALITY: 2nd MID QUARTER

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Press (psi)
1010	0	PUMP ON						10/12	49
1017	0.05	21.45	2060	1.99	6.93	-197.4	-	10/12	56
1027	0.20	20.71	2.129	0.54	7.08	-164.0	0.98	10/12	58
1035	0.50	20.36	2.153	0.40	7.10	-143.3	0.00		
1042	0.65	20.27	2.152	0.37	7.10	-139.8	0.00		
1047	0.75	20.21	2.151	0.36	7.11	-141.1	0.00		
1052	0.85	20.16	2.146	0.35	7.11	-142.3	0.00		
1057	1.00	20.05	2.146	0.35	7.11	-141.2	0.00		
1102	1.10	20.06	2.139	0.33	7.11	-135.1	0.00		
1107	1.20	20.07	2.137	0.34	7.11	-138.1	0.00		
1109		PUMP OFF							
1110		START SAMPLE COLLECTION							
1136		SAMPLE COMPLETED							
						2 L IPEC			
						0.5 L IPEC			
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sunde turbidity meter	LeMotte <sup>6</sup> 2020 / 2530-1701

NOTES AND OBSERVATIONS:

WELL ID: MW 32-85

SAMPLE ID: 024

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny 70's

PROJECT NO: 01.0017869.92  
 DATE: 9/9/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
79.3 to 92.8

TOTAL VOLUME PURGED: 0.70 gal

SAMPLING PORT  
85

5

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

WATER QUALITY: 2nd MID QUARTER

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pres (psi)
1242	0		PUMP	ON				10   12	49
1256	0.01	20.94	1.611	0.80	7.06	-88.2	—	8   14	39
1302	0.03	21.18	1.615	0.65	7.05	-75.0	0.87		
1309	0.07	21.36	1.614	0.76	7.06	-68.7	0.49		
1314	0.10	21.55	1.615	0.75	7.05	-60.5	1.21		
1320	0.15	21.91	1.616	0.71	7.06	-51.3	0.64		
1325	0.20	22.11	1.616	0.65	7.08	-45.2	0.15		
1331	0.24	22.18	1.616	0.59	7.09	-34.2	0.11		
1338	0.30	22.16	1.617	0.54	7.11	-27.3	0.26		
1343	0.32	22.08	1.617	0.52	7.11	-19.1	0.04		
1348	0.35	21.99	1.616	0.49	7.12	-7.0	0.06		
1353	0.40	22.00	1.615	0.46	7.13	0.0	0.01		
1358	0.44	22.06	1.614	0.45	7.13	+8.2	0.00		
1403	0.50	22.04	1.614	0.45	7.13	10.1	0.00		
1408	0.54	22.04	1.614	0.44	7.13	11.4	0.00	↓	↓
1410			PUMP OFF						
1411			START SAMPLE COLLECTION						
1529			SAMPLE COMPLETED : 2 L IPEC						
			0.5 L IPEC						
			PUMP OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	LaMotte 2020 / 2530-1701

NOTES AND OBSERVATIONS:

WELL ID: MW 32 . 59

SAMPLE ID: 021

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: Sunny 70's

PROJECT NO: 01.0017869.92  
 DATE: 9/9/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
28.3 to 61.3

TOTAL VOLUME PURGED: 2.55 gal

SAMPLING PORT  
59

6

PURGE RATE: variable (gal/min)

PURGE METHOD: Double Valve Pump

WATER QUALITY: 2nd MID QUARTER

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Press (psi)
1242	0		PUMP	ON				8   8	26
1256	0.10	21.00	0.533	3.71	6.83	43.9	—	8   14	39
1302	0.30	20.32	0.658	6.19	7.22	36.2	0.00		
1309	0.70	20.28	0.669	6.36	7.36	38.6	0.00		
1314	1.0	20.38	0.672	6.44	7.44	41.9	0.00		
1320	1.30	20.56	0.674	6.54	7.50	44.0	0.00		
1325	1.55	20.42	0.674	6.61	7.53	46.6	0.00		
1331	1.80	20.41	0.673	6.77	7.55	49.0	0.00		
1338	2.10	20.37	0.673	6.85	7.57	51.5	0.00		
1343	2.40	20.3	0.673	6.78	7.58	52.3	0.00	↓	↓
1345		PUMP	OFF						
1346		START	SAMPLE COLLECTION						
1357		SAMPLE	COMPLETED : 2 L IPEC						
			0.5 L IPEC						
		PUMP	OFF						

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 556J Sonde	2
turbidity meter	La Motte 2020/2530-1701

NOTES AND OBSERVATIONS:









WELL ID: MW 31-49

SAMPLE ID: 02B

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: M. Sunny 80's

PROJECT NO: 01.0017869.92  
 DATE: 9/7/10  
 SAMPLER(S): M. BRITOS

SAMPLING INTERVAL (depth in ft below top of casing)  
34.8 to 49.3

TOTAL VOLUME PURGED: 1.95 gal

SAMPLING PORT  
49 2<sup>nd</sup> MID QUARTER

PURGE RATE: variable (gal/min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
1212	0	PUMP ON						9/10	20
1229		PUMP OFF		YSI #3 not working					
1233		PUMP ON		" replaced with YSI #6					
1239	0.1	22.40	1.390	5.18	7.10	70.4		8/10	28
1245	0.35	22.02	1.413	4.12	7.11	72.3	0.00		
1252	0.60	21.80	1.416	3.76	7.10	72.0	0.00		
1300	0.80	21.61	1.415	3.58	7.12	73.1	0.00		
1310	1.15	21.50	1.415	3.63	7.15	74.3	0.00		
1320	1.50	21.35	1.416	3.65	7.16	75.4	0.00		
1325	1.70	21.40	1.416	3.62	7.16	75.8	0.00		
1330	1.80	21.33	1.418	3.67	7.17	75.9	0.00		
1333		START SAMPLE COLLECTION							
1349		SAMPLE COMPLETED: 2 L IPEC							
		0.5 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 556J Sonde turbidity meter	1 Lg Mott 2020/2533-1701

NOTES AND OBSERVATIONS:

WELL ID: MW 31-63

SAMPLE ID: 027

### GZA GeoEnvironmental of New York Waterloo Sampling Data Sheet

CLIENT: Entergy - IPEC  
 SITE: Buchanan, NY  
 WEATHER: M. Sunny 80's

PROJECT NO: 01.0017869.92  
 DATE: 9/7/10  
 SAMPLER(S): M-BL TDS

SAMPLING INTERVAL (depth in ft below top of casing)  
55.8 to 63.8

TOTAL VOLUME PURGED: 0.80 gal

SAMPLING PORT  
63 2<sup>nd</sup> MID QUARTER

PURGE RATE: variable (gal / min)  
 PURGE METHOD: Double Valve Pump

**WATER QUALITY:**

Time	Purged Volume (gal)	Temp (°C)	Specific Conductivity (S/cm)	Dissolved Oxygen (g/l)	pH (SU)	ORP	Turbidity (NTU)	Drive/Vent Cycle (seconds)	Drive Pressur (psi)
1212	0	PUMP ON						9/10	20
1229		PUMP OFF		YSI #3 not working					
1233		PUMP ON		" replaced with YSI #6					
1239	0.05	26.81	1.250	0.61	7.09	-44.6	-	8/10	28
1245	0.10	26.86	1.250	0.58	7.13	-42.5	0.00		
1252	0.15	26.77	1.219	0.93	7.15	-31.3	0.00		
1300	0.20	26.36	1.143	1.54	7.17	-9.8	0.00		
1310	0.30	26.11	1.089	2.23	7.20	+7.1	0.00		
1320	0.35	26.03	1.074	2.44	7.21	11.8	0.00		
1325	0.40	26.02	1.076	2.46	7.22	12.8	0.00		
1330	0.45	26.06	1.077	2.45	7.22	14.1	0.00		
1337	0.50	25.98	1.095	2.49	7.16	26.6	0.00		
1342	0.55	25.97	1.107	2.48	7.19	23.3	0.00		
1347	0.58	25.89	1.125	2.49	7.20	20.7	0.00		
1354	0.60	25.87	1.136	2.45	7.22	19.6	0.00		
1359	0.65	25.88	1.142	2.48	7.21	18.9	0.00		
1401		START SAMPLING COLLECTION							
1528		SAMPLE COMPLETED: 2 L IPEC 0.5 L IPEC							
		PUMP OFF							

Equipment Used	Equipment Identification #
YSI 556 MPS Reader and 5563 Sonde turbidity meter	5 Lu Motte 2020/2533-1701

NOTES AND OBSERVATIONS:



## APPENDIX F DOSE CALCULATIONS



Facility Groundwater Flux Calculation

Site Indian Point  
Job No. 17869.02

Prepared By: JAS  
Reviewed By: mb

Parameter Values:

year  
2010

Totals						
Total Catchment Zone (ft <sup>2</sup> )		Total Improved Zone (ft <sup>2</sup> )		Recharge (ft/yr)	Precipitation (ft/yr)	
3,969,765		1,432,972		0.61	3.10	
Surface Area						
Northern Clean Zone Improved (ft <sup>2</sup> )	Unit 2 North Improved Zone (ft <sup>2</sup> )	Unit 1/2 Improved Zone (ft <sup>2</sup> )	Unit 3 North Improved Zone (ft <sup>2</sup> )	Unit 3 South Improved Zone (ft <sup>2</sup> )	Southern Clean Improved Zone (ft <sup>2</sup> )	
0	148,214	433,904	316,210	321,290	213,354	
Northern Clean Unimproved Zone (ft <sup>2</sup> )	Unit 2 North Unimproved Zone (ft <sup>2</sup> )	Unit 1/2 Unimproved Zone (ft <sup>2</sup> )	Unit 3 North Unimproved Zone (ft <sup>2</sup> )	Unit 3 South Unimproved Zone (ft <sup>2</sup> )	Southern Clean Zone Unimproved (ft <sup>2</sup> )	
106,429	204,317	438,221	323,116	268,862	585,600	
Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	Discounted Area Within Zone	
50,265	0	291,166	106,718	17,730	144,347	
Northern Clean Zone Catchment (ft <sup>2</sup> )	Unit 2 North Catchment Zone (ft <sup>2</sup> )	Unit 1/2 Catchment Zone (ft <sup>2</sup> )	Unit 3 North Catchment Zone (ft <sup>2</sup> )	Unit 3 South Zone (ft <sup>2</sup> )	Southern Clean Zone (ft <sup>2</sup> )	
156,694	352,531	1,163,311	746,044	607,882	943,302	
Activity (pCi/L)						
Groundwater						
Upper Zone Before Canal	Northern Clean Zone Catchment	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South Zone	Southern Clean Zone
150	150	337	4,016	399	678	159
Lower Zone Before Canal	150	239	3,376	1,307	545	147
Upper Zone After Canal	150	249	3,226	306	678	159
Lower Zone After Canal	150	478	942	500	545	147
Stormwater Discharging to Canal (pCi/L)						
Storm Water for Northern Clean Zone	Storm Water for Unit 2 North	Storm Water for Unit 1/2	Storm Water for Unit 3 North	Storm Water for Unit 3 South	Storm Water for Southern Clean Zone	
NA	1,531	NA	0	1,172	283	
	Avg MH-4a		Avg CB-14 and CB-34	Avg U3-CB-B8	Avg D1, C3, E6, & E10	
Stormwater Discharging to River (pCi/L)						
Storm Water for Northern Clean Zone	Storm Water for Unit 2 North	Storm Water for Unit 1/2	Storm Water for Unit 3 North	Storm Water for Unit 3 South	Storm Water for Southern Clean Zone	
NA	129	0	0	NA	201	
	Avg MH-1 and MH-12	Avg MH-14	Avg CB-15		Avg E13, CB-C2	

Potential Water Received by Storm Drain System

= (Improved Area) x Precipitation

Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone	Units
0	459,463	1,345,103	980,252	995,993	661,399	ft <sup>3</sup> /yr
0	1,259	3,635	2,686	2,729	1,812	ft <sup>3</sup> /day
0.00	6.54	19.14	13.95	14.18	9.41	GPM
0	13,010,545	38,089,071	27,757,643	28,203,511	18,728,730	L/Yr

The total amount of water available to be received by the storm system is computed as the combined area of buildings and paved areas in the catchment multiplied by the annual precipitation rate. Note this conservatively assumes that the amount of water lost to the atmosphere or other sinks after precipitation has fallen on paved or built up surfaces is zero.

Water Directly Recharged to Aquifer from Precipitation

= Unimproved Area x Recharge

Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone	Units
85,782	164,680	353,206	260,431	216,703	471,994	ft <sup>3</sup> /yr
235	451	968	714	594	1,293	ft <sup>3</sup> /day
1.22	2.34	5.03	3.71	3.08	6.72	GPM
2,429,073	4,663,211	10,001,688	7,374,588	6,136,349	13,365,375	L/Yr

Note that this calculation reflects recharge to the aquifer in non-paved areas. The Recharge value listed above and used in this calculation reflects only that portion of precipitation that actually recharges the aquifer.



Facility Groundwater Flux Calculation

Site Indian Point  
Job No. 17869.02

Prepared By: JAS  
Reviewed By: mib

Water Recharged to Aquifer (Direct Recharge Plus Storm Water Leakage Minus Building Drain Removal)

= (Direct Recharge + X% Water Received by Storm System) - (Y% x Water Removed by Building Drains)

**Total Water Discharged to Aquifer**

Upper and Lower Zone	[Northern Clean Area Catchment + (0% Storm Drain Water)] <sup>1</sup>	[Unit 2 North + (50% Storm Drain Water)]-[5gpm]	[Unit 1/2 Area Catchment + (30% Storm Drain Water)]-[7.5 gpm]	[Unit 3 North Area Catchment + (60% Storm Drain Water)]-[7.5gpm]	[Unit 3 South Area + (10% Storm Drain Water)]	[Southern Clean Zone Area + (40% Storm Drain Water)]	Units
		85,782	43,099	229,768	321,614	316,303	736,553
	235	118	630	881	867	2,018	ft <sup>3</sup> /day
	1.22	0.61	3.27	4.58	4.50	10.48	GPM
	2,429,073	1,220,421	6,506,317	9,107,080	8,956,700	20,356,867	L/Yr

<sup>1</sup> There are no improved surfaces in Northern Clean Zone.

Groundwater Discharged to Canal

=Water Recharged to Aquifer x X% flowing to Canal

Upper and Lower Zone	Northern Clean Area Catchment x 0%	Unit 2 North x 15.2%	Unit 1/2 Area Catchment 24.2%	Unit 3 North Area Catchment x 22.9%	Unit 3 South Area x68.4%	Southern Clean Zone Area x 0%	Units
		0	6,551	55,604	73,649	216,351	0
	0	18	152	202	593	0	ft <sup>3</sup> /day
	0.00	0.09	0.79	1.05	3.08	0.00	GPM
	0	185,504	1,574,529	2,085,521	6,126,383	0	L/Yr

Groundwater Discharged to River

=Water Recharged to Aquifer x X% flowing to River x Y% Flowing in Appropriate Vertical Zone

Upper Zone	Northern Clean Area Catchment x 100% x 59.3%	Unit 2 North x 84.8% x 15.1%	Unit 1/2 Area Catchment x 75.8% x 11.7%	Unit 3 North Area Catchment x 77.1% x 47.9%	Unit 3 South Area x 31.6% x 31.3%	Southern Clean Zone Area x 100% x 55.2%	Units
		50,869	5,519	20,377	118,775	31,285	406,577
	139	15	56	325	86	1,114	ft <sup>3</sup> /day
	0.72	0.08	0.29	1.69	0.45	5.79	GPM
	1,440,440	156,273	577,019	3,363,327	885,889	11,512,991	L/Yr
Lower Zone	Northern Clean Area Catchment x 100% x 40.7%	Unit 2 North x 84.8% x 84.9%	Unit 1/2 Area Catchment 75.8% x 88.3%	Unit 3 North Area Catchment x 77.1% x 52.1%	Unit 3 South Area x 31.6% x 68.7%	Southern Clean Zone Area x 100% x 44.8%	Units
		34,913	31,029	153,787	129,189	68,667	329,976
	96	85	421	354	188	904	ft <sup>3</sup> /day
	0.50	0.44	2.19	1.84	0.96	4.70	GPM
	988,633	878,645	4,354,769	3,658,232	1,944,428	9,343,877	L/Yr

Water Remaining in Storm Drains and Discharged to Canal

=Storm Drain Water x X% Not Leaking to Groundwater and Not Discharging to River

Northern Clean Area Catchment (0% Storm Drain Water)	Unit 2 North (45% Unit 2 North and 30% of Unit 1/2 Storm Drain Water). Plus 5 gpm (351k cf/yr) from U2 footing drain.	Unit 1/2 Area Catchment (0% Storm Drain Water)	Unit 3 North Area Catchment (3% Unit 3 North Storm Drain Water)	Unit 3 South Area (3% Unit 3 North and 42% Unit 3 South Storm Drain Water)	Southern Clean Zone Area (30% Unit 1/2, 27% Unit 3 North, 43% Unit 3 South, and 55% Southern Clean Zone Storm Drain Water)	Units
0	961,289	0	29,408	447,727	1,460,247	ft <sup>3</sup> /yr
0	2,634	0	81	1,227	4,001	ft <sup>3</sup> /day
0	13.68	0.00	0.42	6.37	20.78	GPM
0	27,221,998	0	832,729	12,678,204	41,349,597	L/Yr

Water Remaining in Storm Drains and Discharged to River

Northern Clean Area Catchment (0% Storm Drain Water)	Unit 2 North (5% Storm Drain Water)	Unit 1/2 Area Catchment (10% Storm Drain Water)	Unit 3 North Area Catchment (7% Storm Drain Water)	Unit 3 South Area (5% Storm Drain Water)	Southern Clean Zone Area (5% Storm Drain Water)	Units
0	22,973	134,510	68,618	49,800	33,070	ft <sup>3</sup> /yr
0	63	369	188	136	91	ft <sup>3</sup> /day
0	0.33	1.91	0.98	0.71	0.47	GPM
0	650,527	3,808,907	1,943,035	1,410,176	936,437	L/Yr





Facility Groundwater Flux Calculation

Site Indian Point  
Job No. 17869.92

Prepared By: JAS  
Reviewed By: mb

Flux Calculations

Conceptual Model: Migration Pathway Summary

	Northern Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	Southern Clean Zone
GW	100% Upper and Lower Zone To River	84.8% Upper Zone and Lower Zone Flow To River. 15.2% Upper Zone and Lower Zone Flow to Canal	75.8% Upper Zone and Lower Zone To River. 24.2% Upper Zone and Lower Zone to Canal	77.1% Upper Zone and Lower Zone To River. 22.9% Upper Zone and Lower Zone to Canal	31.8% Upper Zone and Lower Zone To River. 68.4% Upper Zone and Lower Zone to Canal	100% Upper and Lower Zone To River
SW	NA	To Canal (Storm Water Considered Clean; Estimated at 5.5 GPM) and To River (5% Storm Water)	To Canal (60% Storm Water) and To River (10% Storm Water)	To Canal (33% Storm Water) and To River (7% Storm Water)	To Canal (85% Storm Water) and To River (5% Storm Water)	To Canal (55% Storm Water) and To River (5% Storm Water)

Flux (pCi/Yr)

	North Clean Area	Unit 2 North	Unit 1/2	Unit 3 North	Unit 3 South	South Clean Zone	Total
GW to River-Upper Zone	2.16E+08	3.90E+07	1.86E+09	1.03E+09	6.01E+08	1.83E+09	5.57E+09
GW to River-Lower Zone	1.48E+08	4.20E+08	4.10E+09	1.83E+09	1.06E+09	1.37E+09	8.93E+09
GW to Canal	0.00E+00	6.25E+07	6.33E+09	8.31E+08	4.15E+09	0.00E+00	1.14E+10
SW to Canal	NA	4.17E+10	0.00E+00	0.00E+00	1.49E+10	1.17E+10	6.82E+10
SW to River	NA	8.40E+07	0.00E+00	0.00E+00	0.00E+00	1.89E+08	2.73E+08

Curies/Yr ==> 0.09

Notes:

The recharge rate used herein, 28% of precipitation (~10 in/yr), is within the range of values discussed in the USGS modeling report! The reported recharge ranged from 3.6 inches/year to 7.5 inches/year for a till to 20 inches per year for coarse grained glacially stratified deposits. A yearly rolling average precipitation value measured at the Facility meteorological station is also used in the computations. The catchment area was defined using an AutoCAD topo map for the Site and surrounding area. The catchment was defined by starting at the area marked "line of water grant" and tracking east, away from the River, to define portions of the land surface contributing water to the selected discharge zone. Calculations assume that run-off or overland flow in unimproved areas of the Site is negligible, there are no changes in storage and the Hudson River is a gaining stream.

1. USGS. Water Use, Ground-Water Recharge and Availability, and Quality of Water in the Greenwich Area, Fairfield County, Connecticut and Westchester County, New York, 2000-2002



## **APPENDIX G UNIT 2 TRITIUM PLUME TREND ANALYSES**

**TABLE G1  
MANN-KENDALL TREND EVALUATION SUMMARY  
TRITIUM IN GROUNDWATER NEAR UNIT 2  
INDIAN POINT ENERGY CENTER  
BUCHANAN, NY**

Well ID	Number of Data Points	Number of Times below MDC	Minimum Tritium Activity (pCi/L)	Maximum Tritium Activity (pCi/L)	Mann-Kendall Statistic (S)	Normalized Test Statistic (Z)	Probability	Trend at 95% Level of Significance
MW-30-69	39	0	7.36E+04	6.01E+05	-164	-1.97	0.976	decreasing
MW-30-84	26	0	3.78E+03	1.25E+04	92	2.01	0.978	increasing
MW-31-49	38	0	2.98E+02	1.04E+05	63	0.78	0.782	no trend
MW-31-63	26	0	5.00E+03	7.35E+04	124	2.71	0.997	increasing
MW-31-85	26	0	3.17E+02	2.25E+04	128	2.80	0.997	increasing
MW-32-59	25	0	4.13E+02	1.55E+05	54	1.24	0.892	no trend
MW-32-85	24	0	5.42E+03	1.44E+04	94	2.31	0.989	increasing
MW-32-149	21	0	1.99E+02	1.05E+04	-2	-0.03	0.512	no trend
MW-32-173	19	0	4.31E+02	5.89E+03	-9	-0.28	0.610	no trend
MW-32-190	23	0	1.58E+02	1.13E+04	-175	-4.60	1.000	decreasing
MW-33	26	0	3.69E+03	2.64E+05	-167	-3.66	1.000	decreasing
MW-35	20	0	1.04E+03	1.19E+05	-88	-2.82	0.998	decreasing
MW-36-24	17	2	1.54E+02	3.42E+04	16	0.62	0.732	no trend
MW-36-41	12	0	6.11E+03	5.52E+04	-33	-2.19	0.986	decreasing
MW-36-52	17	0	5.97E+03	2.68E+04	-94	-3.83	1.000	decreasing
MW-37-22	19	0	2.26E+03	3.49E+04	-55	-1.89	0.971	decreasing
MW-37-32	19	0	2.49E+03	3.01E+04	-61	-2.10	0.982	decreasing
MW-37-40	18	0	4.22E+03	1.70E+04	-93	-3.48	1.000	decreasing
MW-37-57	19	0	4.05E+03	4.48E+04	-87	-3.01	0.999	decreasing
MW-42-49	19	0	1.12E+03	7.22E+04	-45	-1.54	0.938	no trend
MW-42-78	14	0	3.46E+02	1.28E+03	-17	-0.88	0.809	no trend
MW-49-26	21	0	2.82E+03	1.54E+04	-174	-5.22	1.000	decreasing
MW-49-42	21	0	2.20E+03	1.13E+04	-164	-4.92	1.000	decreasing
MW-49-65	21	0	1.26E+03	5.76E+03	-147	-4.41	1.000	decreasing
MW-50-42	22	4	1.01E+02	9.75E+03	-57	-1.58	0.943	no trend
MW-50-66	26	0	2.08E+03	1.08E+04	-201	-4.41	1.000	decreasing
MW-53-82	16	0	4.54E+02	1.32E+04	-2	-0.05	0.518	no trend
MW-53-120	19	0	3.81E+03	9.61E+03	-111	-3.85	1.000	decreasing
MW-55-24	15	0	7.82E+02	3.08E+03	-18	-0.84	0.800	no trend
MW-55-35	14	0	8.53E+02	9.04E+03	-35	-1.86	0.969	decreasing
MW-55-54	15	0	5.47E+03	1.31E+04	-27	-1.29	0.901	no trend
MW-111	35	0	6.81E+03	5.78E+05	-264	-3.74	1.000	decreasing
<b>DOWNGRADIENT WELLS</b>								
MW-66-21	14	0	8.28E+01	3.57E+03	-7	-0.33	0.629	no trend
MW-66-36	13	0	3.05E+03	9.10E+03	-62	-3.72	1.000	decreasing
MW-67-39	12	0	2.55E+03	5.07E+03	-36	-2.40	0.992	decreasing
MW-67-105	13	0	1.26E+03	2.93E+03	-46	-2.75	0.997	decreasing
MW-67-173	13	0	6.72E+02	1.05E+03	-41	-2.44	0.993	decreasing
MW-67-219	12	0	9.22E+02	1.44E+03	-4	-0.21	0.581	no trend
MW-67-276	12	0	6.79E+02	1.18E+03	-7	-0.41	0.660	no trend
MW-67-323	12	0	3.13E+02	1.29E+03	20	1.30	0.904	no trend
MW-67-340	12	0	3.69E+02	6.69E+02	28	1.85	0.968	increasing

Notes: Calculations based on Mann-Kendall trend evaluations as presented in U.S. EPA Practical Methods for Data Analysis, U.S. EPA QA/G-9 QA00 UPDATE, July 2000, Section 4.3.4

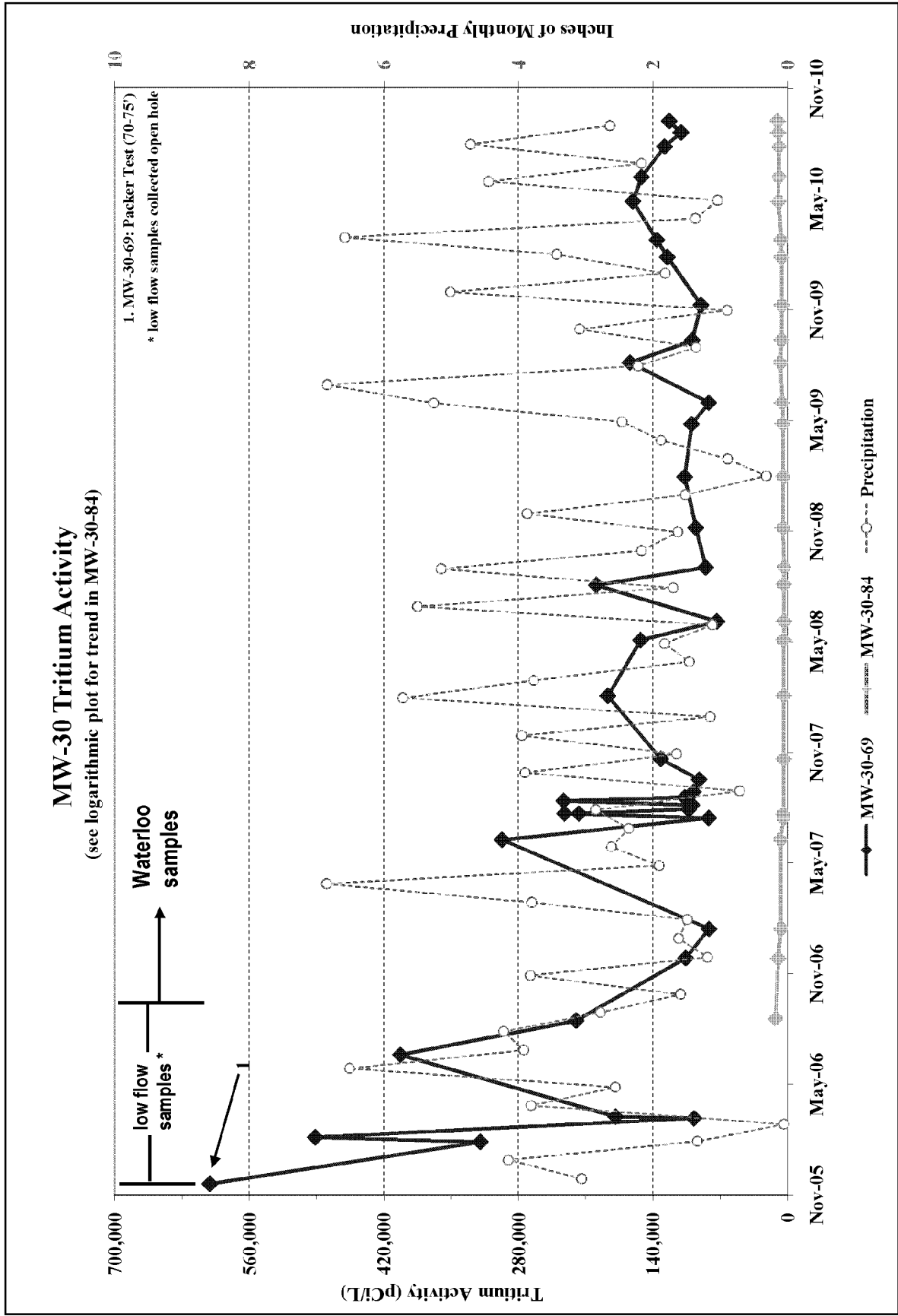
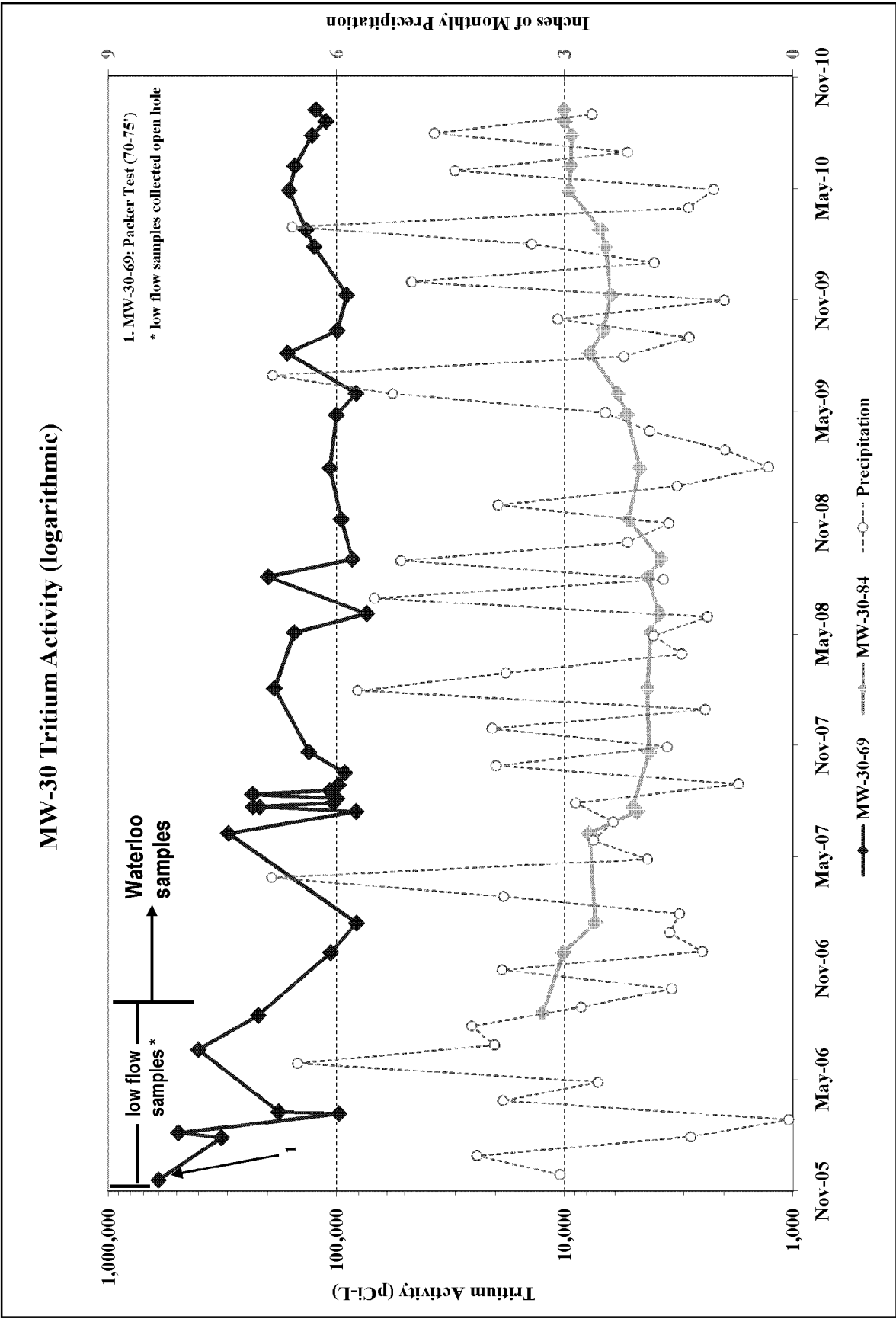


FIGURE G1



**FIGURE G1a**

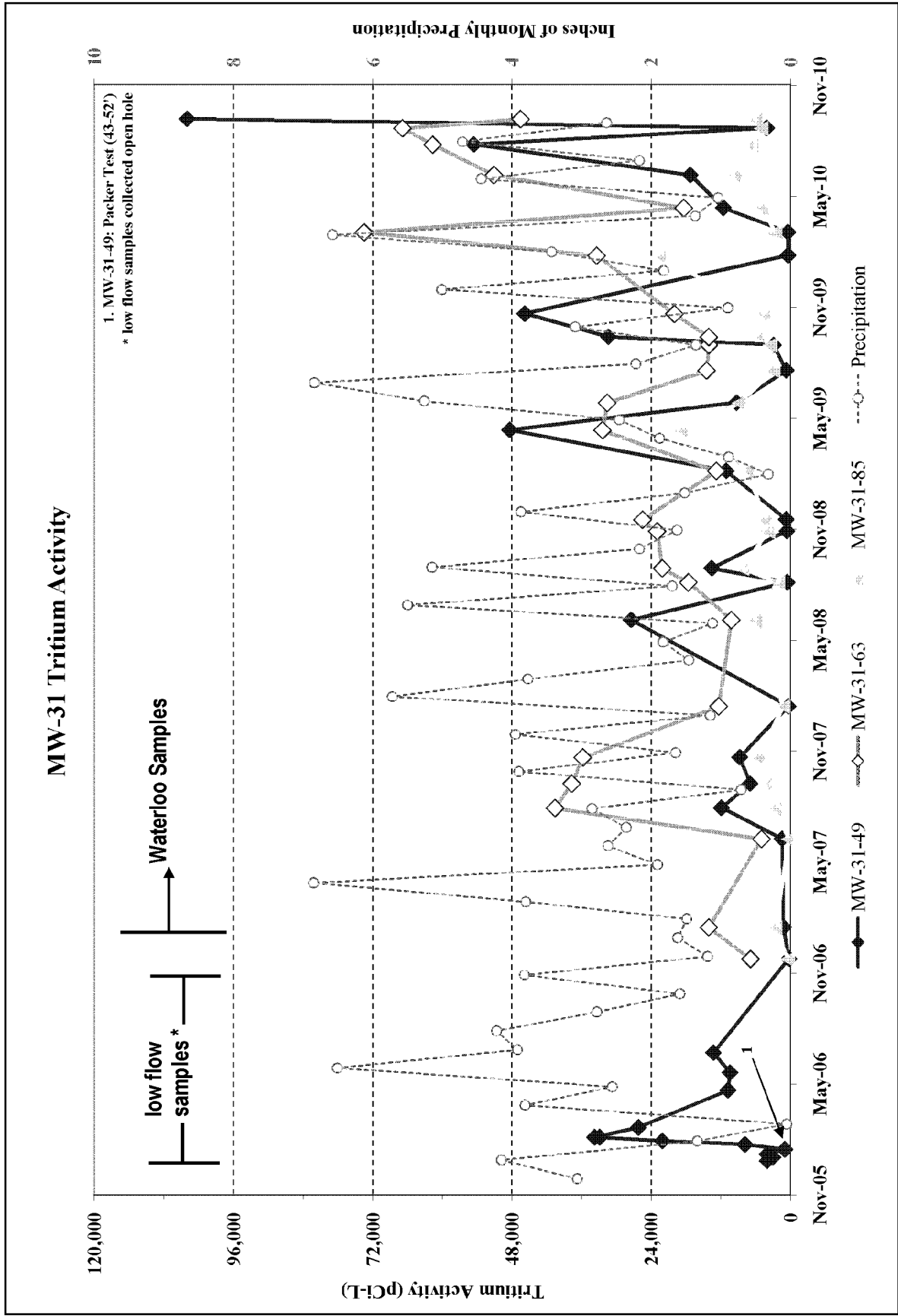
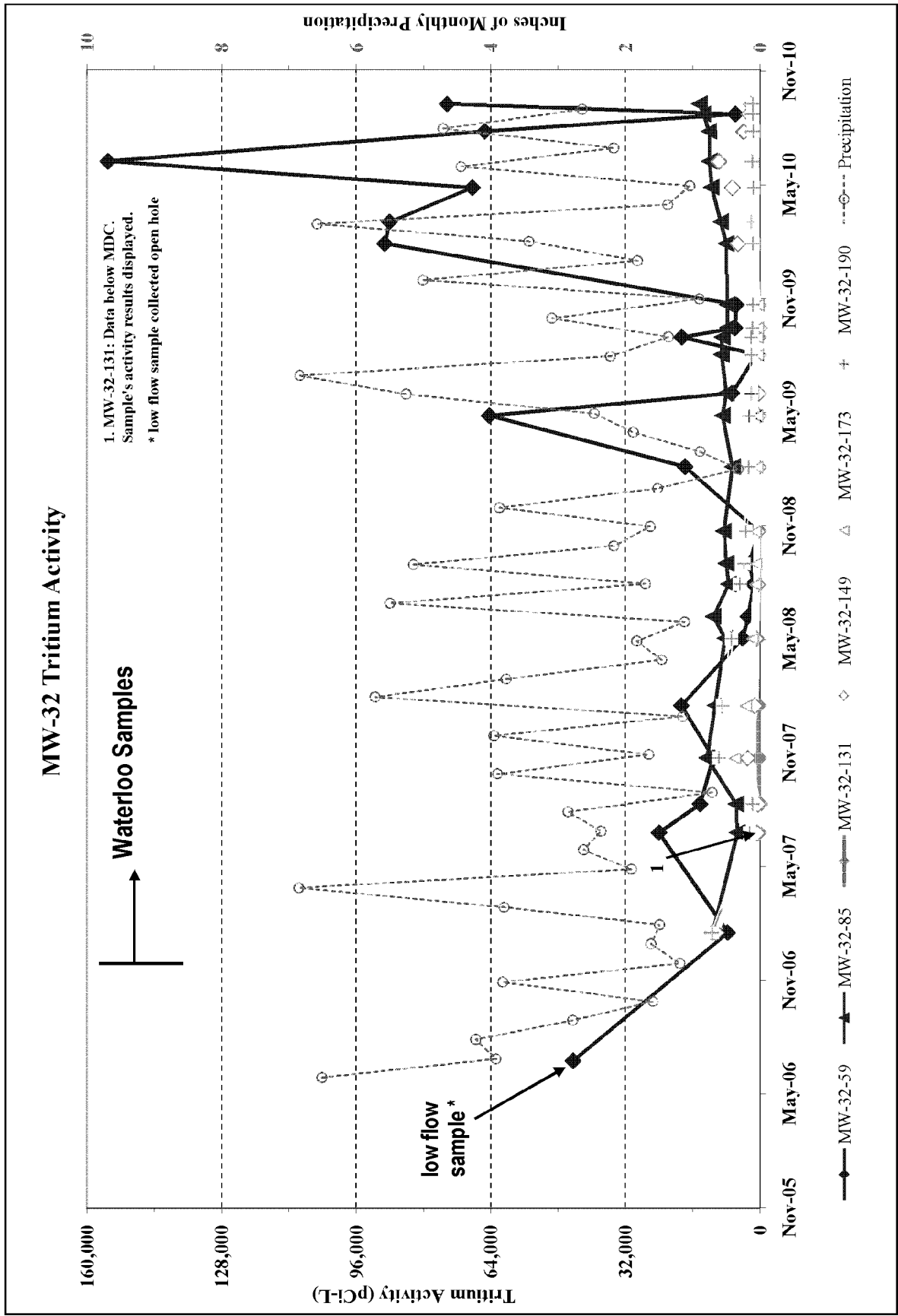


FIGURE G2



**FIGURE G3**

# MW-33 Tritium Activity

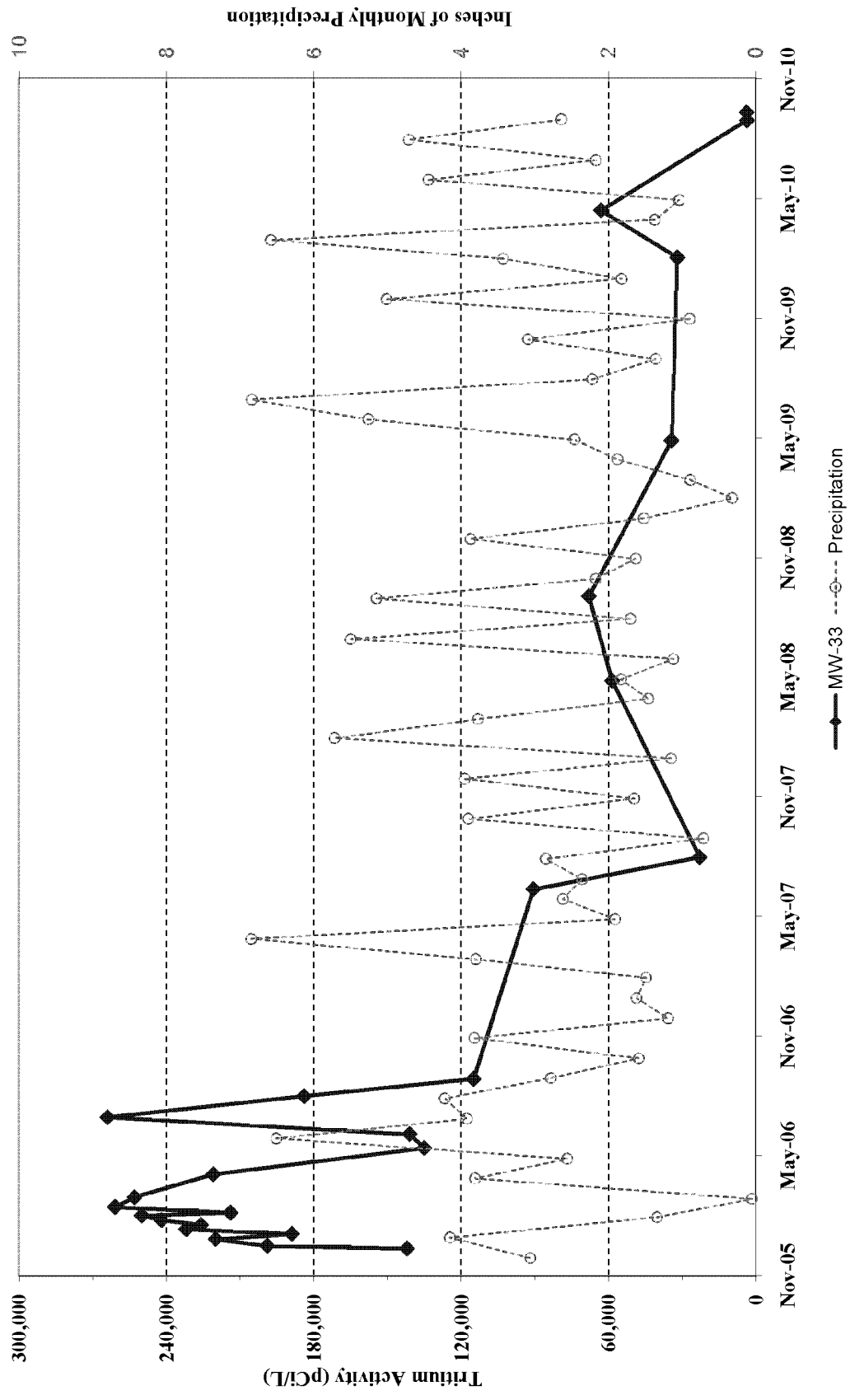


FIGURE G4



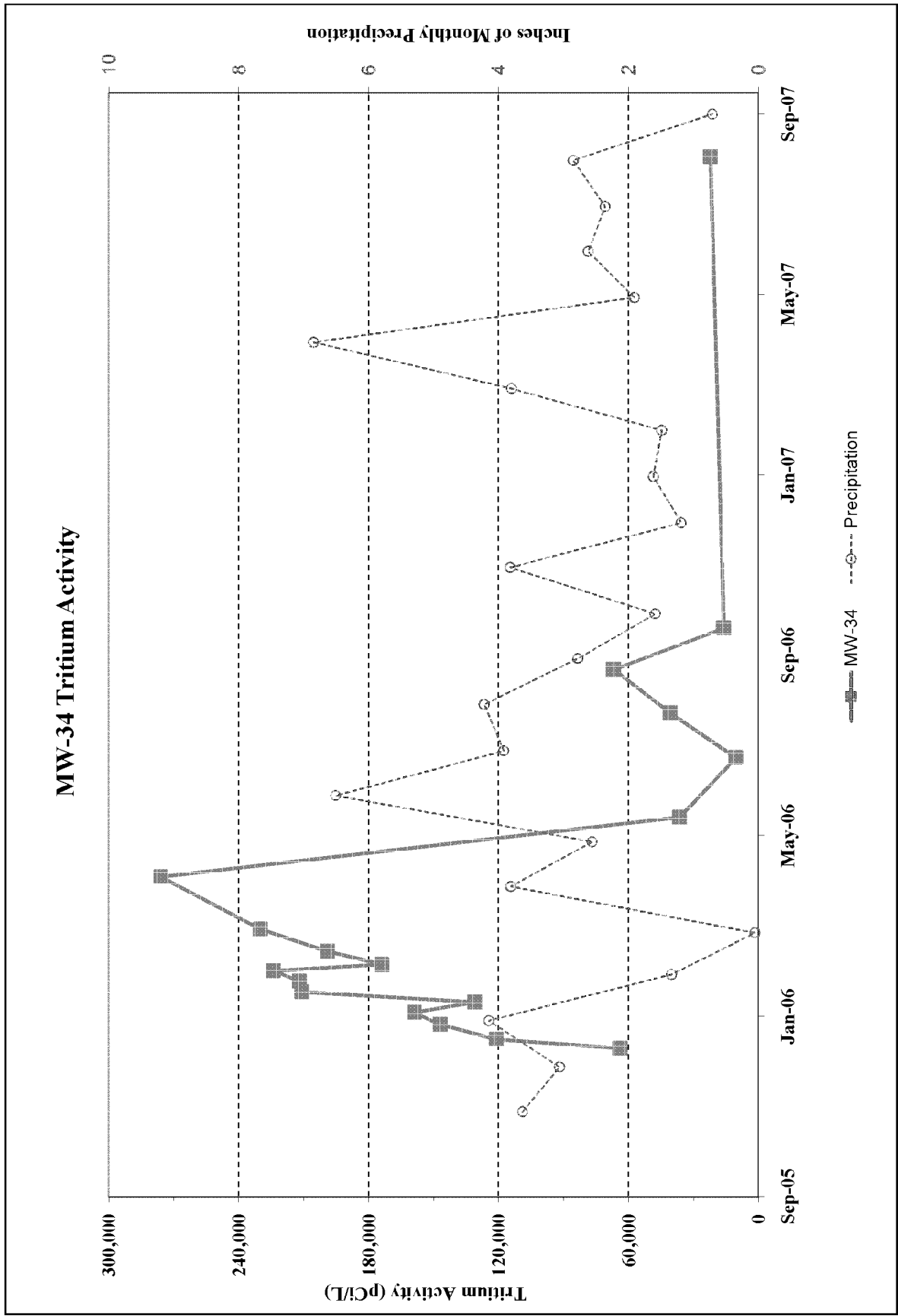


FIGURE G5

# MW-35 Tritium Activity

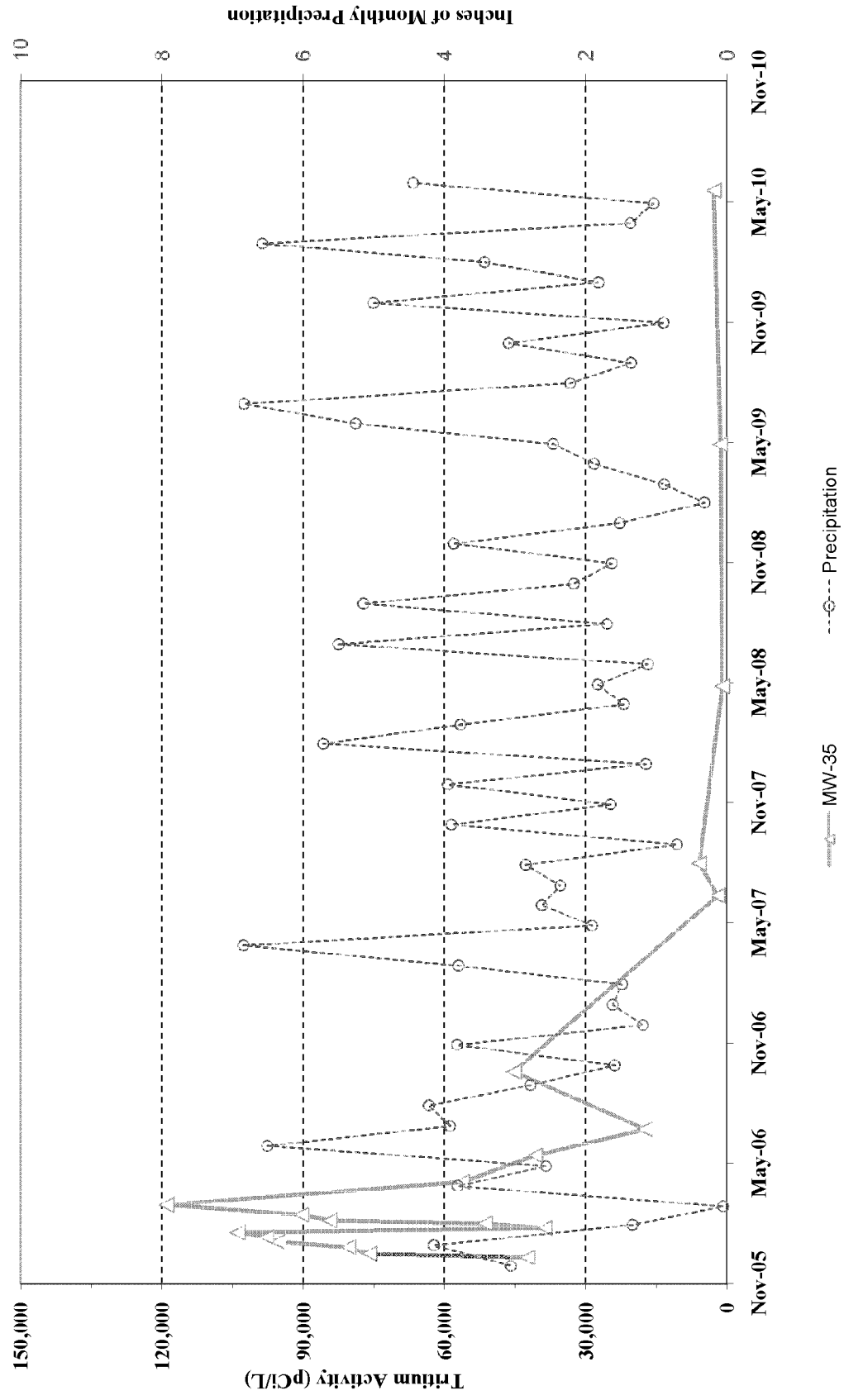


FIGURE G6

# MW-36 Tritium Activity

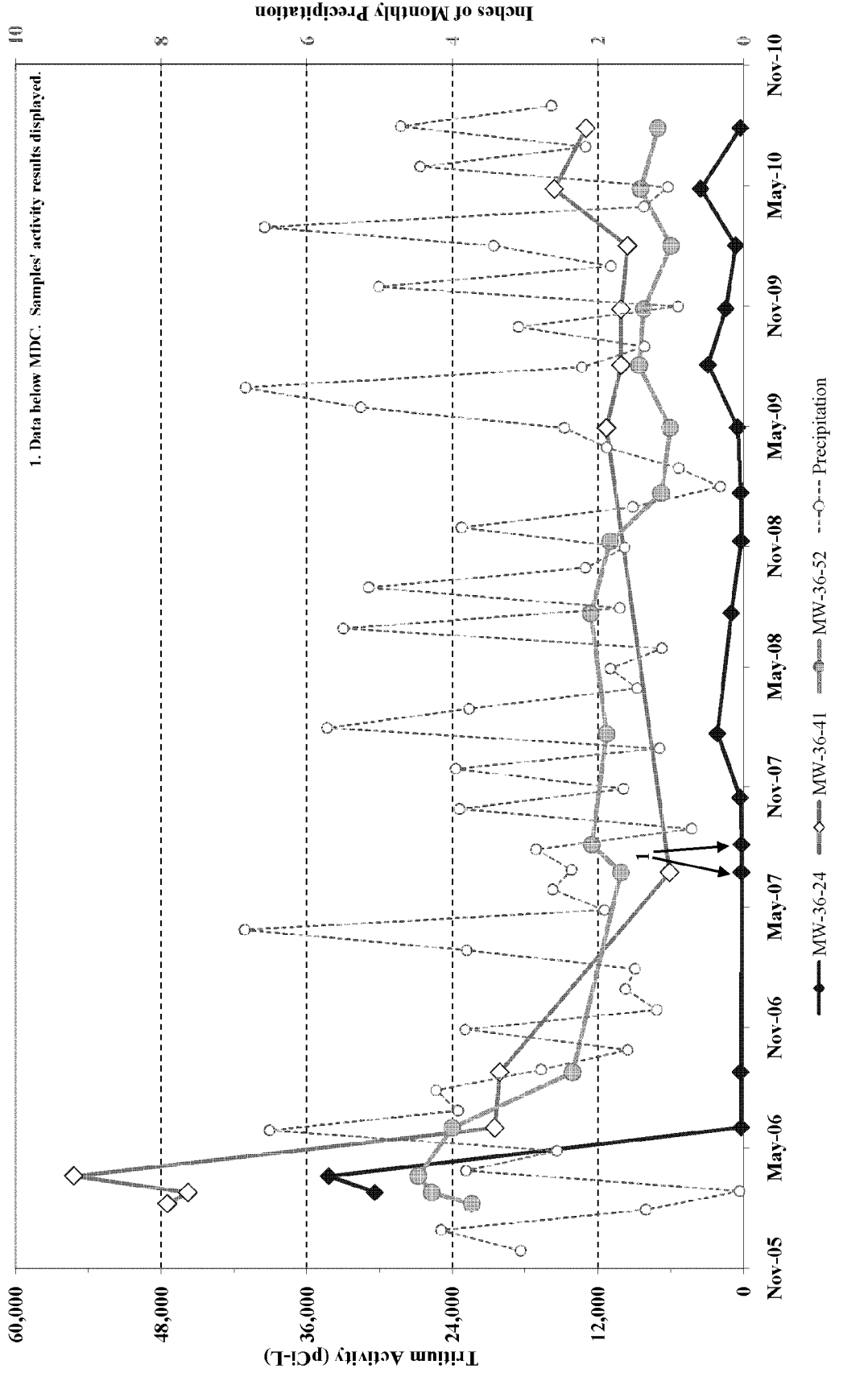


FIGURE G7

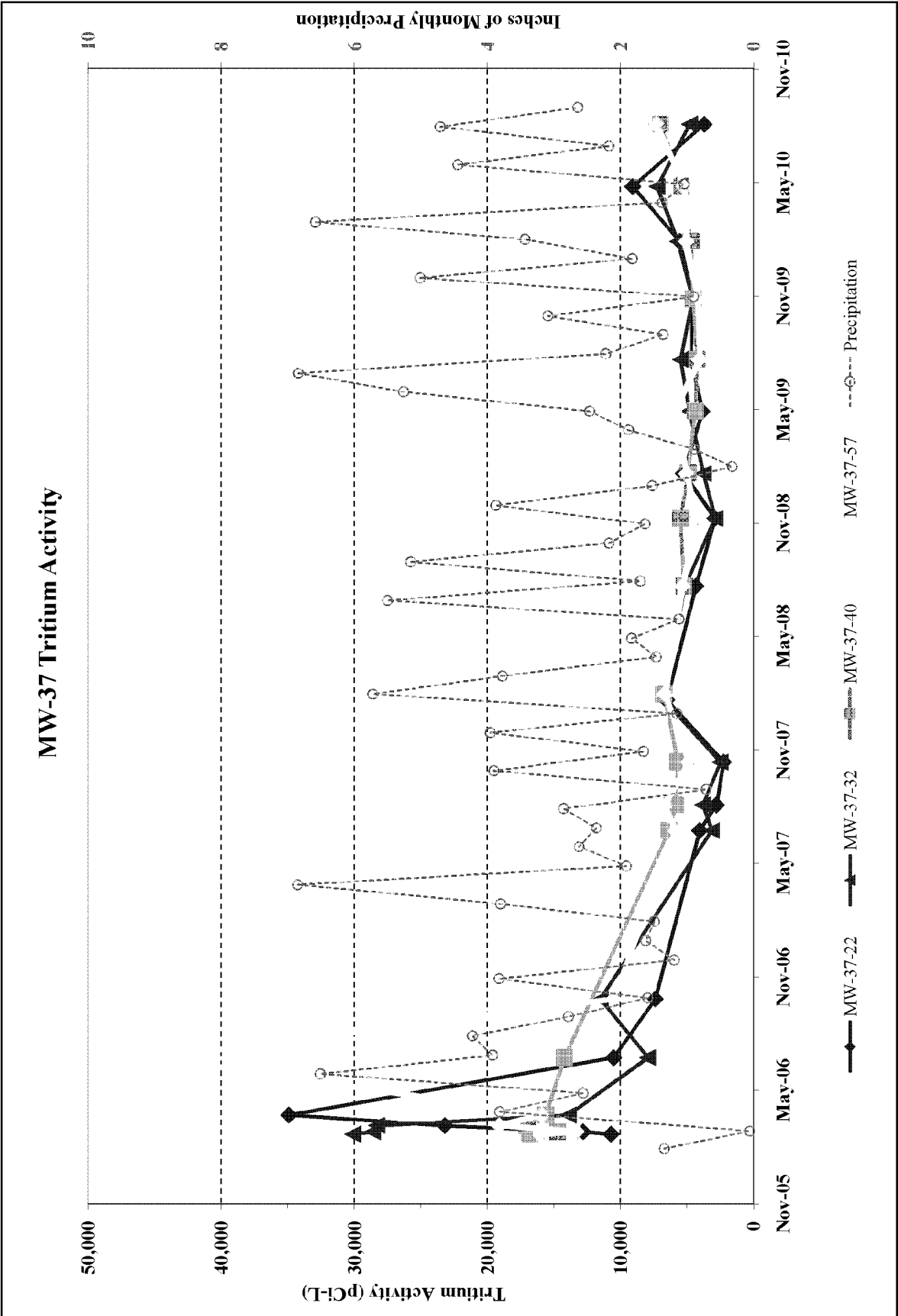


FIGURE G8

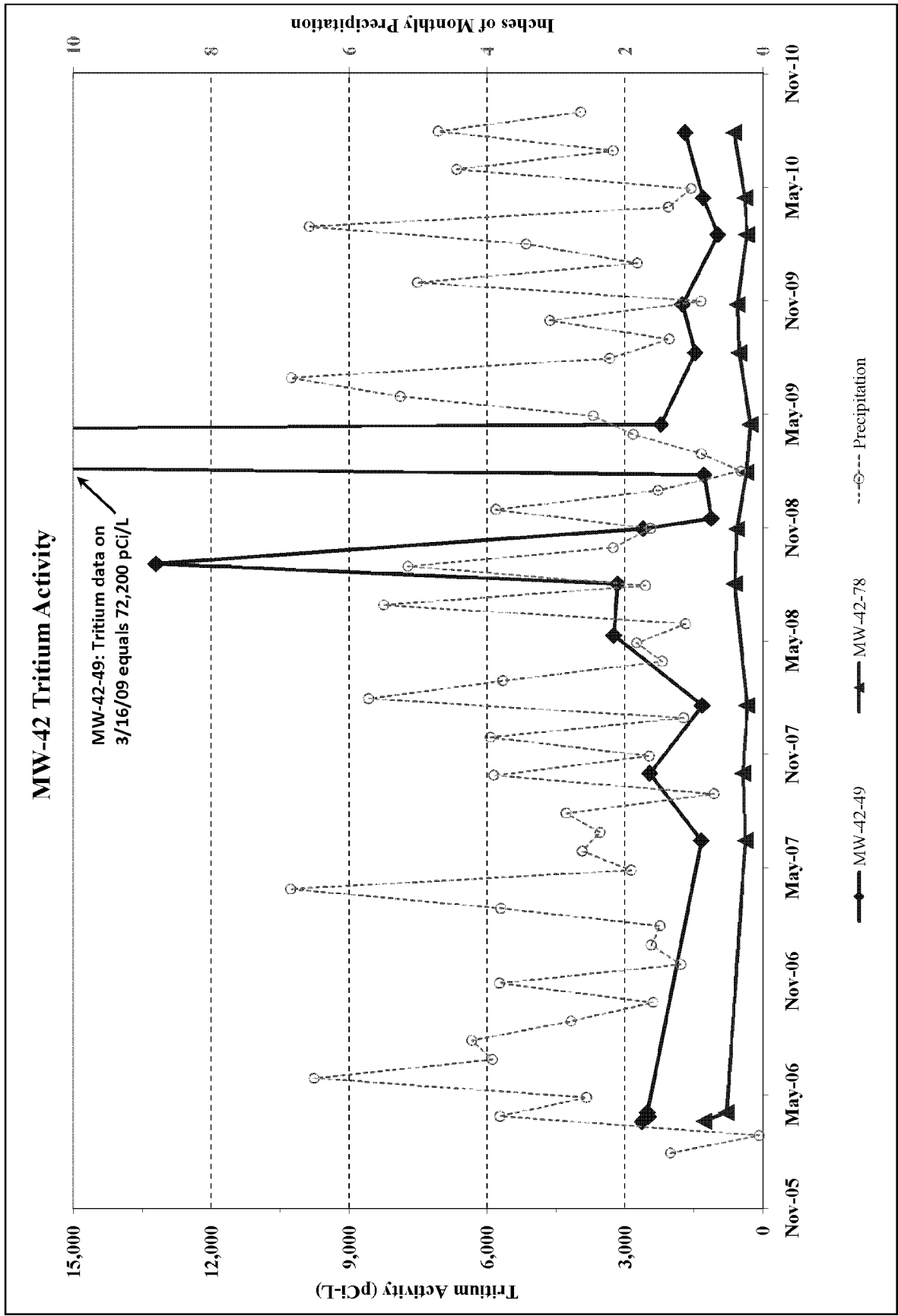


FIGURE G9

# MW-49 Tritium Activity

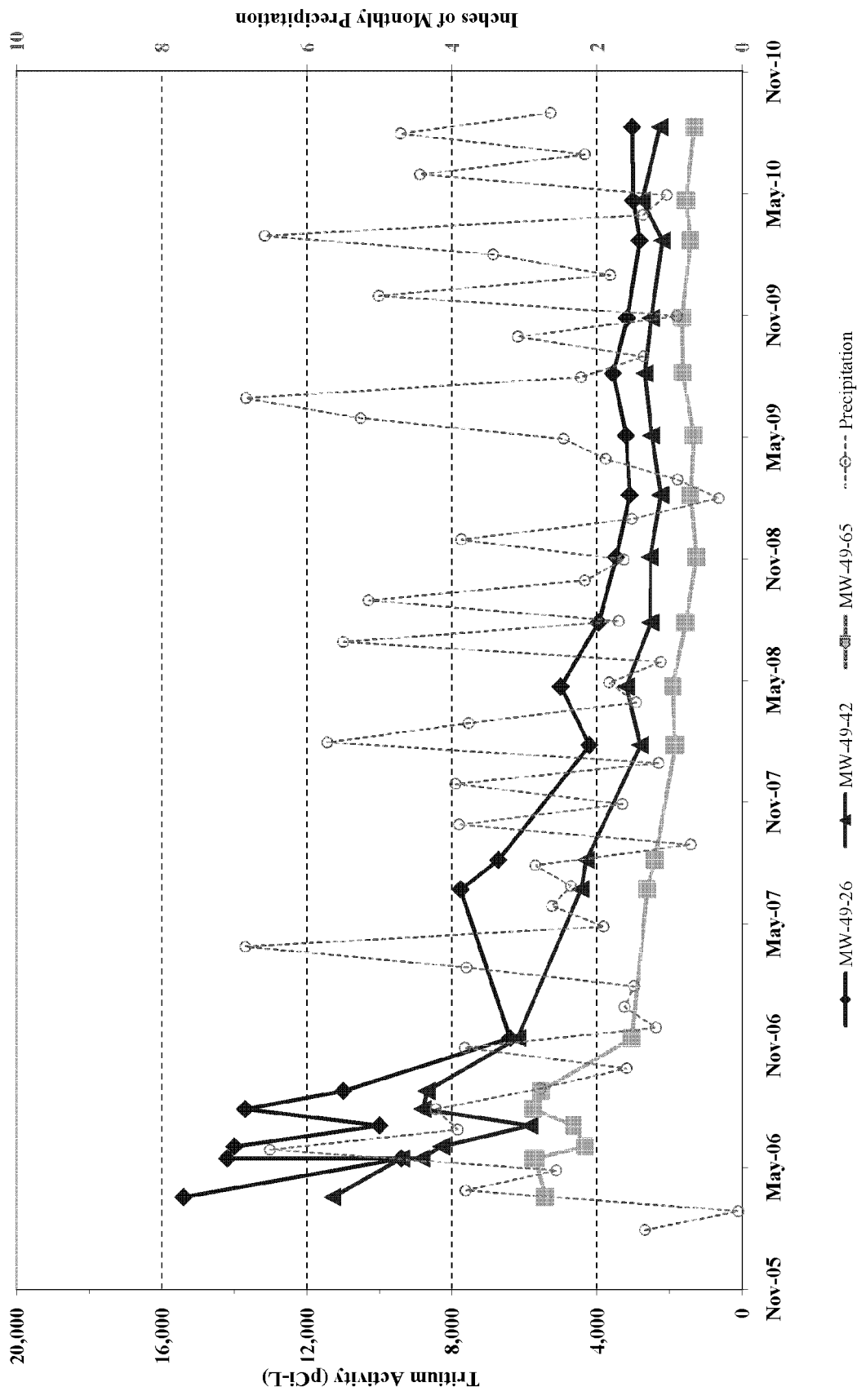


FIGURE G10

# MW-50 Tritium Activity

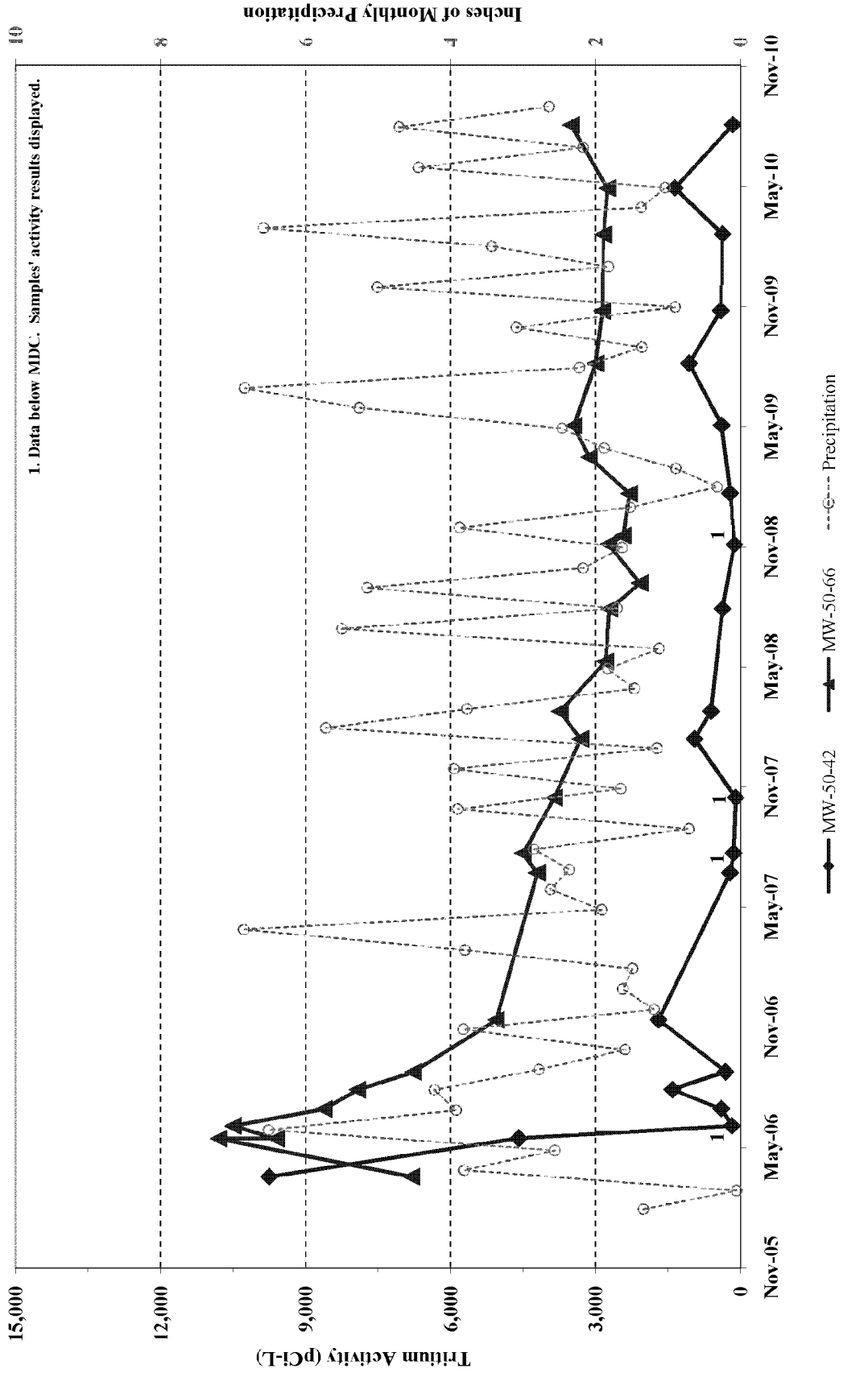
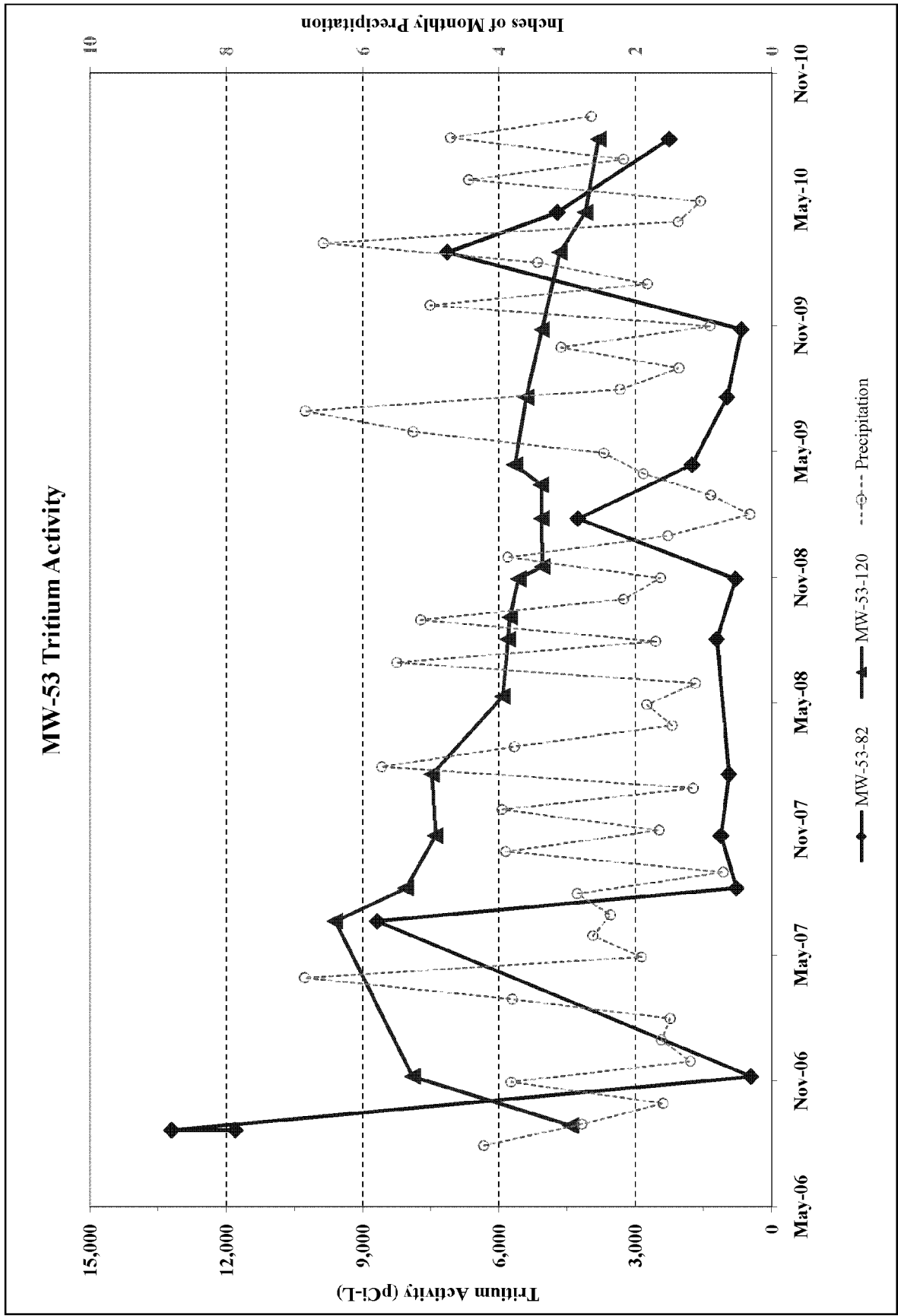


FIGURE G11



**FIGURE G12**



# MW-55 Tritium Activity

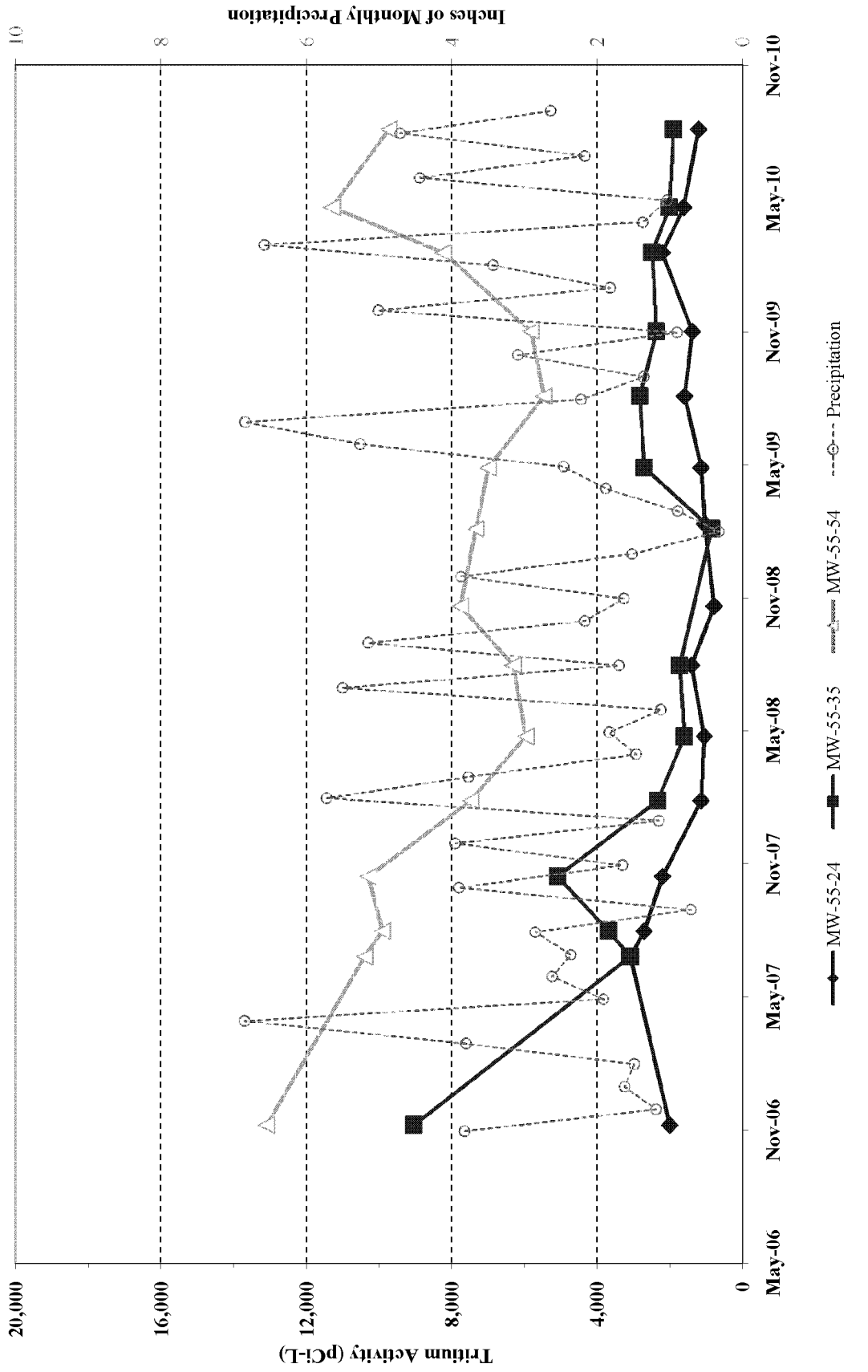
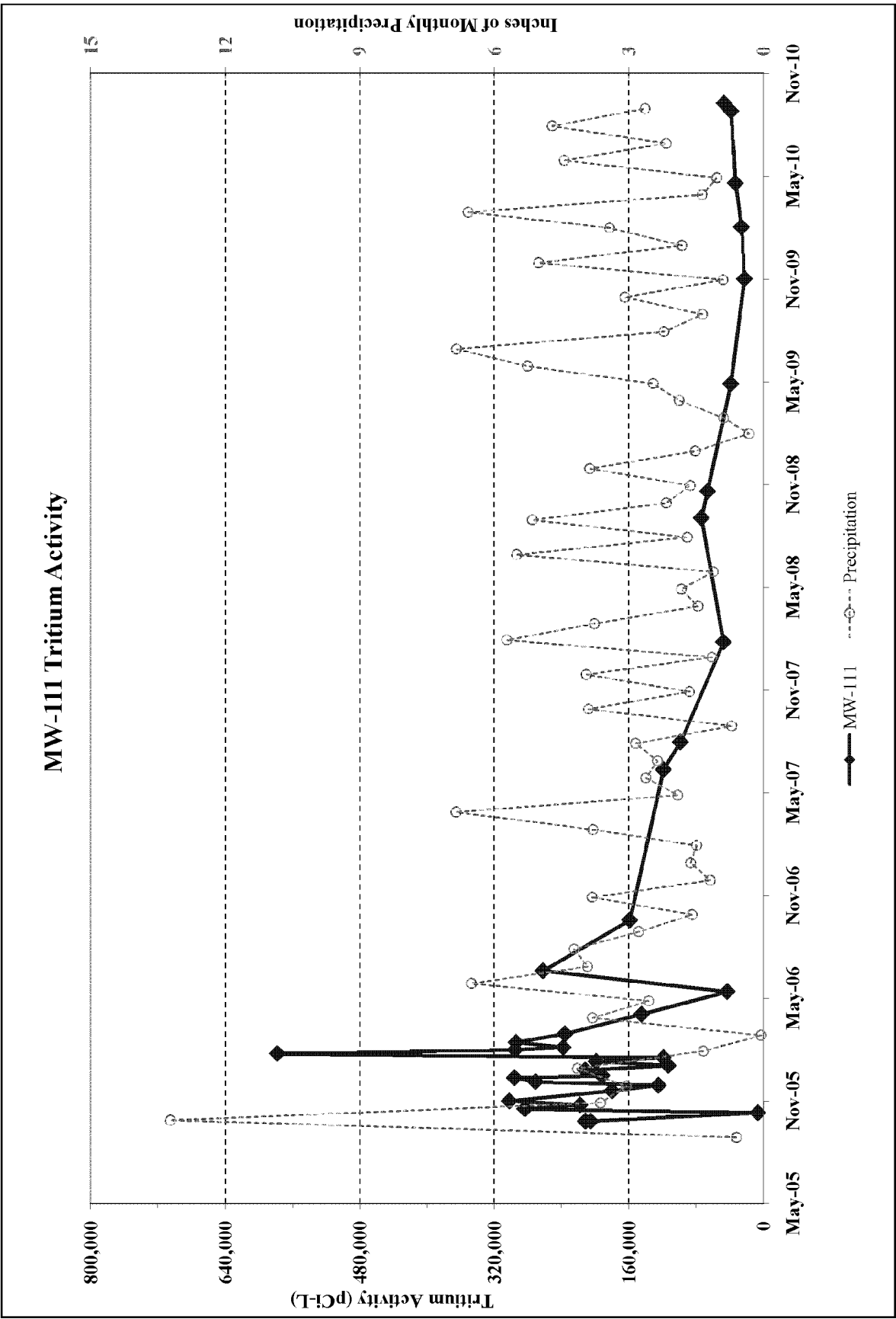


FIGURE G13



**FIGURE G14**

# MW-66 Tritium Activity

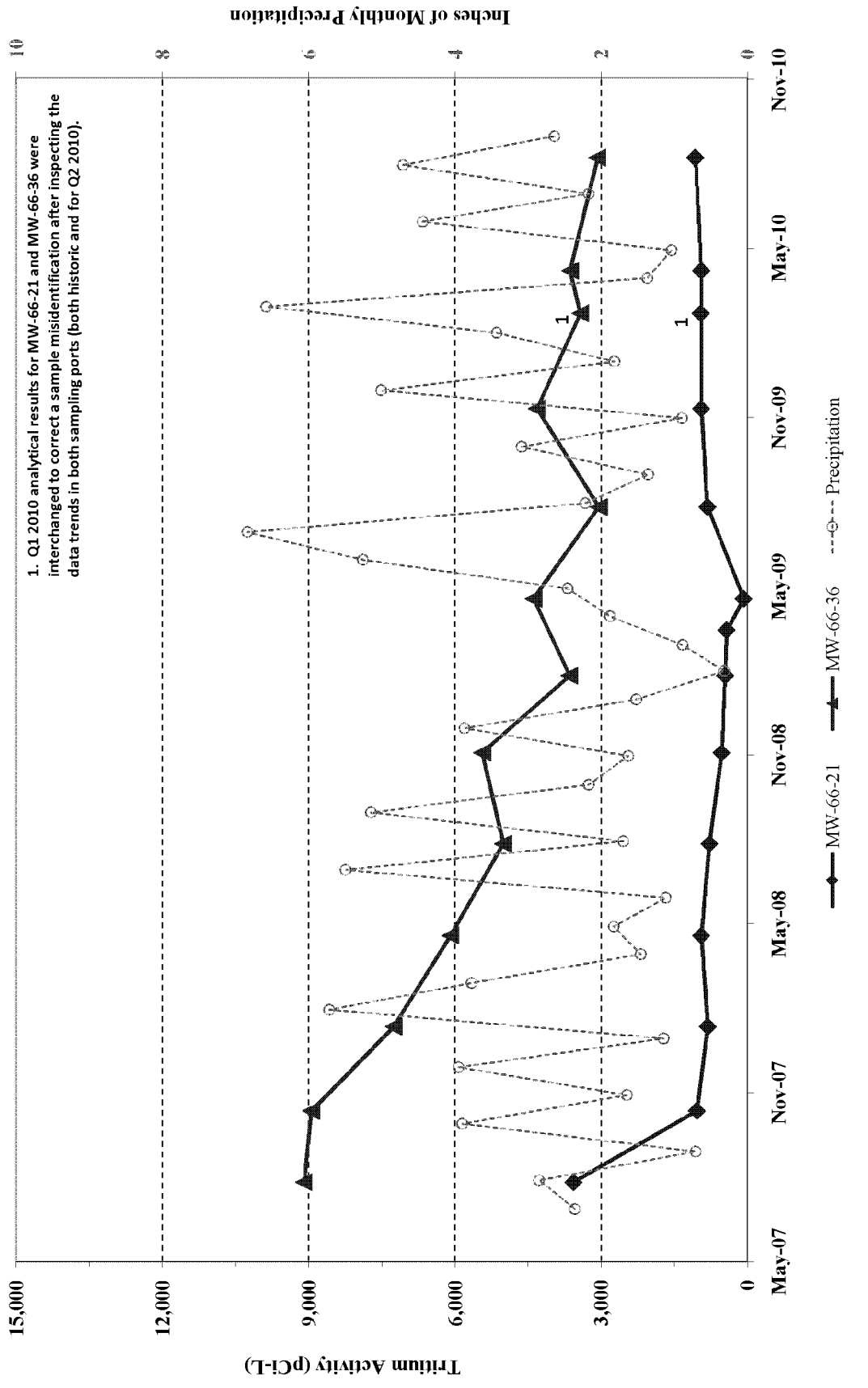
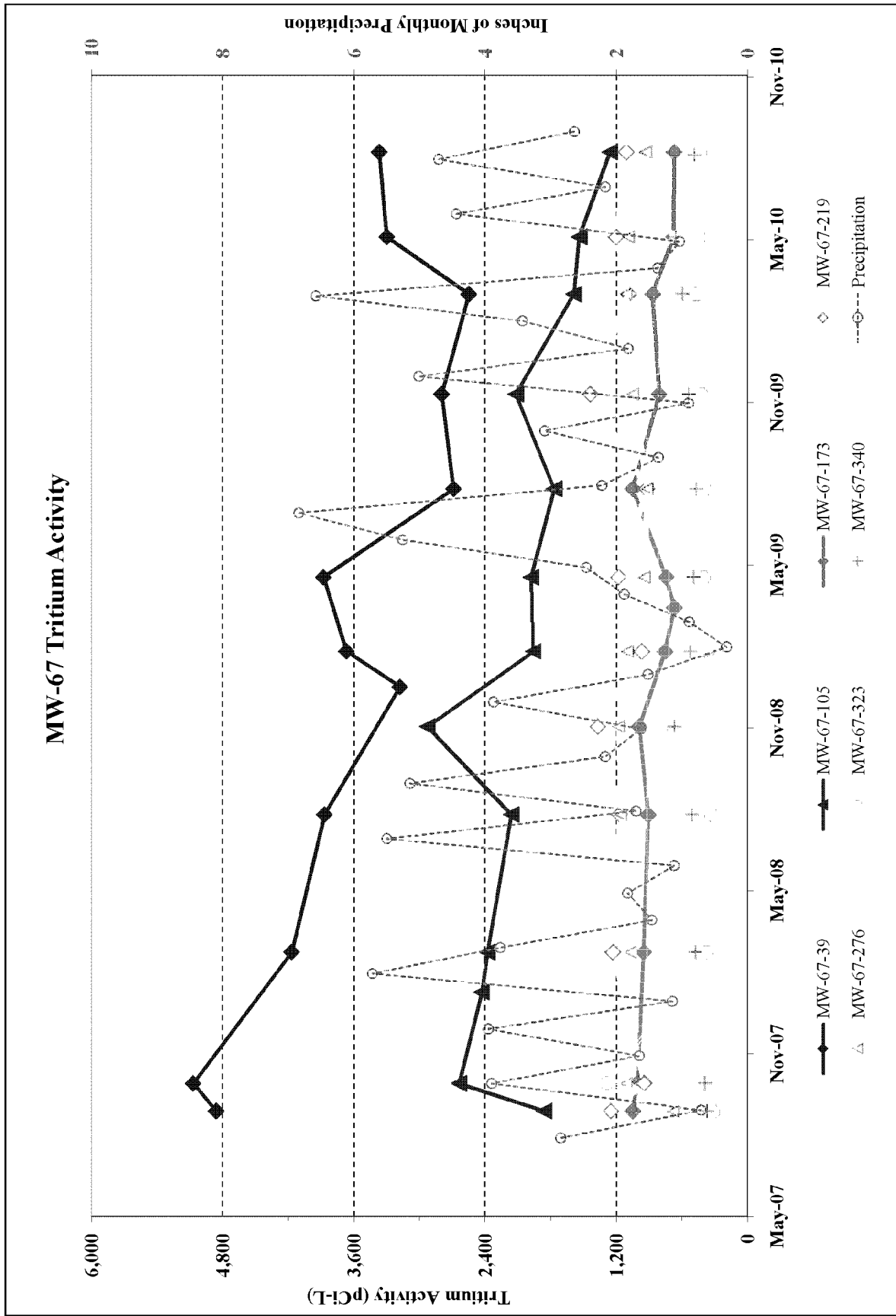
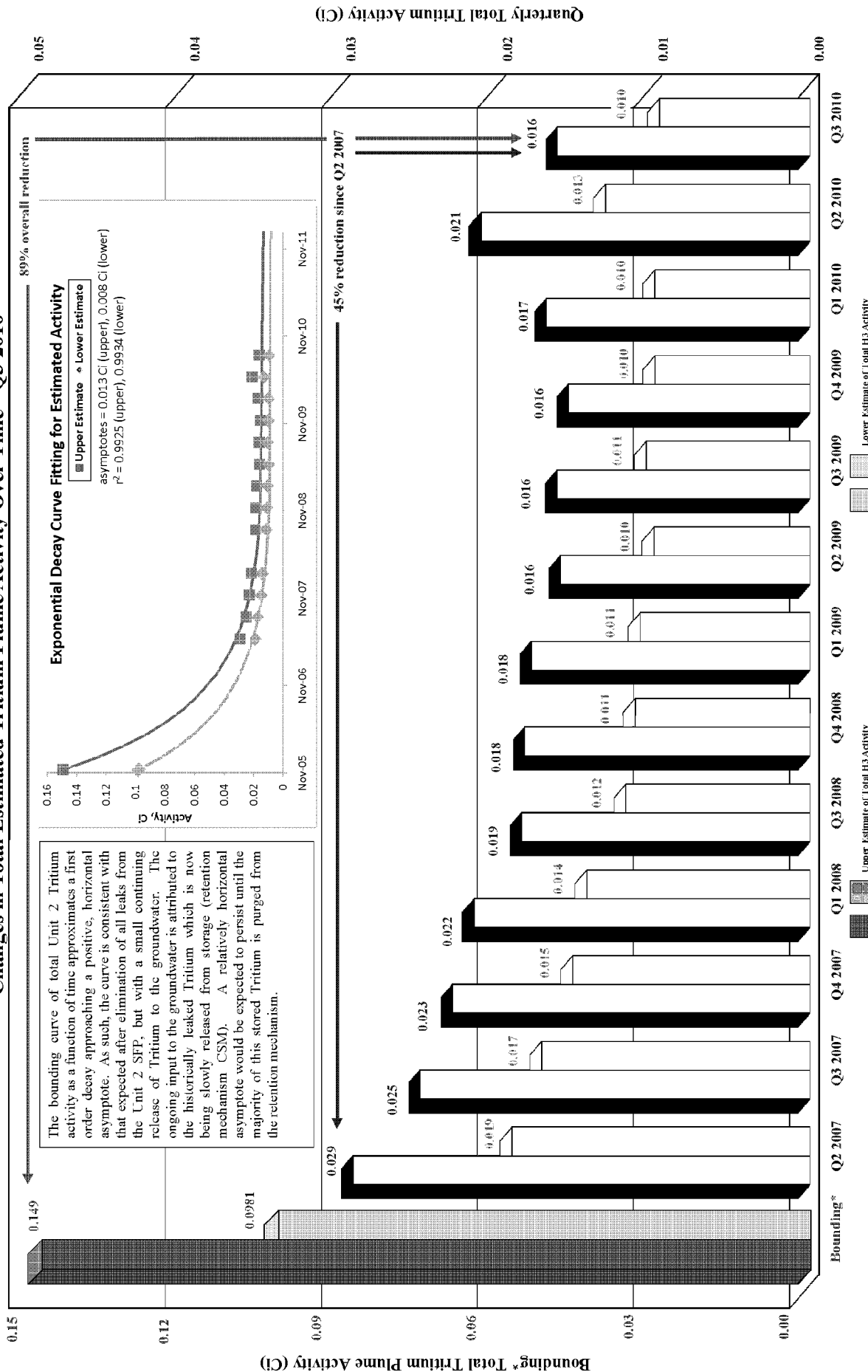


FIGURE G15



**FIGURE G16**

### Changes in Total Estimated Tritium Plume Activity Over Time - Q3 2010



Note: Lower estimate is based on a porosity of 0.0003 which was derived from a pumping test conducted in 2006. Upper estimate is based on a porosity of 0.003 derived from a tracer test conducted in 2007. The Q2 2007 to Q1 2010 Tritium plume activity estimates are each based on Tritium levels measured in the groundwater monitoring installations at individual quarterly "snapshots" in time.  
 \*The bounding activity estimate, however, encompasses a longer period of time, and is focused on the Tritium levels existing during the earlier portions of the groundwater investigation. During this period of time, before termination of all the identified SFP leaks, Tritium concentrations were at their highest levels, but the network of monitoring installations was still being installed. Therefore, measurements made at multiple times were required to capture early data covering the full extent of the Tritium plume; primarily over the period from Nov 2005 through Nov 2006 (a smaller percentage of the Tritium level required inclusion of measurements through Sep 07). For the bounding Tritium plume activity estimate, the highest value recorded for each monitoring location during this time period was used in the analysis. For further discussion see Sections 6.0, 7.0 and 8.0 of the Final Hydrogeologic Site Investigation Report, prepared by OZA and dated January 7, 2008.

Figure G-17



## **APPENDIX H SOUTHERN BOUNDARY WELLS**

# TEMPORAL TRITIUM TRENDS IN SOUTHERN BOUNDARY WELLS

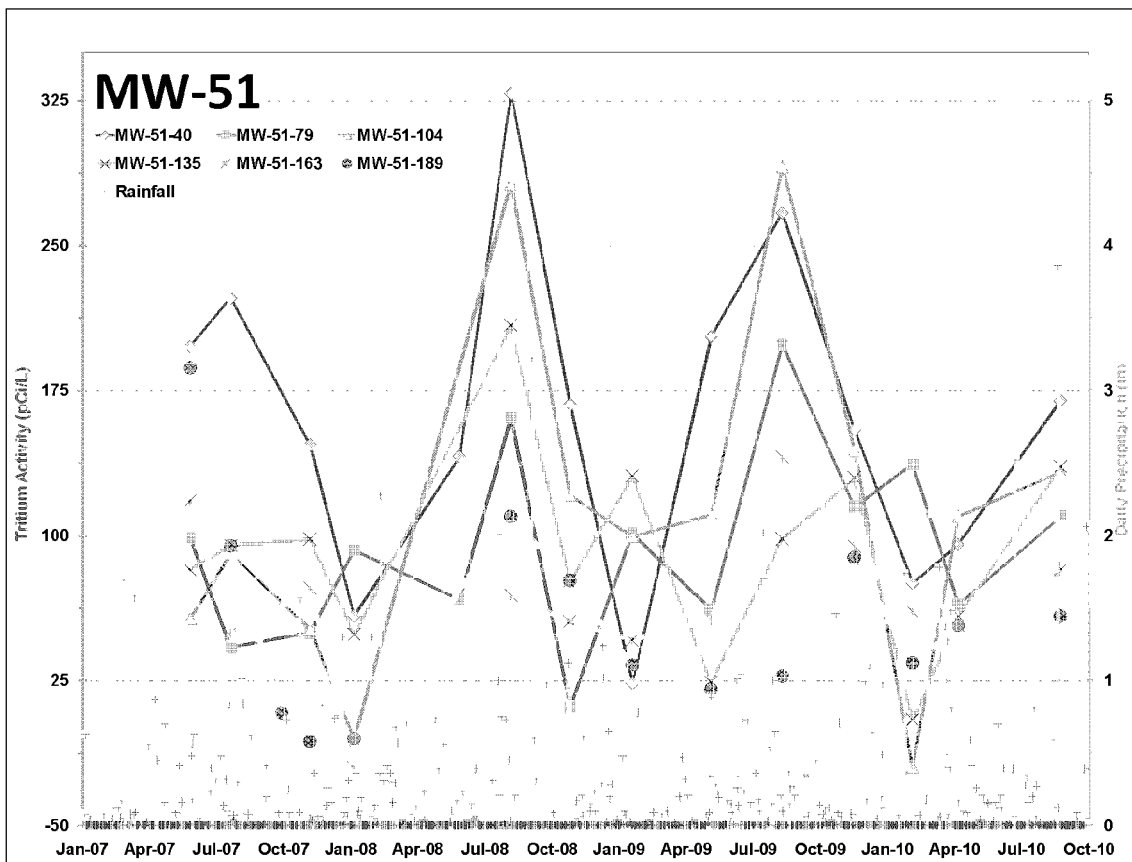
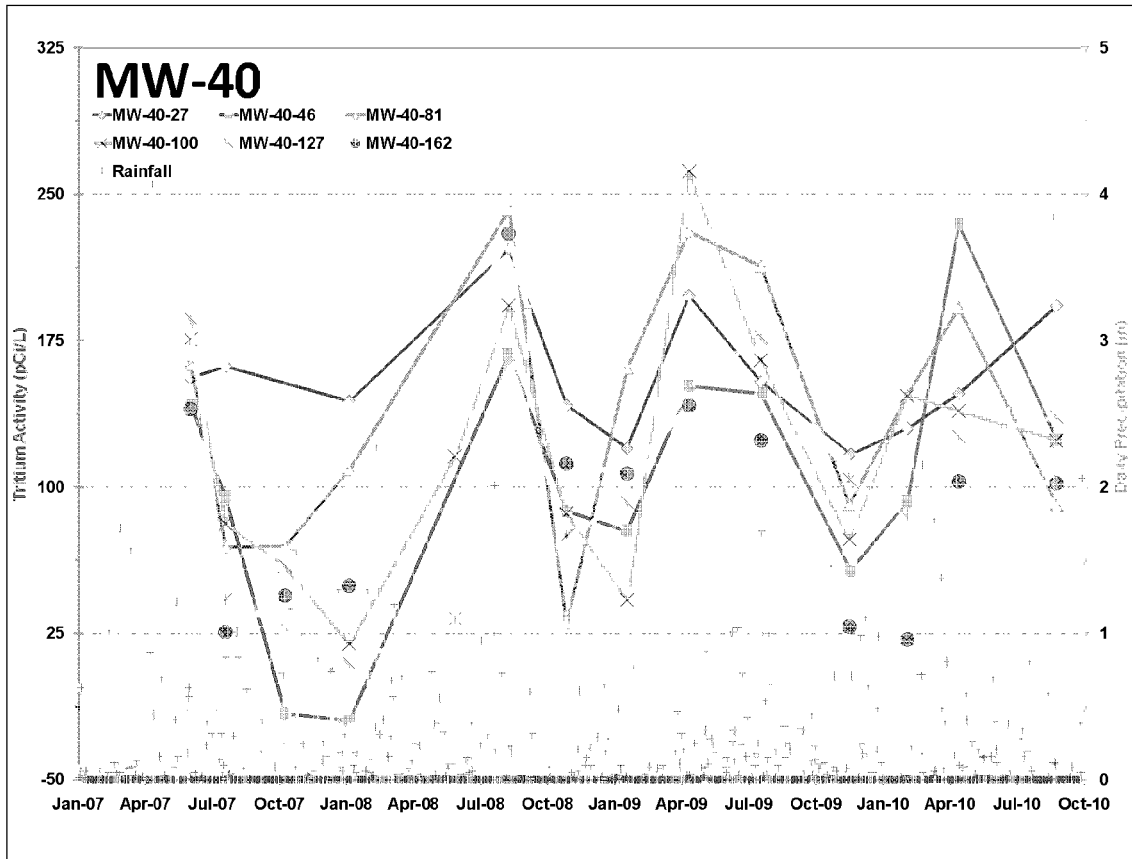


FIGURE H1